

# Broadband Outdoor Radiometer Calibration

## **BORCAL 2006-02**

Customer:  
NREL-SRRL-BMS

Calibration Facility:  
Solar Radiation Research Laboratory

Latitude: 39.740°N  
Longitude: 105.180°W  
Elevation: 1829.0 meters AMSL  
Avg. Station Pressure: 835.0 mBar  
Time Zone: -7.0

Calibration date  
06/11/2006 to 06/17/2006

Report Date  
June 19, 2006

## **NOTICE**

This report was prepared as an account of work sponsored by an agency of the United States government. Neither the United States government nor any agency thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States government or any agency thereof.

# Broadband Outdoor Radiometer Calibration Report

Table of contents

Introduction.....3

Reference irradiance plots.....4

Meteorological plots.....5

Control Instrument history plots.....6

Results summary.....8

Appendix 1 Instrument Details.....A1-1

Appendix 2 BORCAL Notes.....A2-1

# Introduction

This report compiles the calibration results from a Broadband Outdoor Radiometer Calibration (BORCAL). The work was accomplished at the Radiometer Calibration Facility shown on the front of this report. The calibration results reported here are traceable to the World Radiometric Reference and to the National Institute of Standards and Technology.

This report includes these sections:

- Calibration Environment - meteorological conditions and irradiance reference data encountered during the event.
- Control Instruments - a group of instruments included in each BORCAL event that provides a measure of process consistency.
- Results Summary - a table of all instruments included in this report summarizing their calibration results and uncertainty.
- Instrument Details - the calibration certificates and suggested methods of applying results for each instrument.

The BORCAL process is described in "Improved Methods for Broadband Outdoor Radiometer Calibration (BORCAL)," Wilcox, S., Andreas, A., Reda, I., and Myers, D., Proceedings of the ARM Science Team Meeting, St. Petersburg, Florida, April 2002.

# Reference Irradiance

0.0° / 0.0° Tilt / Azm

Figure 1. Reference Irradiance

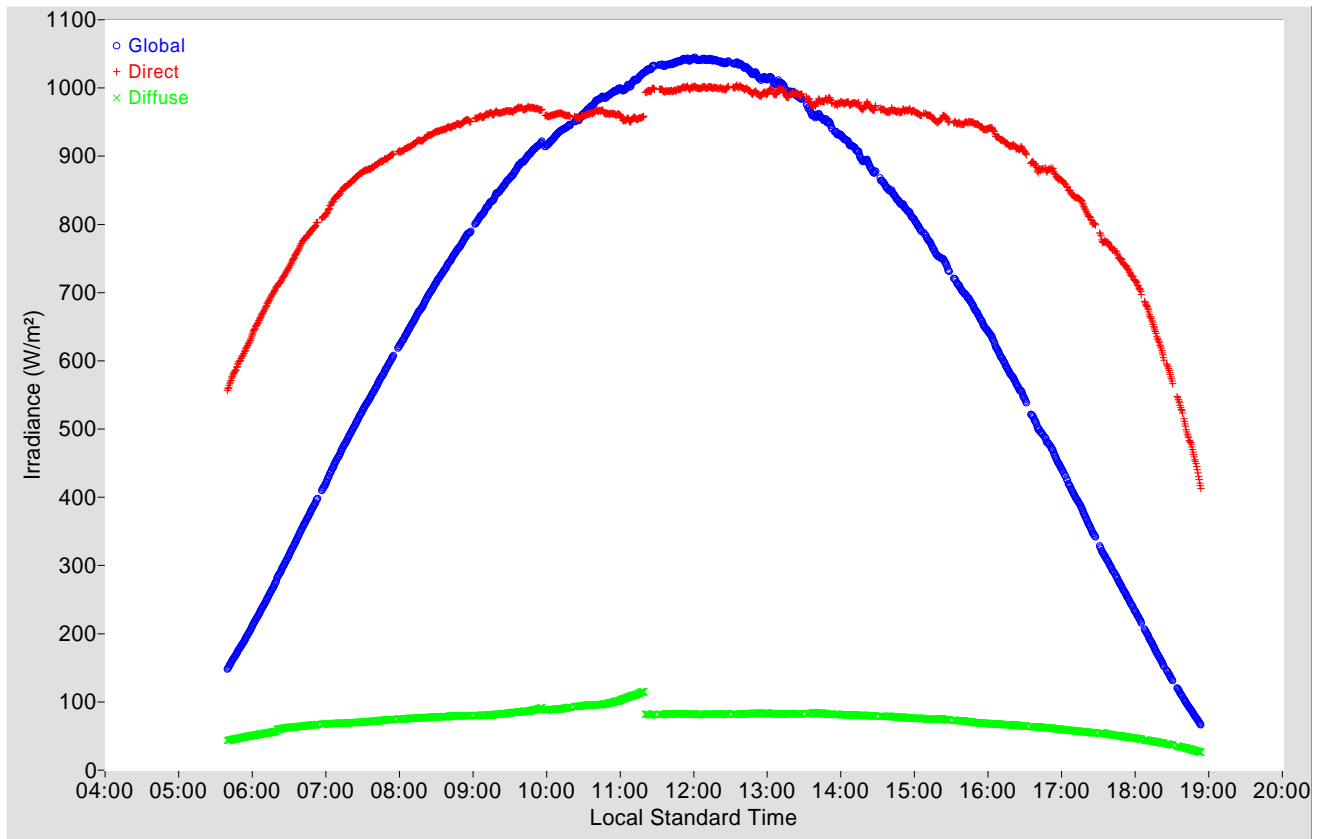
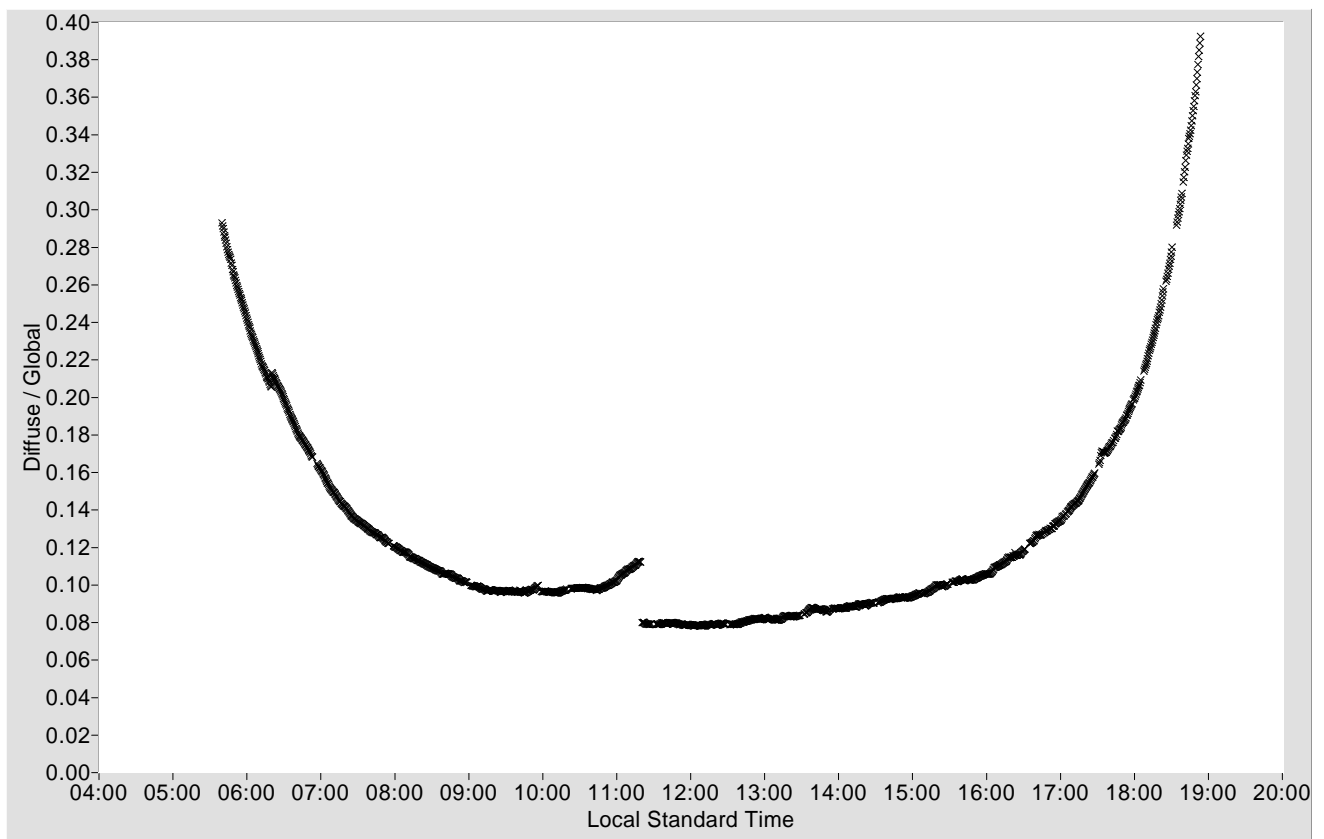


Figure 2. Diffuse / Global

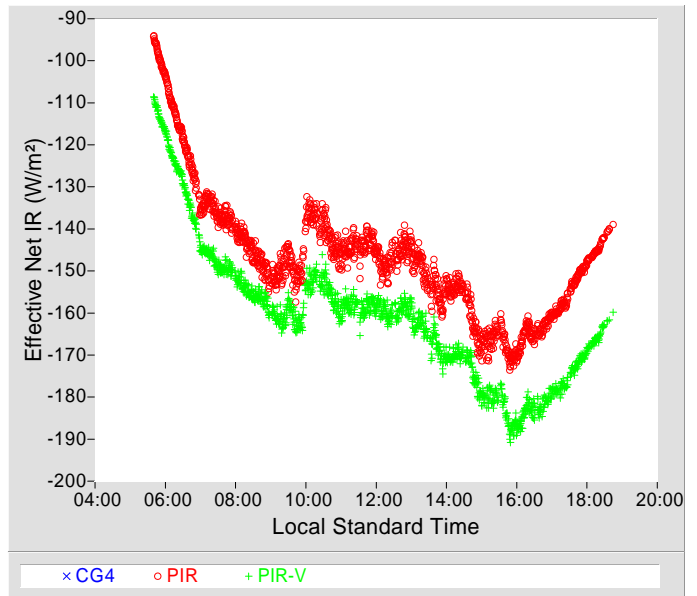


# Meteorological Observations

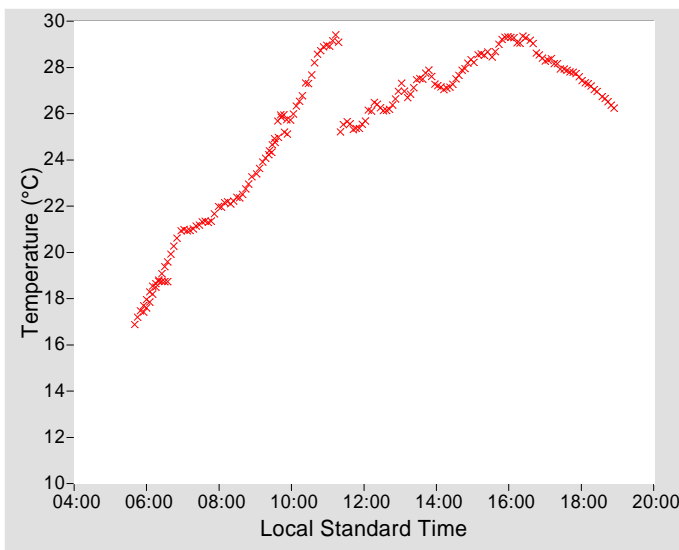
**Table 1. Meteorological Observations**

Observations	Mean
Temperature (°C)	25.19
Humidity (%)	32.85
Pressure (mBar)	817.3
Est. Aerosol Optical Depth (BB)	0.0582

