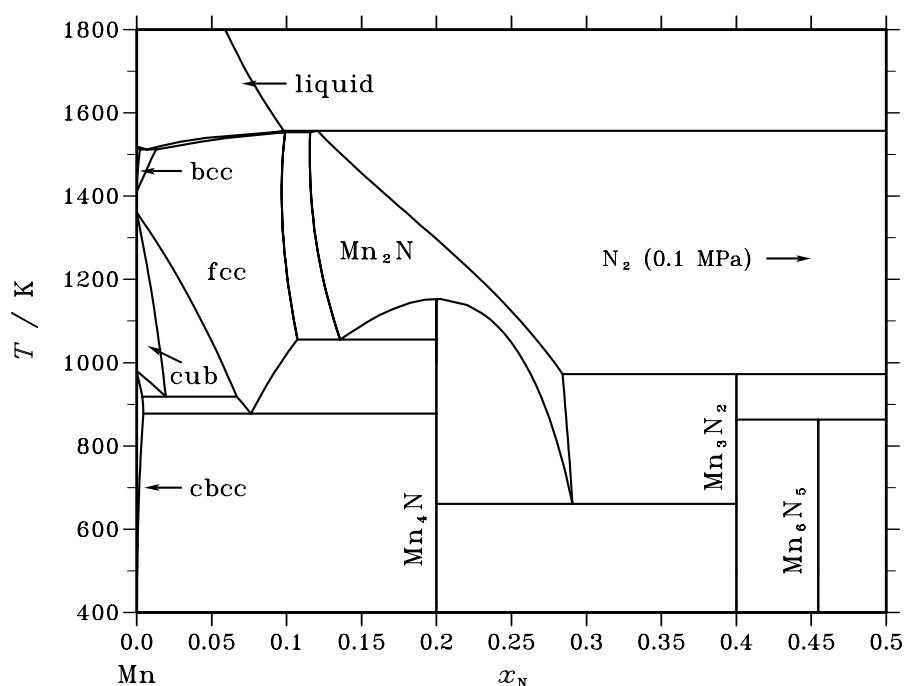


**Mn – N (Manganese – Nitrogen)****Fig. 1.** Calculated phase diagram for the system Mn-N.

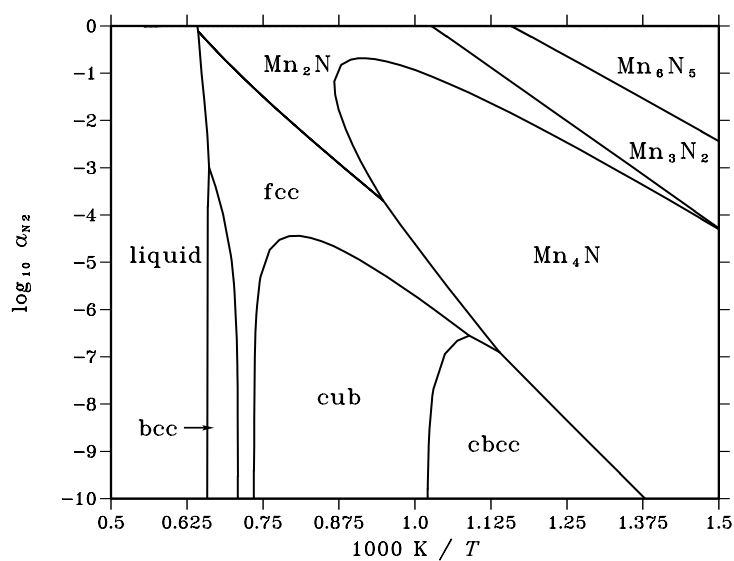
Mn and N are both important alloying elements in steel. By increasing the Mn content the solubility of N can also be increased in stainless steels. The solubility of N in the Mn phases are highest in the fcc-phase. At even higher N content there are several stable nitrides, at low temperature  $\text{Fe}_4\text{N}$ ,  $\text{Mn}_3\text{N}_2$  and  $\text{Mn}_6\text{N}_5$ , all modelled as stoichiometric. At higher temperature the hexagonal  $\text{Mn}_2\text{N}$  is stable with a broad composition range. A thermodynamic assessment of the Mn-N system has been reported in [93Qiu].

