

## Case Study 8: QFT Robust Control

This case study contains an application implementing the QFT robust control which aims at maximizing the energy extraction for a PMSG-based WECS. The control structure contains two separate controllers,  $C_1$  and  $C_2$ , developed by applying the QFT method on the concerned WECS operating in two wind velocity ranges: 3–9 m/s and 5–11 m/s respectively. This application uses the mdl-file named `robust_QFT_ctrl.mdl`; it is described below.

*Scope:* Evaluation by numerical simulation of the control method aiming at maximizing the captured power for a low-power fixed-pitch PMSG-based wind turbine by using a control structure designed using the QFT method. As the system is nonlinear, variant, presents quasi-unknown dynamics and is subject to unknown disturbances, this method can be the key to obtain a robust controller for driving the WECS to its optimal energy regime in the partial-load operation. Two controllers (each containing a prefilter and a compensator) have been developed using the QFT Toolbox from MATLAB®. The two controllers are embedded in a multi-model control structure.

*Application analysis:* The file `data_robust_QFT.m` contains the system data. The parameters concerning the system modelling as well as the QFT controller transfer functions are given here. The mdl-file is organized as follows. The plant is placed central-upper, the controller block is at the bottom of the diagram. The wind velocity synthesizer, placed in the upper-left corner, allows using a pre-computed non-stationary wind speed sequence (selection 4) for feeding the WECS; other sequences (including constant wind) are also available. In the bottom-left corner one can see some blocks (from up to down): the system data loading button, the scopes and some computation/display blocks.

The plant is modelled using the simplified aerodynamic model (which provides the wind torque), the motion equation of the rigid drive train and the  $d$ - $q$  modelling of the PMSG (providing  $i_d$ ,  $i_q$  and the electromagnetic torque).

The controller is structured as follows. The wind velocity and the rotational speed feed the two controllers. Their output is weighted by a weighting generator. The weights are obtained based on the low-frequency component of the wind speed. These weights are complementary, as the two controllers are designed for different wind velocity ranges. A filter cancelling the turbulence component can be employed in obtaining the weights.

*Running the application:*

*Step 1:* Load system parameters.

*Step 2:* Select from the menu “Simulation → Parameters” a convenient time horizon and proceed with the simulation.

*Step 3:* The switch feeding the control input in the block entitled `QFT control` must be set on the “multi-model controller” position.

*Step 4:* Select the pre-computed sequence of wind speed (selection 4).

*Step 5:* Dynamical system behaviour can be viewed by opening the scopes (upper-left corner of the application file). Operating point position or its standard deviation around the ORC can be plotted using the LSS mechanical power and rotational speed data (vectors `pwr1` and `omg1`) saved in the workspace from the associated scopes. Check the control performance by opening the power coefficient (`cP`) and the tip speed (`lam`) scopes, also. The control components,

corresponding to the two controllers in the multi-model design structure, are  $c_{-1}$  and  $c_{-2}$ . The histograms of the tip speed ratio for several values of the wind filter cut-of frequency (from 5 s to 25 s) can be plotted using the following commands:

```
lam1=lam(1000:length(lam),2);      % uses the tip speed sequence data stored on
                                   % the associated scope
[hst,ics]=hist(lam1,100);          % histogram with 100 bins
plot(ics,hst/length(lam1),'k');    % normalisation
```

*Step 6:* Change the wind velocity to constant value (selection 1) and change the wind mean value in steps of 1 m/s. The system dynamic behaviour can be seen on the HSS rotational speed ( $\omega_{mgh}$ ) scope; the disturbance rejection can be assessed on the tip speed ratio or the power coefficient scopes. The electromagnetic torque evolutions ( $e_{mT}$ ), showing the dynamic response deterioration, can be viewed on the corresponding scope.

*Step 7:* Set the switch feeding the control input in the block named QFT control on the “QFT controller” position.

*Step 8:* Repeat *Steps* from 4 to 6 to assess the QFT-controlled WECS dynamic behaviour and controller performance.

*Remarks:* The PMSG is considered to be voltage-controlled by a rectifier-chopper pair, whose influence on the PMSG can be assessed through the equivalent resistance experienced by the generator. In the diagram  $R_{ch}$  plays the role of  $R_S$  from the textbook.

The user can develop other controller(s) by following the design procedure given in Appendix B.3 from the textbook.