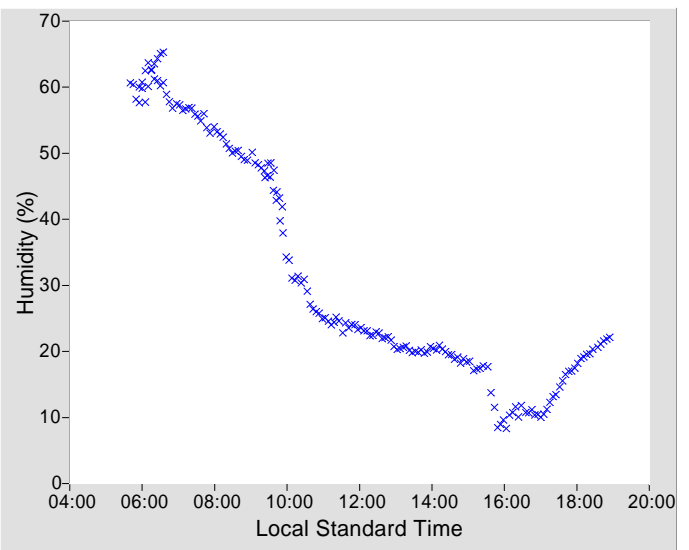
**Figure 3. Effective Net Infrared**



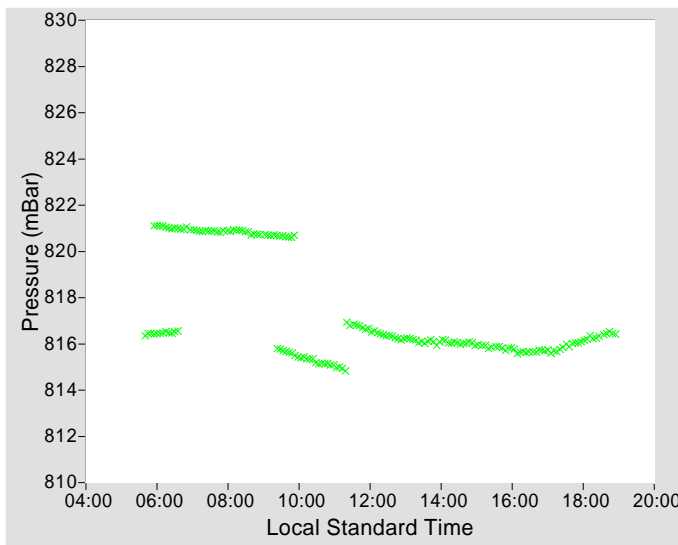
**Figure 4. Temperature**



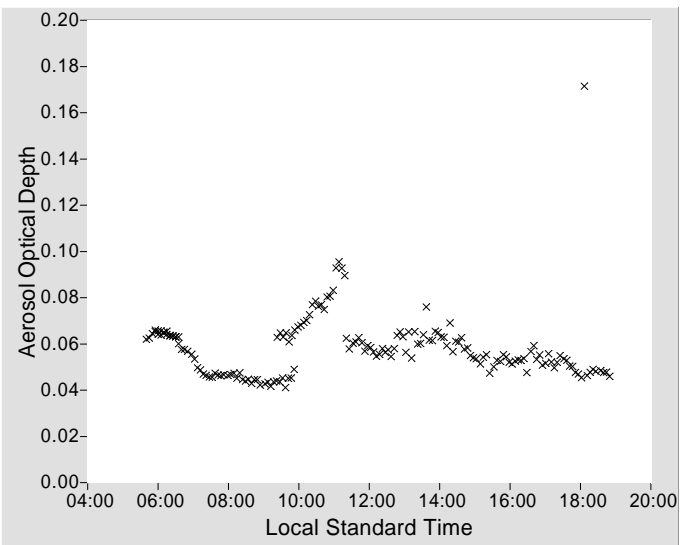
**Figure 5. Humidity**



**Figure 6. Pressure**



**Figure 7. Estimated Broadband Aerosol Optical Depth**



# Control Instrument History

Figure 8. Eppley FPP Control Instrument History

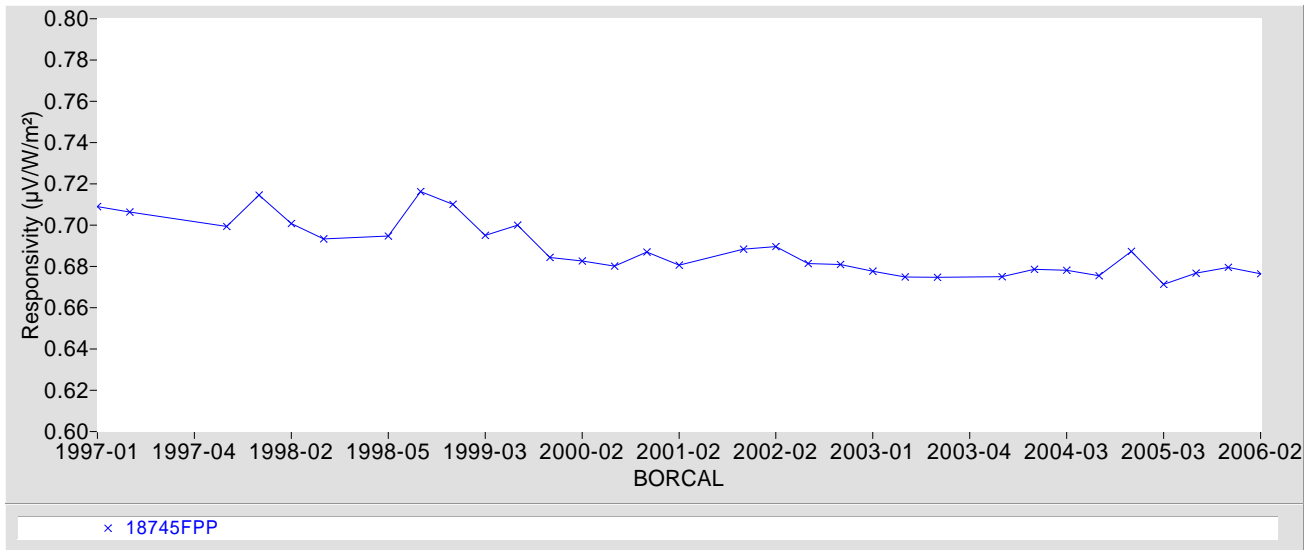


Figure 9. Eppley NIP Control Instrument History

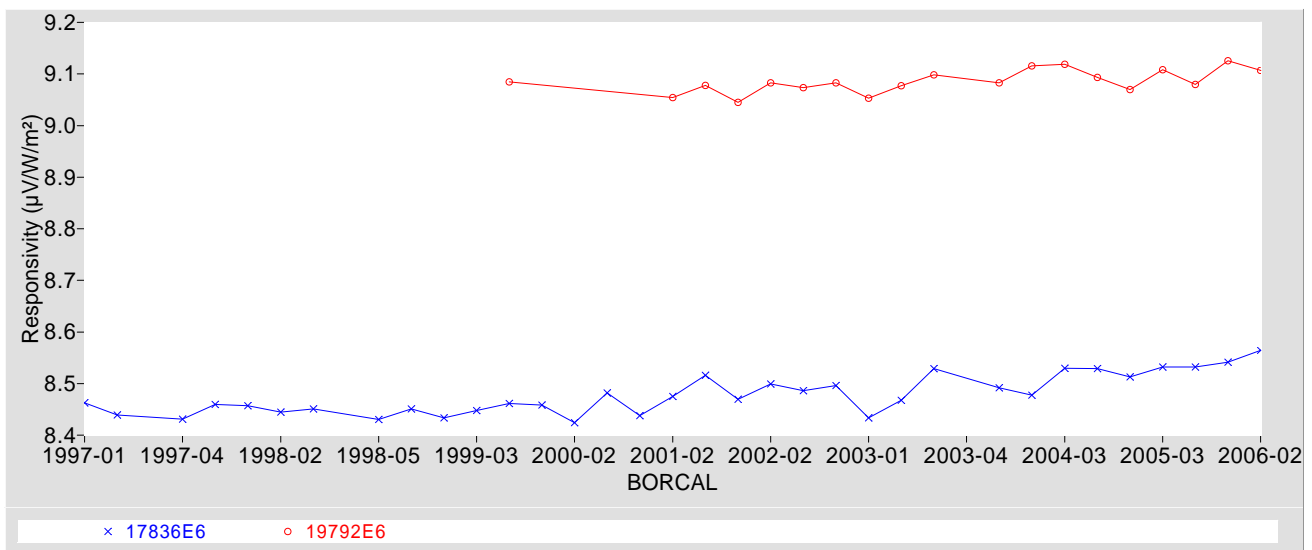
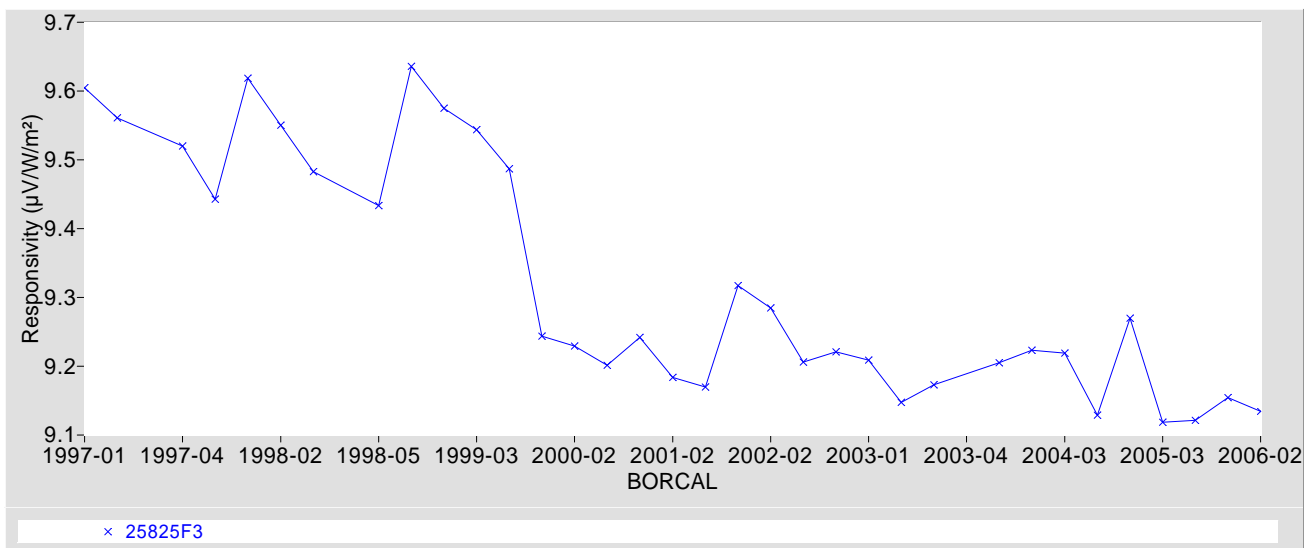
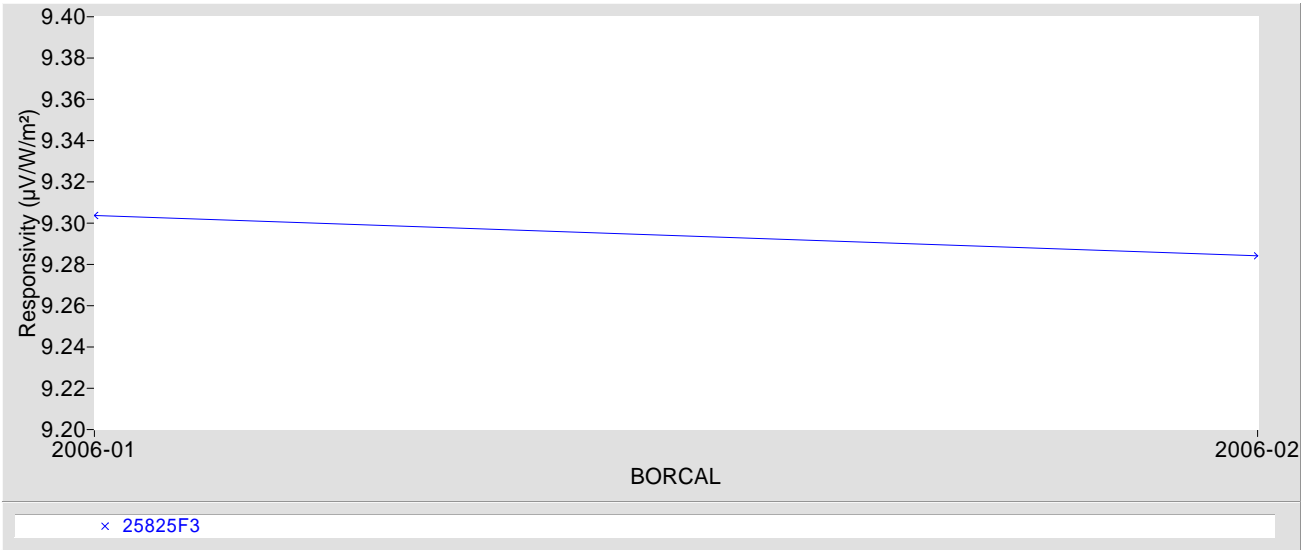