**Table I.** Phases, structures and models.

Phase	Struktur-bericht	Prototype	Pearson symbol	Space group	SGTE name	Model
liquid					LIQUID	$(\text{Mn},\text{N})_1$
fcc	A1	Cu	$cF4$	$Fm\bar{3}m$	FCC_A1	$\text{Mn}_1(\text{N},\square)_1$
bcc	A2	W	$cI2$	$Im\bar{3}m$	BCC_A2	$\text{Mn}_1(\text{N},\square)_3$
cbcc	A12	$\alpha\text{Mn}$	$cI58$	$I\bar{4}3m$	CBCC_A12	$\text{Mn}_1(\text{N},\square)_1$
cub	A13	$\beta\text{Mn}$	$cP20$	$P4_132$	CUB_A13	$\text{Mn}_1(\text{N},\square)_1$
$\text{Mn}_4\text{N}$	$L'_1$	$\text{Fe}_4\text{N}$	$cP5$	$Pm\bar{3}m$	FE4N	$\text{Mn}_4\text{N}_1$
$\text{Mn}_2\text{N}$	$L'_3$	$\text{Fe}_2\text{N}$	$hP3$	$P6_3/mmc$	HCP_A3	$\text{Mn}_2(\text{N},\square)_1$
$\text{Mn}_3\text{N}_2$	$L'_2b$	$\text{ThH}_2$	$tI6$	$I4/mmm$	MN6N4	$\text{Mn}_3\text{N}_2$
$\text{Mn}_6\text{N}_5$	...	...	$tF^*$	...	MN6N5	$\text{Mn}_6\text{N}_5$

**Table II.** Invariant reactions.

Reaction	Type	$T / \text{K}$	Compositions / $x_{\text{N}}$			$\Delta_{\text{f}}H / (\text{J/mol})$
liquid + gas $\rightleftharpoons \text{Mn}_2\text{N}$	gas-peritectic	1556.9	0.098	0.999	0.121	–22096
liquid + $\text{Mn}_2\text{N} \rightleftharpoons \text{fcc}$	peritectic	1553.7	0.091	0.116	0.099	–12756
liquid $\rightleftharpoons \text{bcc} + \text{fcc}$	eutectic	1511.6	0.007	0.002	0.013	–14103
$\text{Mn}_2\text{N} \rightleftharpoons \text{Mn}_4\text{N}$	congruent	1152.9	0.200	0.200		–6361
$\text{Mn}_2\text{N} \rightleftharpoons \text{fcc} + \text{Mn}_4\text{N}$	eutectoid	1055.1	0.136	0.107	0.200	–2265
$\text{Mn}_2\text{N} + \text{gas} \rightleftharpoons \text{Mn}_3\text{N}_2$	gas-peritectoid	972.9	0.284	1.000	0.400	–14050
cub $\rightleftharpoons \text{cbcc} + \text{fcc}$	eutectoid	918.0	0.019	0.004	0.067	–1513
$\text{fcc} \rightleftharpoons \text{cbcc} + \text{Mn}_4\text{N}$	eutectoid	877.8	0.076	0.004	0.200	–4006
$\text{Mn}_3\text{N}_2 + \text{gas} \rightleftharpoons \text{Mn}_6\text{N}_5$	gas-peritectoid	863.0	0.400	1.000	0.455	–6118
$\text{Mn}_2\text{N} \rightleftharpoons \text{Mn}_4\text{N} + \text{Mn}_3\text{N}_2$	eutectoid	661.0	0.291	0.200	0.400	–4006

**Fig. 2.** Calculated temperature-activity phase diagram. Reference state:  $\frac{1}{2}\text{N}_2(\text{gas}, 0.1 \text{ MPa})$ .**Table III.** Standard reaction quantities at 298.15 K for the compounds per mole of atoms.

Compound	$x_{\text{N}}$	$\Delta_{\text{f}}G^{\circ} / (\text{J/mol})$	$\Delta_{\text{f}}H^{\circ} / (\text{J/mol})$	$\Delta_{\text{f}}S^{\circ} / (\text{J/(mol}\cdot\text{K)})$	$\Delta_{\text{f}}C_P^{\circ} / (\text{J/(mol}\cdot\text{K)})$
$\text{Mn}_4\text{N}$	0.200	–19474	–23177	–12.419	0.072
$\text{Mn}_3\text{N}_2$	0.400	–29143	–38378	–30.974	1.232
$\text{Mn}_6\text{N}_5$	0.455	–30690	–41426	–36.007	1.547

## References

- [93Qiu] C. Qiu, A. Fernández Guillermet: Z. Metallkd. **84** (1993) 11–22.