Figure 10. Eppley PSP Control Instrument History



# Control Instrument History

Figure 11. Eppley PSP Control Instrument History (Effective Net IR Corrected)





# Results Summary

**Table 2. Results Summary**

Instrument	RS@45 <sup>1</sup> ( $\mu\text{V}/\text{W}/\text{m}^2$ )	CF@45 <sup>1</sup> ( $\text{W}/\text{m}^2/\text{mV}$ )	U95 (%)	RSc@45 <sup>1 2</sup> ( $\mu\text{V}/\text{W}/\text{m}^2$ )	CFc@45 <sup>1 2</sup> ( $\text{W}/\text{m}^2/\text{mV}$ )	U95 corr. <sup>2</sup> (%)	RS net <sup>3</sup> ( $\mu\text{V}/\text{W}/\text{m}^2$ )	Page
010034	10.896	91.776	+1.85 / -1.37	n/a	n/a	n/a	n/a	A1-2
015189	10.871	91.988	+2.53 / -1.09	n/a	n/a	n/a	n/a	A1-7
18035F3	7.9216	126.24	+3.26 / -3.26	n/a	n/a	n/a	n/a	A1-12
25819F3	8.4979	117.68	+4.51 / -5.82	n/a	n/a	n/a	n/a	A1-17
30560F3	8.6185	116.03	+2.53 / -2.69	n/a	n/a	n/a	n/a	A1-22
31355E6	8.5877	116.45	+0.95 / -1.64	n/a	n/a	n/a	n/a	A1-27
PY1726	9.6898	103.20	+1.46 / -1.39	n/a	n/a	n/a	n/a	A1-30
PY1744	14.379	69.548	+2.13 / -1.54	n/a	n/a	n/a	n/a	A1-35
PY28244	12.889	77.585	+1.43 / -1.55	n/a	n/a	n/a	n/a	A1-40
PY28257	13.167	75.948	+3.32 / -5.49	n/a	n/a	n/a	n/a	A1-45

Note: Ancillary Data for BORCAL starts on page A1-50.

<sup>1</sup> CF = 1000 / Rs      <sup>2</sup> Effective Net IR Corrected

<sup>3</sup> Instrument's Effective Net IR Response

# **Appendix 1**

## **Instrument Details**

Calibration Certificates: 2 Pages for each Pyrheliometer/Shaded Pyranometer and 3 Pages for each Unshaded Pyranometer.

Suggested Methods: 1 Page for each Pyrheliometer/Shaded Pyranometer and 2 Pages for each Unshaded Pyranometer.

Ancillary Data for BORCAL: Last Page of a Calibration Certificate. Note: This appears only once, at the end of Appendix 1.

# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate

**Test Instrument:** Pyranometer **Manufacturer:** Kipp & Zonen  
**Model:** CM22 **Serial Number:** 010034  
**Calibration Date:** 6/17/2006 **Due Date:** 6/17/2007  
**Customer:** NREL-SRRL-BMS **Calibration Site Parameters:** see Ancillary Data  
**Environmental Conditions:** Outdoors, under natural sunlight (see Ancillary Data)  
**Data Acquisition Dates:** 6/11-12, 6/17

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppeley Absolute Cavity Radiometer Model HF, S/N 31104	03/14/2006	03/14/2007
Diffuse Irradiance †	Eppeley Black and White Pyranometer Model 8-48, S/N 32858	04/05/2006	04/05/2007
Diffuse Irradiance †	Eppeley Black and White Pyranometer Model 8-48, S/N 32871	04/05/2006	04/05/2007
Data Acquisition ‡	NREL Data Proof Scanner System Model RAP-DAQ, S/N 2005-998	11/22/2005	11/22/2006
Data Acquisition ‡	NREL Data Proof Scanner System Model RAP-DAQ, S/N 2005-999	11/22/2005	11/22/2006

† Traceable to the World Radiometric Reference

‡ Traceable to the National Institute of Standards and Technology

**Number of pages of certificate:** 4

**Calibration Procedure:** [1] Myers, D., Stoffel, T., Reda, I., Wilcox, S., and Andreas, A., 2002, "Recent Progress in Reducing the Uncertainty in and Improving Pyranometer Calibrations." Journal of Solar Energy Engineering, vol. 124, pp. 44-50. The American Society of Mechanical Engineers, Transactions of the ASME.  
[2] "Improved Methods for Broadband Outdoor Radiometer Calibration (BORCAL)," Wilcox, S., Andreas, A., Reda, I., and Myers, D., Proceedings of the ARM Science Team Meeting, St. Petersburg, Florida, April 2002. Available upon request.

This calibration certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval by the calibration facility. Calibration certificates without signatures are not valid.

**Calibrated by:** Ibrahim Reda and Steve Wilcox

**Certified by:**

-----  
Afshin M. Andreas

Title: Scientist II

Date: -----

**Quality Assured by:**

-----  
Daryl R. Myers

Title: Senior Scientist II

Date: -----

# Calibration Results

## 010034 Kipp & Zonen CM22

Figure 1. Responsivity vs Incident Angle

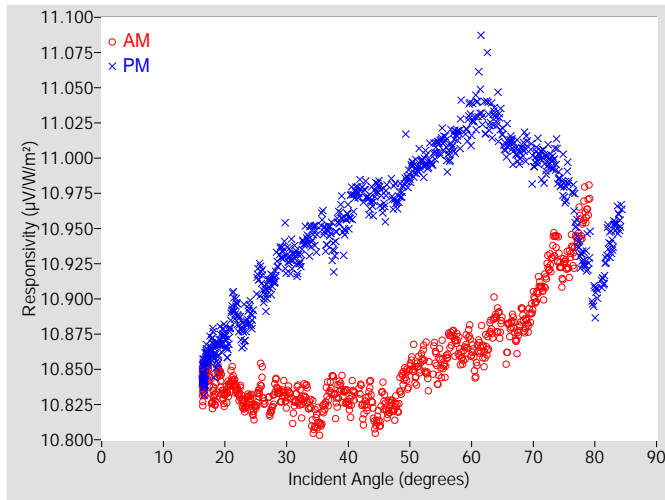


Figure 2. Responsivity vs Local Standard Time

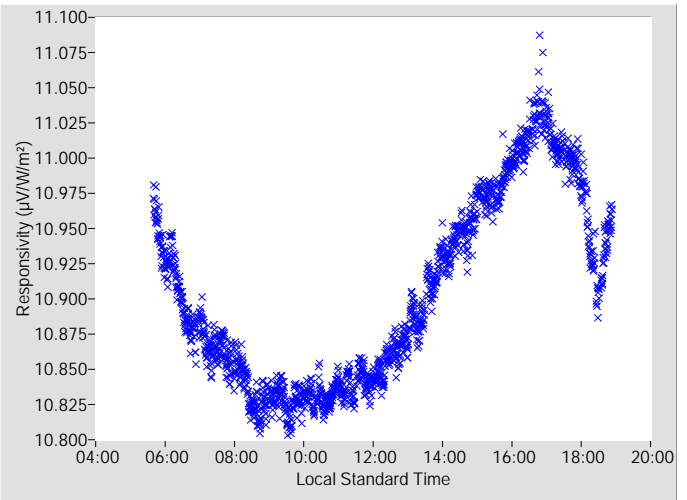


Table 2. Calibration Label Values

RS @ 45° (μV/W/m²) ‡	U95 (%) †	Tilt / Azm
10.896	+1.85 / -1.37	0.0° / 0.0°

† Valid incident angle range: 30.0° to 60.0°

‡ Estimated thermal offset error during calibration = -2.0000 W/m²

Table 3. Instrument Responsivity (RS) and Calibration Uncertainty (U95)

Inc. Angle†	AM			PM			Inc. Angle†	AM			PM		
	RS (μV/W/m²)	U95 ± (%)	Azm. Angle‡	RS (μV/W/m²)	U95 ± (%)	Azm. Angle‡		RS (μV/W/m²)	U95 ± (%)	Azm. Angle‡	RS (μV/W/m²)	U95 ± (%)	Azm. Angle‡
0	N/A	N/A	N/A	N/A	N/A	N/A	46	10.824	0.55	95.25	10.970	0.54	265.15
2	N/A	N/A	N/A	N/A	N/A	N/A	48	10.826	0.57	93.42	10.969	0.53	266.92
4	N/A	N/A	N/A	N/A	N/A	N/A	50	10.850	0.57	91.71	10.990	0.56	268.69
6	N/A	N/A	N/A	N/A	N/A	N/A	52	10.860	0.59	90.01	10.995	0.55	270.35
8	N/A	N/A	N/A	N/A	N/A	N/A	54	10.860	0.61	88.35	11.005	0.56	272.00
10	N/A	N/A	N/A	N/A	N/A	N/A	56	10.861	0.62	86.73	11.002	0.59	273.59
12	N/A	N/A	N/A	N/A	N/A	N/A	58	10.863	0.64	85.18	11.021	0.62	275.16
14	N/A	N/A	N/A	N/A	N/A	N/A	60	10.867	0.67	83.63	11.027	0.64	276.68
16	N/A	N/A	N/A	N/A	N/A	N/A	62	10.863	0.70	82.09	11.026	0.71	278.23
18	10.830	0.48	152.29	10.865	0.48	207.17	64	10.885	0.74	80.56	11.031	0.69	279.79
20	10.831	0.52	142.35	10.872	0.48	219.25	66	10.875	0.79	79.05	11.013	0.72	281.28
22	10.834	0.51	134.08	10.890	0.49	227.25	68	10.888	0.84	77.51	11.002	0.76	282.82
24	10.830	0.49	127.80	10.889	0.48	233.21	70	10.898	0.92	75.97	10.996	0.84	284.32
26	10.841	0.51	122.72	10.914	0.49	238.22	72	10.915	0.98	74.51	10.994	0.89	285.88
28	10.833	0.50	118.49	10.915	0.49	242.38	74	10.933	1.08	72.98	10.994	0.98	287.42
30	10.830	0.50	114.71	10.933	0.50	246.01	76	10.931	1.20	71.39	10.984	N/A	288.82
32	10.831	0.51	111.42	10.926	0.49	249.20	78	10.952	1.36	69.80	10.929	1.25	290.63
34	10.821	0.52	108.49	10.945	0.49	252.04	80	N/A	N/A	N/A	10.902	1.50	292.28
36	10.821	0.52	105.90	10.952	0.50	254.60	82	N/A	N/A	N/A	10.938	1.83	293.95
38	10.826	0.52	103.48	10.945	0.55	257.00	84	N/A	N/A	N/A	10.956	2.39	295.67
40	10.827	0.52	101.22	10.958	0.54	259.19	86	N/A	N/A	N/A	N/A	N/A	N/A
42	10.832	0.53	99.12	10.979	0.51	261.26	88	N/A	N/A	N/A	N/A	N/A	N/A
44	10.821	0.55	97.14	10.970	0.52	263.23	90	N/A	N/A	N/A	N/A	N/A	N/A

† Angle of incidence (degrees)

‡ Average azimuth angle for ±0.3° of incidence angle

N/A - Not Available

# Effective Net Infrared Corrected Calibration Results

## 010034 Kipp & Zonen CM22

Figure 3. Responsivity vs Incident Angle

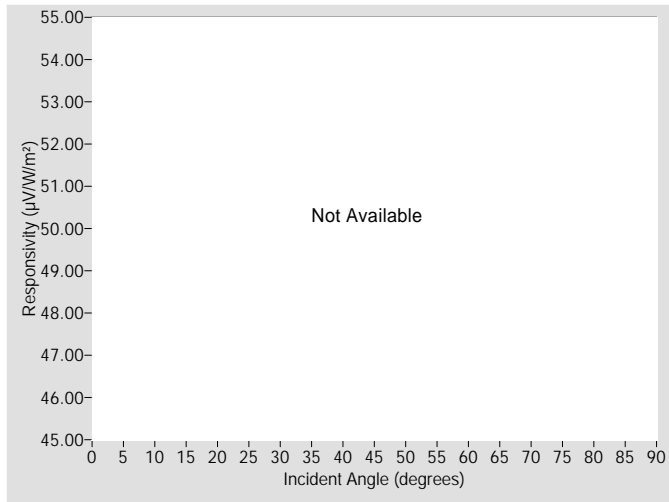


Figure 4. Responsivity vs Local Standard Time

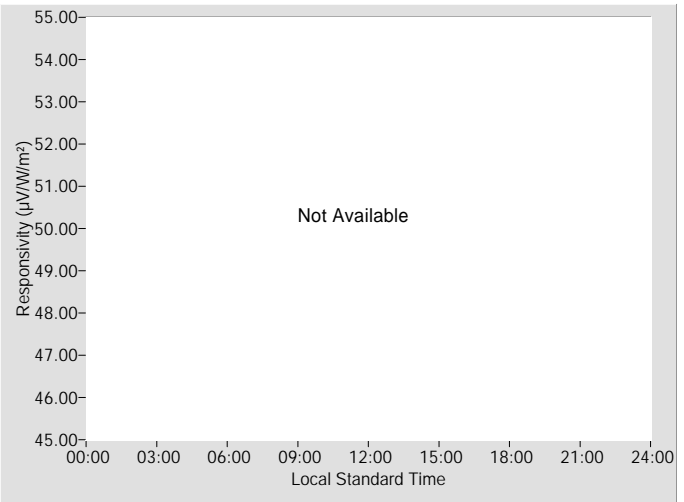


Table 4. Net IR Corrected Calibration Label Values

RSc @ 45° (µV/W/m²) ‡	U95 (%) †	Tilt / Azm
N/A	N/A	0.0° / 0.0°

† Valid incident angle range: N/A

‡ RSnet = N/A

Table 5. Net IR Corrected Instrument Responsivity (RS) and Calibration Uncertainty (U95)

Inc. Angle†	AM			PM			Inc. Angle†	AM			PM		
	RSc (µV/W/m²)	U95 ± (%)	Azm. Angle‡	RSc (µV/W/m²)	U95 ± (%)	Azm. Angle‡		RSc (µV/W/m²)	U95 ± (%)	Azm. Angle‡	RSc (µV/W/m²)	U95 ± (%)	Azm. Angle‡
0	N/A	N/A	N/A	N/A	N/A	N/A	46	N/A	N/A	N/A	N/A	N/A	N/A
2	N/A	N/A	N/A	N/A	N/A	N/A	48	N/A	N/A	N/A	N/A	N/A	N/A
4	N/A	N/A	N/A	N/A	N/A	N/A	50	N/A	N/A	N/A	N/A	N/A	N/A
6	N/A	N/A	N/A	N/A	N/A	N/A	52	N/A	N/A	N/A	N/A	N/A	N/A
8	N/A	N/A	N/A	N/A	N/A	N/A	54	N/A	N/A	N/A	N/A	N/A	N/A
10	N/A	N/A	N/A	N/A	N/A	N/A	56	N/A	N/A	N/A	N/A	N/A	N/A
12	N/A	N/A	N/A	N/A	N/A	N/A	58	N/A	N/A	N/A	N/A	N/A	N/A
14	N/A	N/A	N/A	N/A	N/A	N/A	60	N/A	N/A	N/A	N/A	N/A	N/A
16	N/A	N/A	N/A	N/A	N/A	N/A	62	N/A	N/A	N/A	N/A	N/A	N/A
18	N/A	N/A	N/A	N/A	N/A	N/A	64	N/A	N/A	N/A	N/A	N/A	N/A
20	N/A	N/A	N/A	N/A	N/A	N/A	66	N/A	N/A	N/A	N/A	N/A	N/A
22	N/A	N/A	N/A	N/A	N/A	N/A	68	N/A	N/A	N/A	N/A	N/A	N/A
24	N/A	N/A	N/A	N/A	N/A	N/A	70	N/A	N/A	N/A	N/A	N/A	N/A
26	N/A	N/A	N/A	N/A	N/A	N/A	72	N/A	N/A	N/A	N/A	N/A	N/A
28	N/A	N/A	N/A	N/A	N/A	N/A	74	N/A	N/A	N/A	N/A	N/A	N/A
30	N/A	N/A	N/A	N/A	N/A	N/A	76	N/A	N/A	N/A	N/A	N/A	N/A
32	N/A	N/A	N/A	N/A	N/A	N/A	78	N/A	N/A	N/A	N/A	N/A	N/A
34	N/A	N/A	N/A	N/A	N/A	N/A	80	N/A	N/A	N/A	N/A	N/A	N/A
36	N/A	N/A	N/A	N/A	N/A	N/A	82	N/A	N/A	N/A	N/A	N/A	N/A
38	N/A	N/A	N/A	N/A	N/A	N/A	84	N/A	N/A	N/A	N/A	N/A	N/A
40	N/A	N/A	N/A	N/A	N/A	N/A	86	N/A	N/A	N/A	N/A	N/A	N/A
42	N/A	N/A	N/A	N/A	N/A	N/A	88	N/A	N/A	N/A	N/A	N/A	N/A
44	N/A	N/A	N/A	N/A	N/A	N/A	90	N/A	N/A	N/A	N/A	N/A	N/A

† Angle of incidence (degrees)

‡ Average azimuth angle for ±0.3° of incidence angle

N/A - Not Available

# Suggested Methods of Applying Calibration Results

## 010034 Kipp & Zonen CM22

Listed below are the results for the methods documented in "Improved Methods for Broadband Outdoor Radiometer Calibration (BORCAL)," Wilcox et al., Proceedings of the ARM Science Team Meeting, St. Petersburg, Florida, April 2002. Computing the net infrared corrected solar irradiance is documented in "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error during Outdoor Calibration using the Component Sum Method," Reda et al., Journal of Atmospheric and Oceanic Technology V. 22 (10), pp. 1531-1540, October 2005.

In all cases, the solar irradiance is calculated from the instrument responsivity using one of these equations:

$$IRR = V / RS \quad [1]$$

$$IRR (corr.) = (V - W_{net} * RS_{net}) / RS_c \quad [2]$$

where,

$IRR$  = solar irradiance (Watts per square meter),

$V$  = radiometer output voltage (microvolts),

$RS$  = responsivity of the radiometer ( $\mu V/W/m^2$ ),

$IRR (corr.)$  = effective net infrared corrected solar irradiance ( $W/m^2$ ),

$W_{net}$  = effective net infrared measured by pyrgeometer ( $W/m^2$ ),

$RS_{net}$  = pyranometer net infrared response ( $\mu V/W/m^2$ ), see Table 4,

$RS_c$  = effective net infrared corrected responsivity ( $\mu V/W/m^2$ ).

**1. Two-degree Responsivities:** Responsivities are obtained from Certificate Table 3 or 5. See Note 1 on next page.

**2. AM and PM Responsivity Functions:** See Note 1 on next page.

Figure 1. Responsivity Function

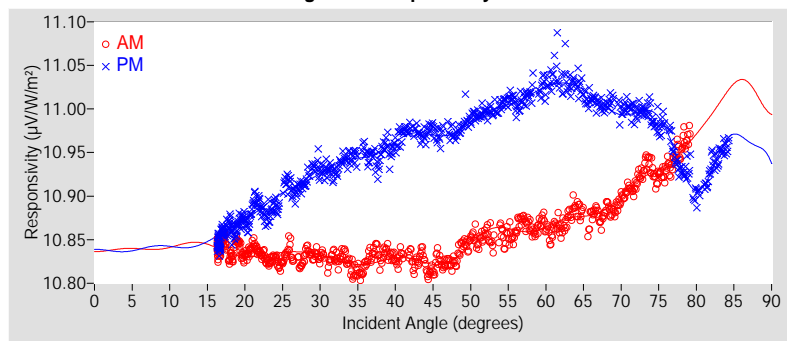
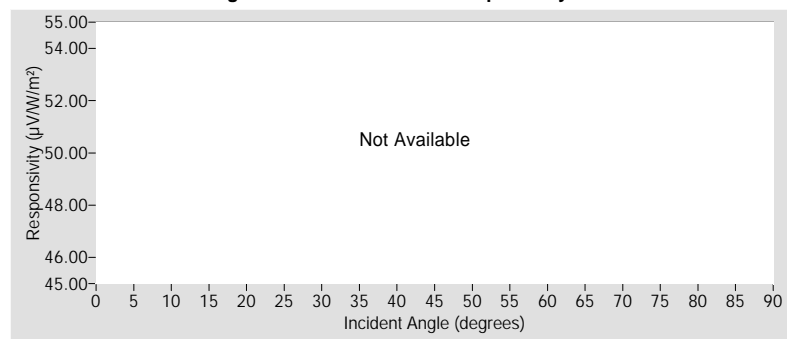


Figure 2. Net IR Corrected Responsivity Function



$$RS (am) = \sum_{i=0}^n a_i \cdot \cos^i(I) \quad [3]$$

$$RS (pm) = \sum_{j=0}^m b_j \cdot \cos^j(I)$$

where the coefficients  $a_i$  and  $b_j$  are available upon request.

The quality of the function fit to data is shown in Figure 1 and 2.

Table 1. Function Validity

	AM	PM
Uncertainty U95 (%)	±0.98	±0.98
R <sup>2</sup>	0.9999999	0.9999998
Valid incidence angle range	16.3° to 79.1°	16.3° to 84.3°
Net IR corr. uncert. U95 (%)	N/A	N/A
Net IR corrected R <sup>2</sup>	N/A	N/A
Corr. valid inc. angle range	N/A	N/A

**3. Nine-degree Bin Responsivity:** See Note 1 on next page.

Table 2. Nine-degree responsivities

Inc. Angle	Responsivity						Net IR Corr. Responsivity					
	AM		PM		Combined		AM		PM		Combined	
	RS ( $\mu V/W/m^2$ )	U95 (%)	RS ( $\mu V/W/m^2$ )	U95 (%)	RS ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)
0-9	10.839	*	10.839	*	10.839	*	N/A	N/A	N/A	N/A	N/A	N/A
9-18	10.843	*	10.846	*	10.845	*	N/A	N/A	N/A	N/A	N/A	N/A
18-27	10.833	±0.98	10.887	±1.01	10.860	±1.12	N/A	N/A	N/A	N/A	N/A	N/A
27-36	10.829	±0.99	10.931	±1.00	10.880	±1.27	N/A	N/A	N/A	N/A	N/A	N/A
36-45	10.826	±0.99	10.961	±0.99	10.894	±1.39	N/A	N/A	N/A	N/A	N/A	N/A
45-54	10.841	±1.00	10.982	±1.00	10.912	±1.53	N/A	N/A	N/A	N/A	N/A	N/A
54-63	10.864	±0.99	11.017	±0.99	10.941	±1.48	N/A	N/A	N/A	N/A	N/A	N/A
63-72	10.887	±1.00	11.009	±1.00	10.948	±1.40	N/A	N/A	N/A	N/A	N/A	N/A
72-81	10.942	*	10.961	±1.07	10.951	*	N/A	N/A	N/A	N/A	N/A	N/A
81-90	11.012	*	10.952	*	10.982	*	N/A	N/A	N/A	N/A	N/A	N/A

\* The responsivity is based on extrapolated data and the corresponding uncertainty is undefined.

#### 4. The Single Responsivities: See Note 1 below.

**Table 3. Single Responsivities**

Responsivity Characterization	RS ( $\mu\text{V/W/m}^2$ )	U95 † (%)
45°	10.896	+1.85 / -1.37
45° - 55°	10.915	$\pm 1.29$
Composite	10.883	+1.67 / -1.14
45° (Net IR Corr.)	N/A	N/A
45° - 55° (Net IR Corr.)	N/A	N/A
Composite (Net IR Corr.)	N/A	N/A

† Valid incident angle ranges:

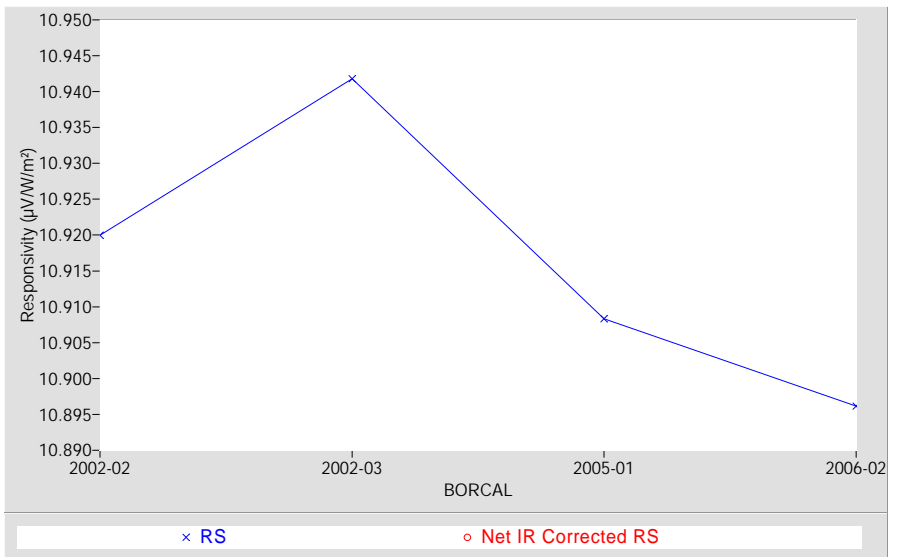
45°: 30.0° to 60.0°

45° - 55°: 45.0° to 55.0°

Composite: 16.3° to 79.1°

The instrument responsivity at  $I = 45^\circ$  may be used to monitor instrument stability. The instrument's history at  $I = 45^\circ$  is shown in Figure 2.

**Figure 2. History of instrument at  $I = 45^\circ$**



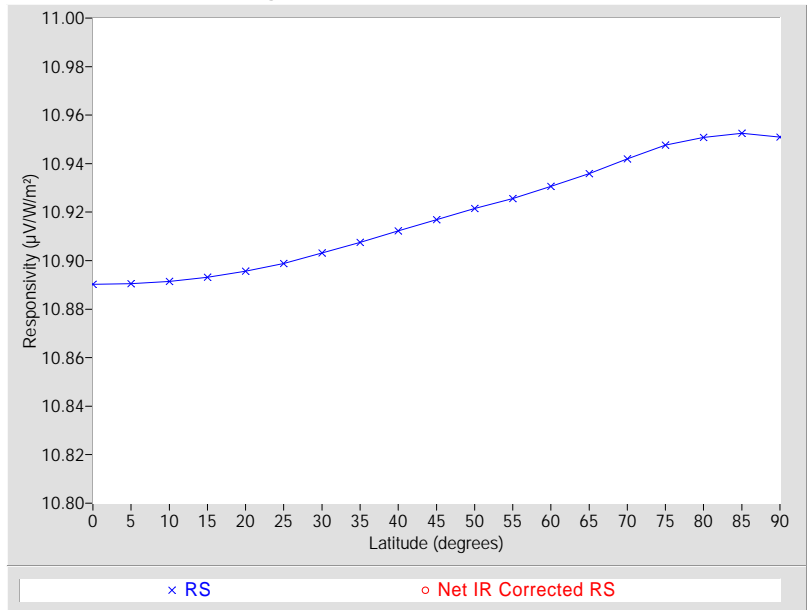
#### 5. Latitude Optimized Responsivity: See Note 1 below.

**Table 4. Latitude Optimized Responsivities**

Latitude	RS ( $\mu\text{V/W/m}^2$ )	Error estimate* (%)	RSc ( $\mu\text{V/W/m}^2$ )		Error estimate* (%)	
			Net IR Corr.	Net IR Corr.	Net IR Corr.	Net IR Corr.
0	10.890	+1.65 / -1.17	N/A	N/A	N/A	N/A
5	10.890	+1.64 / -1.17	N/A	N/A	N/A	N/A
10	10.891	+1.64 / -1.18	N/A	N/A	N/A	N/A
15	10.893	+1.62 / -1.18	N/A	N/A	N/A	N/A
20	10.896	+1.61 / -1.20	N/A	N/A	N/A	N/A
25	10.899	+1.58 / -1.21	N/A	N/A	N/A	N/A
30	10.903	+1.55 / -1.24	N/A	N/A	N/A	N/A
35	10.908	+1.52 / -1.26	N/A	N/A	N/A	N/A
40	10.912	+1.49 / -1.29	N/A	N/A	N/A	N/A
45	10.917	+1.46 / -1.32	N/A	N/A	N/A	N/A
50	10.922	+1.42 / -1.34	N/A	N/A	N/A	N/A
55	10.926	+1.40 / -1.37	N/A	N/A	N/A	N/A
60	10.931	+1.36 / -1.40	N/A	N/A	N/A	N/A
65	10.936	+1.33 / -1.44	N/A	N/A	N/A	N/A
70	10.942	+1.29 / -1.48	N/A	N/A	N/A	N/A
75	10.948	+1.26 / -1.31	N/A	N/A	N/A	N/A
80	10.951	+1.24 / -1.29	N/A	N/A	N/A	N/A
85	10.952	+1.23 / -1.25	N/A	N/A	N/A	N/A
90	10.951	+1.24 / -1.19	N/A	N/A	N/A	N/A

\* Uncertainty is undefined

**Figure 3. Latitude Optimized Responsivities**



#### Application of the responsivities and uncertainties:

The responsivities above are applied according to equation [1]:

##### Example

Instrument responsivity (RS) =  $7.34 \mu\text{V/W/m}^2 \pm 2.7\%$

Instrument output voltage (V) =  $0.00624 \text{ V}$  ( $6240 \mu\text{V}$ )

Irradiance (IRR) =  $V / RS = 6240 / 7.34 = 850.1 \text{ W/m}^2 \pm 2.7\%$

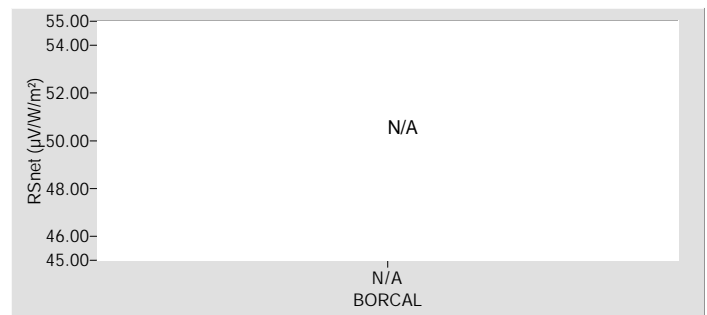
Thus, at the 95% confidence level, the irradiance lies between 827.1 and 873.1  $\text{W/m}^2$

##### Note 1:

All above methods, in conjunction with knowledge of the net infrared and sky irradiance distribution, may be used to determine the effective instrument responsivity with less uncertainties.

#### Instrument's Effective Net Infrared History (RSnet):

**Figure 4. Instrument's RSnet History**



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate

**Test Instrument:** Pyranometer **Manufacturer:** Kipp & Zonen  
**Model:** CM6B **Serial Number:** 015189  
**Calibration Date:** 6/17/2006 **Due Date:** 6/17/2007  
**Customer:** NREL-SRRL-BMS **Calibration Site Parameters:** see Ancillary Data  
**Environmental Conditions:** Outdoors, under natural sunlight (see Ancillary Data)  
**Data Acquisition Dates:** 6/11-12, 6/17

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppeley Absolute Cavity Radiometer Model HF, S/N 31104	03/14/2006	03/14/2007
Diffuse Irradiance †	Eppeley Black and White Pyranometer Model 8-48, S/N 32858	04/05/2006	04/05/2007
Diffuse Irradiance †	Eppeley Black and White Pyranometer Model 8-48, S/N 32871	04/05/2006	04/05/2007
Data Acquisition ‡	NREL Data Proof Scanner System Model RAP-DAQ, S/N 2005-998	11/22/2005	11/22/2006
Data Acquisition ‡	NREL Data Proof Scanner System Model RAP-DAQ, S/N 2005-999	11/22/2005	11/22/2006

† Traceable to the World Radiometric Reference

‡ Traceable to the National Institute of Standards and Technology

**Number of pages of certificate:** 4

**Calibration Procedure:** [1] Myers, D., Stoffel, T., Reda, I., Wilcox, S., and Andreas, A., 2002, "Recent Progress in Reducing the Uncertainty in and Improving Pyranometer Calibrations." Journal of Solar Energy Engineering, vol. 124, pp. 44-50. The American Society of Mechanical Engineers, Transactions of the ASME.  
[2] "Improved Methods for Broadband Outdoor Radiometer Calibration (BORCAL)," Wilcox, S., Andreas, A., Reda, I., and Myers, D., Proceedings of the ARM Science Team Meeting, St. Petersburg, Florida, April 2002. Available upon request.

This calibration certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval by the calibration facility. Calibration certificates without signatures are not valid.

**Calibrated by:** Ibrahim Reda and Steve Wilcox

**Certified by:**

-----  
Afshin M. Andreas

Title: Scientist II

Date: -----

**Quality Assured by:**

-----  
Daryl R. Myers

Title: Senior Scientist II

Date: -----



# Calibration Results

## 015189 Kipp & Zonen CM6B

Figure 1. Responsivity vs Incident Angle

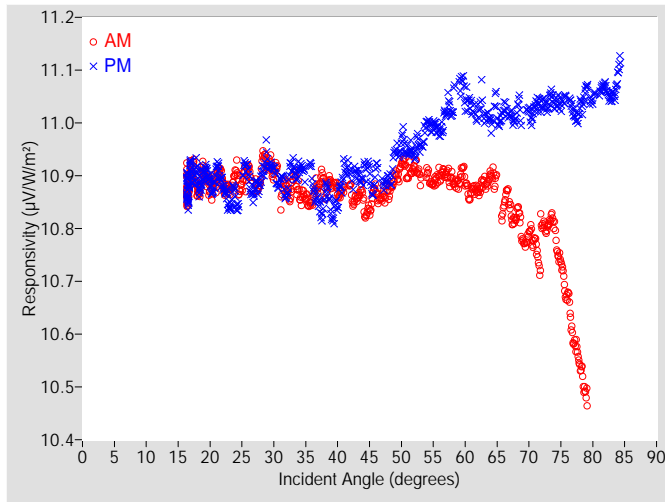


Figure 2. Responsivity vs Local Standard Time

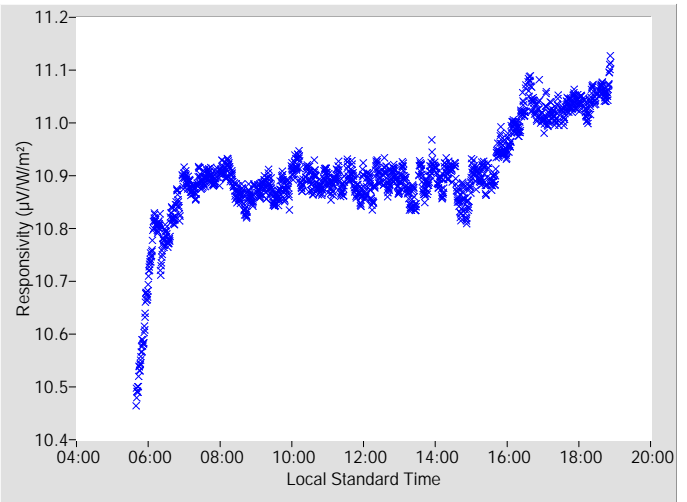


Table 2. Calibration Label Values

RS @ 45° (µV/W/m²) ‡	U95 (%) †	Tilt / Azm
10.871	+2.53 / -1.09	0.0° / 0.0°

† Valid incident angle range: 30.0° to 60.0°

‡ Estimated thermal offset error during calibration = -10.000 W/m²

Table 3. Instrument Responsivity (RS) and Calibration Uncertainty (U95)

Inc. Angle†	AM			PM			Inc. Angle†	AM			PM		
	RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡	RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡		RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡	RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡
0	N/A	N/A	N/A	N/A	N/A	N/A	46	10.870	0.60	95.25	10.909	0.59	265.15
2	N/A	N/A	N/A	N/A	N/A	N/A	48	10.872	0.60	93.43	10.897	0.63	266.88
4	N/A	N/A	N/A	N/A	N/A	N/A	50	10.922	0.59	91.67	10.963	0.59	268.65
6	N/A	N/A	N/A	N/A	N/A	N/A	52	10.916	0.61	90.01	10.939	0.59	270.35
8	N/A	N/A	N/A	N/A	N/A	N/A	54	10.907	0.61	88.32	10.997	0.61	271.97
10	N/A	N/A	N/A	N/A	N/A	N/A	56	10.900	0.63	86.74	10.984	0.62	273.56
12	N/A	N/A	N/A	N/A	N/A	N/A	58	10.893	0.65	85.19	11.032	0.65	275.16
14	N/A	N/A	N/A	N/A	N/A	N/A	60	10.895	0.71	83.63	11.053	0.69	276.69
16	N/A	N/A	N/A	N/A	N/A	N/A	62	10.872	0.70	82.09	11.016	0.73	278.19
18	10.877	0.55	152.31	10.903	0.56	207.19	64	10.900	0.75	80.57	11.001	0.76	279.71
20	10.879	0.57	142.37	10.884	0.52	219.26	66	10.836	0.82	79.05	11.025	0.74	281.25
22	10.887	0.54	134.09	10.882	0.62	227.26	68	10.825	0.89	77.51	11.014	0.80	282.78
24	10.907	0.57	127.81	10.856	0.51	233.22	70	10.791	0.92	75.98	11.020	0.84	284.32
26	10.910	0.54	122.64	10.902	0.59	238.23	72	10.794	1.10	74.51	11.033	0.89	285.90
28	10.903	0.60	118.50	10.898	0.66	242.39	74	10.804	1.14	72.99	11.037	0.98	287.42
30	10.906	0.54	114.72	10.912	0.52	246.04	76	10.673	1.39	71.40	11.050	N/A	288.83
32	10.880	0.56	111.43	10.864	0.57	249.14	78	10.542	1.45	69.80	11.031	1.28	290.64
34	10.868	0.57	108.49	10.916	0.52	251.98	80	N/A	N/A	N/A	11.047	1.48	292.23
36	10.852	0.55	105.90	10.895	0.62	254.61	82	N/A	N/A	N/A	11.068	1.82	293.95
38	10.875	0.56	103.49	10.867	0.59	257.00	84	N/A	N/A	N/A	11.097	2.42	295.68
40	10.870	0.52	101.22	10.853	0.75	259.19	86	N/A	N/A	N/A	N/A	N/A	N/A
42	10.874	0.55	99.08	10.906	0.56	261.21	88	N/A	N/A	N/A	N/A	N/A	N/A
44	10.856	0.60	97.15	10.901	0.55	263.23	90	N/A	N/A	N/A	N/A	N/A	N/A

† Angle of incidence (degrees)

‡ Average azimuth angle for ±0.3° of incidence angle

N/A - Not Available

# Effective Net Infrared Corrected Calibration Results

## 015189 Kipp & Zonen CM6B

Figure 3. Responsivity vs Incident Angle

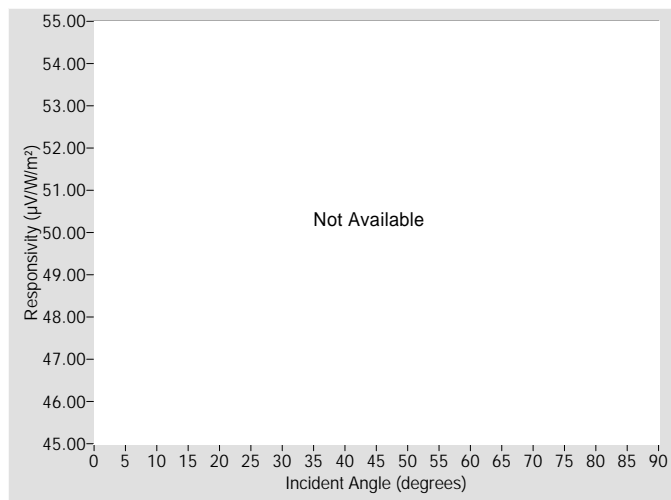


Figure 4. Responsivity vs Local Standard Time

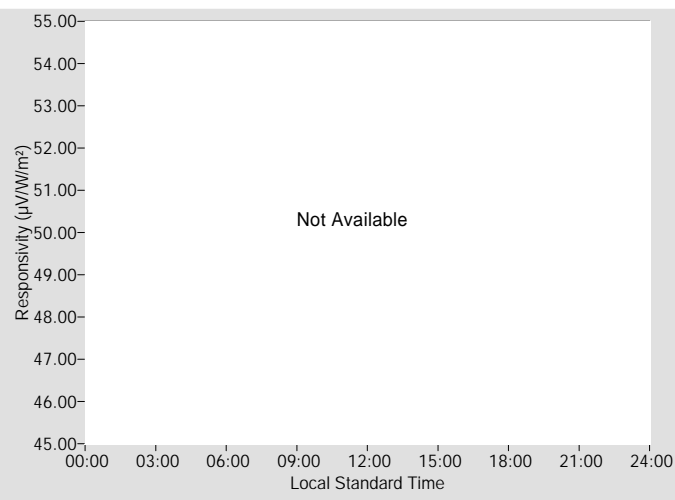


Table 4. Net IR Corrected Calibration Label Values

RSc @ 45° (μV/W/m²) ‡	U95 (%) †	Tilt / Azm
N/A	N/A	0.0° / 0.0°

† Valid incident angle range: N/A

‡ RSnet = N/A

Table 5. Net IR Corrected Instrument Responsivity (RS) and Calibration Uncertainty (U95)

Inc. Angle†	AM			PM			Inc. Angle†	AM			PM		
	RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡	RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡		RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡	RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡
0	N/A	N/A	N/A	N/A	N/A	N/A	46	N/A	N/A	N/A	N/A	N/A	N/A
2	N/A	N/A	N/A	N/A	N/A	N/A	48	N/A	N/A	N/A	N/A	N/A	N/A
4	N/A	N/A	N/A	N/A	N/A	N/A	50	N/A	N/A	N/A	N/A	N/A	N/A
6	N/A	N/A	N/A	N/A	N/A	N/A	52	N/A	N/A	N/A	N/A	N/A	N/A
8	N/A	N/A	N/A	N/A	N/A	N/A	54	N/A	N/A	N/A	N/A	N/A	N/A
10	N/A	N/A	N/A	N/A	N/A	N/A	56	N/A	N/A	N/A	N/A	N/A	N/A
12	N/A	N/A	N/A	N/A	N/A	N/A	58	N/A	N/A	N/A	N/A	N/A	N/A
14	N/A	N/A	N/A	N/A	N/A	N/A	60	N/A	N/A	N/A	N/A	N/A	N/A
16	N/A	N/A	N/A	N/A	N/A	N/A	62	N/A	N/A	N/A	N/A	N/A	N/A
18	N/A	N/A	N/A	N/A	N/A	N/A	64	N/A	N/A	N/A	N/A	N/A	N/A
20	N/A	N/A	N/A	N/A	N/A	N/A	66	N/A	N/A	N/A	N/A	N/A	N/A
22	N/A	N/A	N/A	N/A	N/A	N/A	68	N/A	N/A	N/A	N/A	N/A	N/A
24	N/A	N/A	N/A	N/A	N/A	N/A	70	N/A	N/A	N/A	N/A	N/A	N/A
26	N/A	N/A	N/A	N/A	N/A	N/A	72	N/A	N/A	N/A	N/A	N/A	N/A
28	N/A	N/A	N/A	N/A	N/A	N/A	74	N/A	N/A	N/A	N/A	N/A	N/A
30	N/A	N/A	N/A	N/A	N/A	N/A	76	N/A	N/A	N/A	N/A	N/A	N/A
32	N/A	N/A	N/A	N/A	N/A	N/A	78	N/A	N/A	N/A	N/A	N/A	N/A
34	N/A	N/A	N/A	N/A	N/A	N/A	80	N/A	N/A	N/A	N/A	N/A	N/A
36	N/A	N/A	N/A	N/A	N/A	N/A	82	N/A	N/A	N/A	N/A	N/A	N/A
38	N/A	N/A	N/A	N/A	N/A	N/A	84	N/A	N/A	N/A	N/A	N/A	N/A
40	N/A	N/A	N/A	N/A	N/A	N/A	86	N/A	N/A	N/A	N/A	N/A	N/A
42	N/A	N/A	N/A	N/A	N/A	N/A	88	N/A	N/A	N/A	N/A	N/A	N/A
44	N/A	N/A	N/A	N/A	N/A	N/A	90	N/A	N/A	N/A	N/A	N/A	N/A

† Angle of incidence (degrees)

‡ Average azimuth angle for ±0.3° of incidence angle

N/A - Not Available

## Suggested Methods of Applying Calibration Results

### 015189 Kipp & Zonen CM6B

Listed below are the results for the methods documented in "Improved Methods for Broadband Outdoor Radiometer Calibration (BORCAL)," Wilcox et al., Proceedings of the ARM Science Team Meeting, St. Petersburg, Florida, April 2002. Computing the net infrared corrected solar irradiance is documented in "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error during Outdoor Calibration using the Component Sum Method," Reda et al., Journal of Atmospheric and Oceanic Technology V. 22 (10), pp. 1531-1540, October 2005.

In all cases, the solar irradiance is calculated from the instrument responsivity using one of these equations:

$$IRR = V / RS \quad [1]$$

$$IRR (corr.) = (V - W_{net} * RS_{net}) / RS_{sc} \quad [2]$$

where,

$IRR$  = solar irradiance (Watts per square meter),

$V$  = radiometer output voltage (microvolts),

$RS$  = responsivity of the radiometer ( $\mu V/W/m^2$ ),

$IRR (corr.)$  = effective net infrared corrected solar irradiance ( $W/m^2$ ),

$W_{net}$  = effective net infrared measured by pyrgeometer ( $W/m^2$ ),

$RS_{net}$  = pyranometer net infrared response ( $\mu V/W/m^2$ ), see Table 4,

$RS_{sc}$  = effective net infrared corrected responsivity ( $\mu V/W/m^2$ ).

**1. Two-degree Responsivities:** Responsivities are obtained from Certificate Table 3 or 5. See Note 1 on next page.

**2. AM and PM Responsivity Functions:** See Note 1 on next page.

Figure 1. Responsivity Function

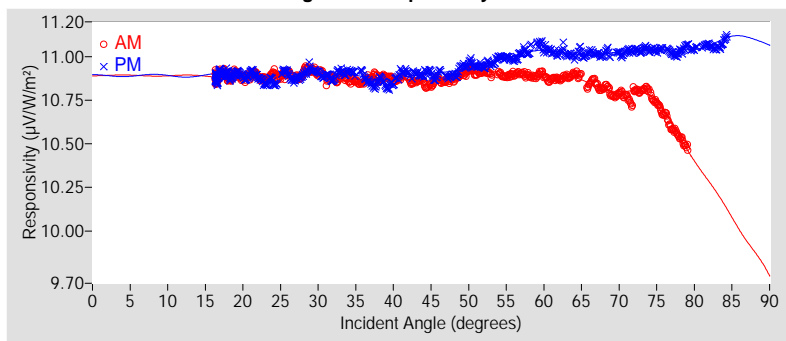


Figure 2. Net IR Corrected Responsivity Function



$$RS (am) = \sum_{i=0}^n a_i \cdot \cos^i(I) \quad [3]$$

$$RS (pm) = \sum_{j=0}^m b_j \cdot \cos^j(I)$$

where the coefficients  $a_i$  and  $b_j$  are available upon request.

The quality of the function fit to data is shown in Figure 1 and 2.

Table 1. Function Validity

	AM	PM
Uncertainty U95 (%)	±1.03	±1.03
R <sup>2</sup>	0.9999995	0.9999988
Valid incidence angle range	16.3° to 79.1°	16.3° to 84.3°
Net IR corr. uncert. U95 (%)	N/A	N/A
Net IR corrected R <sup>2</sup>	N/A	N/A
Corr. valid inc. angle range	N/A	N/A

**3. Nine-degree Bin Responsivity:** See Note 1 on next page.

Table 2. Nine-degree responsivities

Inc. Angle	Responsivity						Net IR Corr. Responsivity					
	AM		PM		Combined		AM		PM		Combined	
	RS ( $\mu V/W/m^2$ )	U95 (%)	RS ( $\mu V/W/m^2$ )	U95 (%)	RS ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)
0-9	10.892	*	10.892	*	10.892	*	N/A	N/A	N/A	N/A	N/A	N/A
9-18	10.889	*	10.892	*	10.891	*	N/A	N/A	N/A	N/A	N/A	N/A
18-27	10.892	±1.04	10.883	±1.04	10.888	±1.06	N/A	N/A	N/A	N/A	N/A	N/A
27-36	10.887	±1.06	10.896	±1.03	10.892	±1.09	N/A	N/A	N/A	N/A	N/A	N/A
36-45	10.867	±1.03	10.882	±1.04	10.875	±1.07	N/A	N/A	N/A	N/A	N/A	N/A
45-54	10.895	±1.06	10.933	±1.08	10.914	±1.27	N/A	N/A	N/A	N/A	N/A	N/A
54-63	10.895	±1.04	11.018	±1.06	10.957	±1.42	N/A	N/A	N/A	N/A	N/A	N/A
63-72	10.834	±1.11	11.017	±1.04	10.926	±1.82	N/A	N/A	N/A	N/A	N/A	N/A
72-81	10.638	*	11.040	±1.03	10.839	*	N/A	N/A	N/A	N/A	N/A	N/A
81-90	10.046	*	11.092	*	10.569	*	N/A	N/A	N/A	N/A	N/A	N/A

\* The responsivity is based on extrapolated data and the corresponding uncertainty is undefined.

#### 4. The Single Responsivities: See Note 1 below.

**Table 3. Single Responsivities**

Responsivity Characterization	RS ( $\mu\text{V/W/m}^2$ )	U95 † (%)
45°	10.871	+2.53 / -1.09
45° - 55°	10.919	$\pm 1.19$
Composite	10.894	+2.19 / -6.90
45° (Net IR Corr.)	N/A	N/A
45° - 55° (Net IR Corr.)	N/A	N/A
Composite (Net IR Corr.)	N/A	N/A

† Valid incident angle ranges:

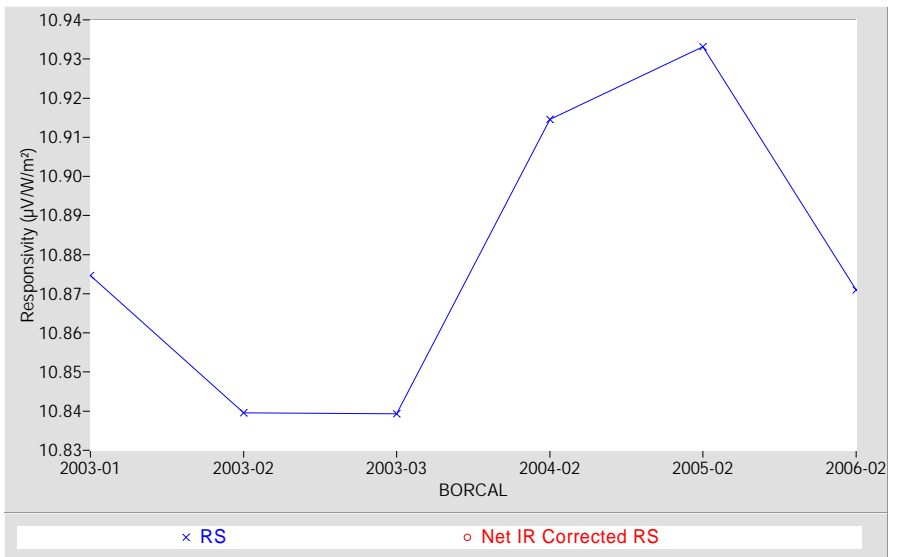
45°: 30.0° to 60.0°

45° - 55°: 45.0° to 55.0°

Composite: 16.3° to 79.1°

The instrument responsivity at  $I = 45^\circ$  may be used to monitor instrument stability. The instrument's history at  $I = 45^\circ$  is shown in Figure 2.

**Figure 2. History of instrument at  $I = 45^\circ$**



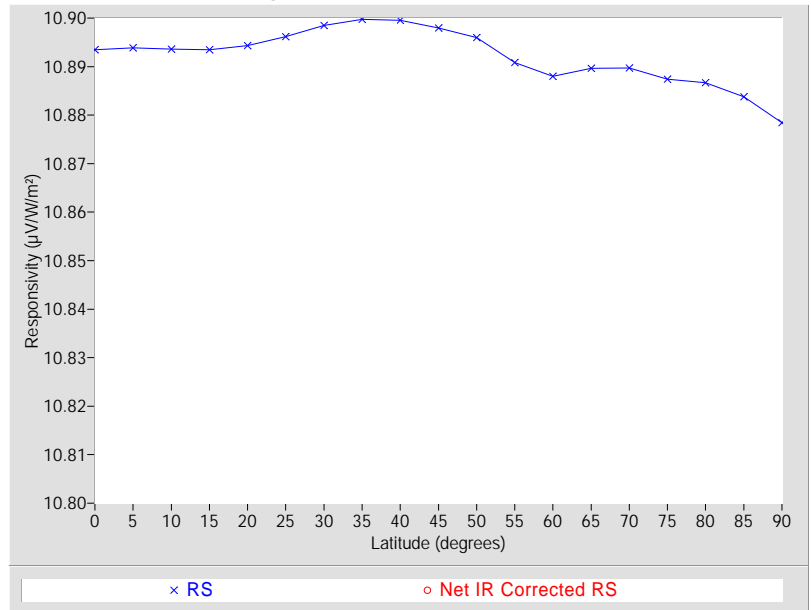
#### 5. Latitude Optimized Responsivity: See Note 1 below.

**Table 4. Latitude Optimized Responsivities**

Latitude	RS ( $\mu\text{V/W/m}^2$ )	Error estimate* (%)	RSc ( $\mu\text{V/W/m}^2$ )	Error estimate* (%)
			Net IR Corr.	Net IR Corr.
0	10.893	+2.32 / -9.91	N/A	N/A
5	10.894	+2.32 / -9.91	N/A	N/A
10	10.894	+2.32 / -9.91	N/A	N/A
15	10.893	+2.32 / -9.91	N/A	N/A
20	10.894	+2.32 / -9.92	N/A	N/A
25	10.896	+2.30 / -9.93	N/A	N/A
30	10.898	+2.28 / -9.95	N/A	N/A
35	10.900	+2.27 / -9.96	N/A	N/A
40	10.900	+2.27 / -9.96	N/A	N/A
45	10.898	+2.29 / -9.95	N/A	N/A
50	10.896	+2.30 / -9.93	N/A	N/A
55	10.891	+2.35 / -9.89	N/A	N/A
60	10.888	+2.37 / -9.86	N/A	N/A
65	10.890	+2.35 / -9.88	N/A	N/A
70	10.890	+2.35 / -9.88	N/A	N/A
75	10.887	+2.37 / -9.86	N/A	N/A
80	10.887	+2.38 / -9.85	N/A	N/A
85	10.884	+2.40 / -9.83	N/A	N/A
90	10.878	+2.45 / -9.79	N/A	N/A

\* Uncertainty is undefined

**Figure 3. Latitude Optimized Responsivities**



#### Application of the responsivities and uncertainties:

The responsivities above are applied according to equation [1]:

##### Example

Instrument responsivity (RS) =  $7.34 \mu\text{V/W/m}^2 \pm 2.7\%$

Instrument output voltage (V) =  $0.00624 \text{ V}$  ( $6240 \mu\text{V}$ )

Irradiance (IRR) =  $V / RS = 6240 / 7.34 = 850.1 \text{ W/m}^2 \pm 2.7\%$

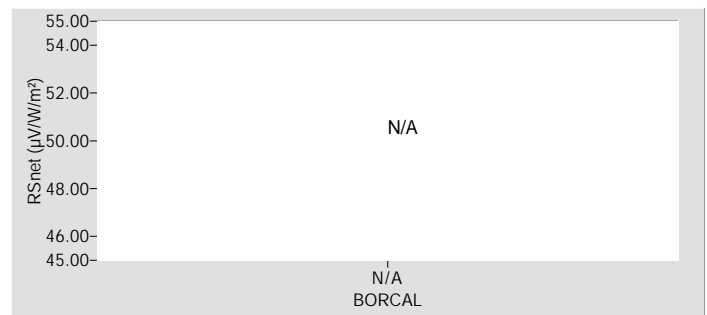
Thus, at the 95% confidence level, the irradiance lies between 827.1 and 873.1  $\text{W/m}^2$

##### Note 1:

All above methods, in conjunction with knowledge of the net infrared and sky irradiance distribution, may be used to determine the effective instrument responsivity with less uncertainties.

#### Instrument's Effective Net Infrared History (RSnet):

**Figure 4. Instrument's RSnet History**



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate

**Test Instrument:** Precision Spectral Pyranometer      **Manufacturer:** Eppley

**Model:** PSP      **Serial Number:** 18035F3

**Calibration Date:** 6/17/2006      **Due Date:** 6/17/2007

**Customer:** NREL-SRRL-BMS      **Calibration Site Parameters:** see Ancillary Data

**Environmental Conditions:** Outdoors, under natural sunlight (see Ancillary Data)

**Data Acquisition Dates:** 6/11-12, 6/17

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 31104	03/14/2006	03/14/2007
Diffuse Irradiance †	Eppley Black and White Pyranometer Model 8-48, S/N 32858	04/05/2006	04/05/2007
Diffuse Irradiance †	Eppley Black and White Pyranometer Model 8-48, S/N 32871	04/05/2006	04/05/2007
Data Acquisition ‡	NREL Data Proof Scanner System Model RAP-DAQ, S/N 2005-998	11/22/2005	11/22/2006
Data Acquisition ‡	NREL Data Proof Scanner System Model RAP-DAQ, S/N 2005-999	11/22/2005	11/22/2006

† Traceable to the World Radiometric Reference

‡ Traceable to the National Institute of Standards and Technology

**Number of pages of certificate:** 4

**Calibration Procedure:** [1] Myers, D., Stoffel, T., Reda, I., Wilcox, S., and Andreas, A., 2002, "Recent Progress in Reducing the Uncertainty in and Improving Pyranometer Calibrations." Journal of Solar Energy Engineering, vol. 124, pp. 44-50. The American Society of Mechanical Engineers, Transactions of the ASME.  
[2] "Improved Methods for Broadband Outdoor Radiometer Calibration (BORCAL)," Wilcox, S., Andreas, A., Reda, I., and Myers, D., Proceedings of the ARM Science Team Meeting, St. Petersburg, Florida, April 2002. Available upon request.

This calibration certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval by the calibration facility. Calibration certificates without signatures are not valid.

**Calibrated by:** Ibrahim Reda and Steve Wilcox

**Certified by:**

-----  
Afshin M. Andreas

Title: Scientist II

Date: -----

**Quality Assured by:**

-----  
Daryl R. Myers

Title: Senior Scientist II

Date: -----

# Calibration Results

## 18035F3 Eppley PSP

Figure 1. Responsivity vs Incident Angle

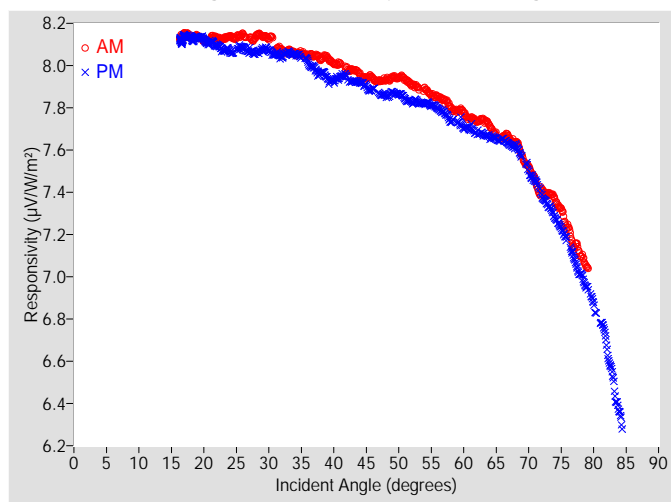


Figure 2. Responsivity vs Local Standard Time

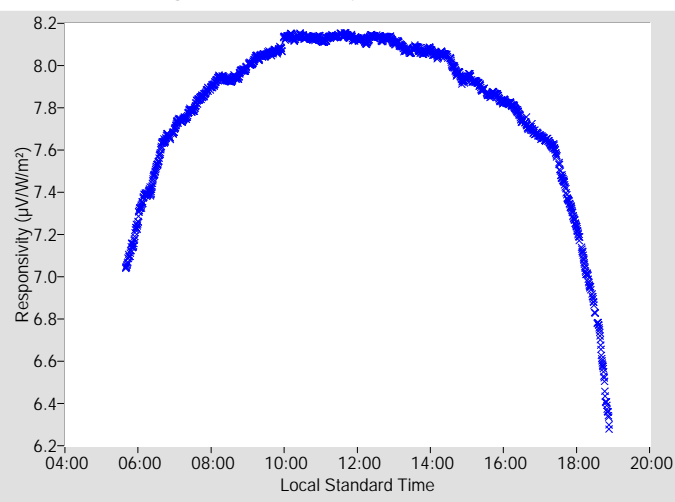


Table 2. Calibration Label Values

RS @ 45° (µV/W/m²) ‡	U95 (%) †	Tilt / Azm
7.9216	+3.26 / -3.26	0.0° / 0.0°

† Valid incident angle range: 30.0° to 60.0°

‡ Estimated thermal offset error during calibration = -20.000 W/m²

Table 3. Instrument Responsivity (RS) and Calibration Uncertainty (U95)

Inc. Angle†	AM			PM			Inc. Angle†	AM			PM		
	RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡	RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡		RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡	RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡
0	N/A	N/A	N/A	N/A	N/A	N/A	46	7.9413	0.58	95.27	7.8876	0.55	265.12
2	N/A	N/A	N/A	N/A	N/A	N/A	48	7.9347	0.56	93.45	7.8580	0.55	266.94
4	N/A	N/A	N/A	N/A	N/A	N/A	50	7.9430	0.58	91.69	7.8640	0.57	268.67
6	N/A	N/A	N/A	N/A	N/A	N/A	52	7.9087	0.62	89.99	7.8263	0.56	270.36
8	N/A	N/A	N/A	N/A	N/A	N/A	54	7.8875	0.62	88.33	7.8201	0.57	271.98
10	N/A	N/A	N/A	N/A	N/A	N/A	56	7.8526	0.64	86.75	7.7960	0.62	273.57
12	N/A	N/A	N/A	N/A	N/A	N/A	58	7.8014	0.74	85.16	7.7379	0.66	275.14
14	N/A	N/A	N/A	N/A	N/A	N/A	60	7.7809	0.74	83.64	7.7050	0.73	276.68
16	N/A	N/A	N/A	N/A	N/A	N/A	62	7.7379	0.70	82.10	7.6828	0.72	278.20
18	8.1378	0.47	152.38	8.1316	0.49	207.25	64	7.7149	0.86	80.54	7.6605	0.70	279.75
20	8.1209	0.53	142.42	8.1242	0.52	219.18	66	7.6629	0.80	79.03	7.6499	0.73	281.28
22	8.1310	0.51	134.02	8.0944	0.56	227.19	68	7.6378	0.97	77.52	7.6147	0.86	282.81
24	8.1386	0.50	127.75	8.0675	0.49	233.36	70	7.5215	1.16	75.99	7.4994	1.02	284.34
26	8.1455	0.51	122.68	8.0861	0.53	238.26	72	7.4062	1.09	74.51	7.3850	1.19	285.87
28	8.1377	0.54	118.45	8.0617	0.51	242.34	74	7.3683	1.18	72.96	7.2815	1.18	287.44
30	8.1302	0.51	114.82	8.0724	0.53	245.92	76	7.2333	1.73	71.37	7.1797	1.43	288.83
32	8.0750	0.53	111.38	8.0418	0.52	249.16	78	7.1040	1.58	69.78	7.0107	1.58	290.61
34	8.0606	0.53	108.51	8.0533	0.52	252.00	80	N/A	N/A	N/A	6.8637	1.74	292.28
36	8.0479	0.52	105.87	8.0181	0.57	254.58	82	N/A	N/A	N/A	6.6752	2.63	293.93
38	8.0297	0.53	103.45	7.9640	0.56	256.97	84	N/A	N/A	N/A	6.3527	3.08	295.69
40	8.0097	0.55	101.24	7.9287	0.54	259.21	86	N/A	N/A	N/A	N/A	N/A	N/A
42	7.9849	0.56	99.10	7.9483	0.57	261.23	88	N/A	N/A	N/A	N/A	N/A	N/A
44	7.9552	0.59	97.11	7.9189	0.54	263.29	90	N/A	N/A	N/A	N/A	N/A	N/A

† Angle of incidence (degrees)

‡ Average azimuth angle for ±0.3° of incidence angle

N/A - Not Available

# Effective Net Infrared Corrected Calibration Results

## 18035F3 Eppley PSP

Figure 3. Responsivity vs Incident Angle

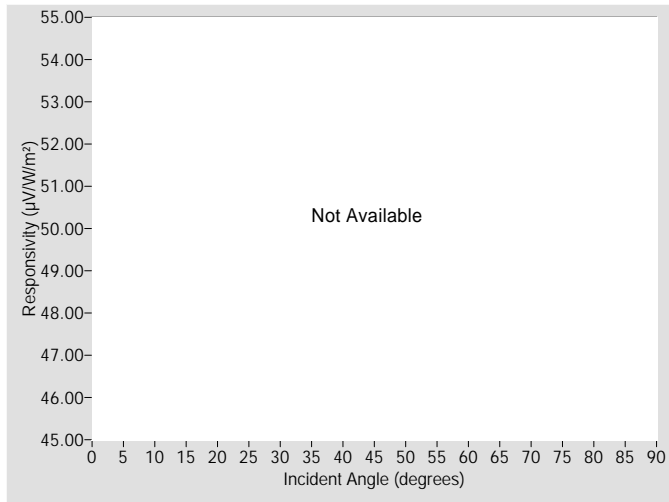


Figure 4. Responsivity vs Local Standard Time

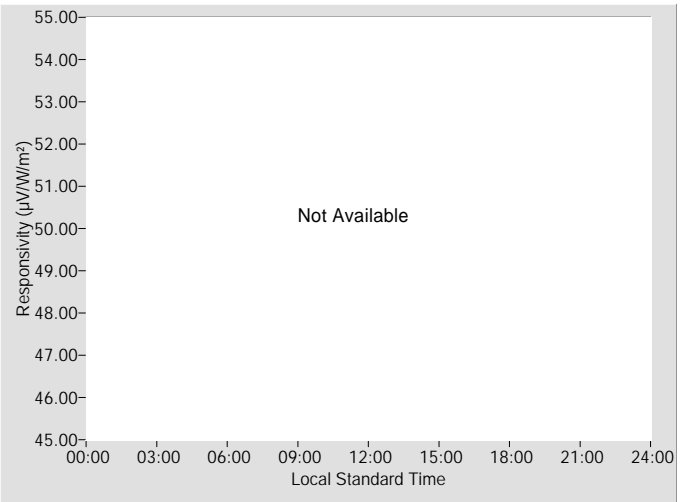


Table 4. Net IR Corrected Calibration Label Values

RSc @ 45° (μV/W/m²) ‡	U95 (%) †	Tilt / Azm
N/A	N/A	0.0° / 0.0°

† Valid incident angle range: N/A

‡ RSnet = N/A

Table 5. Net IR Corrected Instrument Responsivity (RS) and Calibration Uncertainty (U95)

Inc. Angle†	AM			PM			Inc. Angle†	AM			PM		
	RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡	RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡		RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡	RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡
0	N/A	N/A	N/A	N/A	N/A	N/A	46	N/A	N/A	N/A	N/A	N/A	N/A
2	N/A	N/A	N/A	N/A	N/A	N/A	48	N/A	N/A	N/A	N/A	N/A	N/A
4	N/A	N/A	N/A	N/A	N/A	N/A	50	N/A	N/A	N/A	N/A	N/A	N/A
6	N/A	N/A	N/A	N/A	N/A	N/A	52	N/A	N/A	N/A	N/A	N/A	N/A
8	N/A	N/A	N/A	N/A	N/A	N/A	54	N/A	N/A	N/A	N/A	N/A	N/A
10	N/A	N/A	N/A	N/A	N/A	N/A	56	N/A	N/A	N/A	N/A	N/A	N/A
12	N/A	N/A	N/A	N/A	N/A	N/A	58	N/A	N/A	N/A	N/A	N/A	N/A
14	N/A	N/A	N/A	N/A	N/A	N/A	60	N/A	N/A	N/A	N/A	N/A	N/A
16	N/A	N/A	N/A	N/A	N/A	N/A	62	N/A	N/A	N/A	N/A	N/A	N/A
18	N/A	N/A	N/A	N/A	N/A	N/A	64	N/A	N/A	N/A	N/A	N/A	N/A
20	N/A	N/A	N/A	N/A	N/A	N/A	66	N/A	N/A	N/A	N/A	N/A	N/A
22	N/A	N/A	N/A	N/A	N/A	N/A	68	N/A	N/A	N/A	N/A	N/A	N/A
24	N/A	N/A	N/A	N/A	N/A	N/A	70	N/A	N/A	N/A	N/A	N/A	N/A
26	N/A	N/A	N/A	N/A	N/A	N/A	72	N/A	N/A	N/A	N/A	N/A	N/A
28	N/A	N/A	N/A	N/A	N/A	N/A	74	N/A	N/A	N/A	N/A	N/A	N/A
30	N/A	N/A	N/A	N/A	N/A	N/A	76	N/A	N/A	N/A	N/A	N/A	N/A
32	N/A	N/A	N/A	N/A	N/A	N/A	78	N/A	N/A	N/A	N/A	N/A	N/A
34	N/A	N/A	N/A	N/A	N/A	N/A	80	N/A	N/A	N/A	N/A	N/A	N/A
36	N/A	N/A	N/A	N/A	N/A	N/A	82	N/A	N/A	N/A	N/A	N/A	N/A
38	N/A	N/A	N/A	N/A	N/A	N/A	84	N/A	N/A	N/A	N/A	N/A	N/A
40	N/A	N/A	N/A	N/A	N/A	N/A	86	N/A	N/A	N/A	N/A	N/A	N/A
42	N/A	N/A	N/A	N/A	N/A	N/A	88	N/A	N/A	N/A	N/A	N/A	N/A
44	N/A	N/A	N/A	N/A	N/A	N/A	90	N/A	N/A	N/A	N/A	N/A	N/A

† Angle of incidence (degrees)

‡ Average azimuth angle for ±0.3° of incidence angle

N/A - Not Available

## Suggested Methods of Applying Calibration Results

### 18035F3 Eppley PSP

Listed below are the results for the methods documented in "Improved Methods for Broadband Outdoor Radiometer Calibration (BORCAL)," Wilcox et al., Proceedings of the ARM Science Team Meeting, St. Petersburg, Florida, April 2002. Computing the net infrared corrected solar irradiance is documented in "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error during Outdoor Calibration using the Component Sum Method," Reda et al., Journal of Atmospheric and Oceanic Technology V. 22 (10), pp. 1531-1540, October 2005.

In all cases, the solar irradiance is calculated from the instrument responsivity using one of these equations:

$$IRR = V / RS \quad [1]$$

$$IRR (corr.) = (V - W_{net} * RS_{net}) / RS_c \quad [2]$$

where,

$IRR$  = solar irradiance (Watts per square meter),

$V$  = radiometer output voltage (microvolts),

$RS$  = responsivity of the radiometer ( $\mu V/W/m^2$ ),

$IRR (corr.)$  = effective net infrared corrected solar irradiance ( $W/m^2$ ),

$W_{net}$  = effective net infrared measured by pyrgeometer ( $W/m^2$ ),

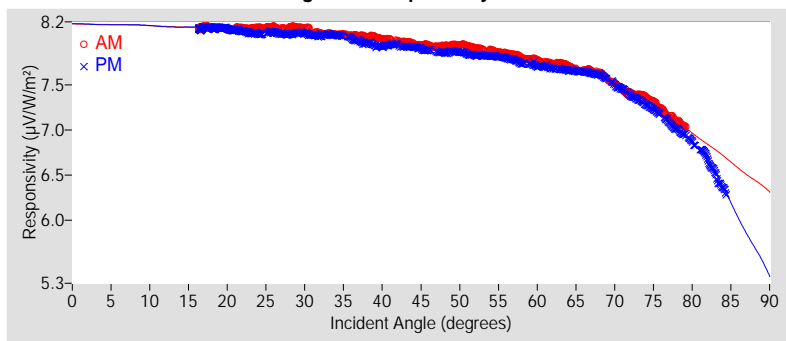
$RS_{net}$  = pyranometer net infrared response ( $\mu V/W/m^2$ ), see Table 4,

$RS_c$  = effective net infrared corrected responsivity ( $\mu V/W/m^2$ ).

**1. Two-degree Responsivities:** Responsivities are obtained from Certificate Table 3 or 5. See Note 1 on next page.

**2. AM and PM Responsivity Functions:** See Note 1 on next page.

Figure 1. Responsivity Function



$$RS (am) = \sum_{i=0}^n a_i \cdot \cos^i(I) \quad [3]$$

$$RS (pm) = \sum_{j=0}^m b_j \cdot \cos^j(I)$$

where the coefficients  $a_i$  and  $b_j$  are available upon request.

The quality of the function fit to data is shown in Figure 1 and 2.

Figure 2. Net IR Corrected Responsivity Function



Table 1. Function Validity

	AM	PM
Uncertainty U95 (%)	±1.28	±1.28
R <sup>2</sup>	0.9999990	0.9999986
Valid incidence angle range	16.3° to 79.1°	16.3° to 84.4°
Net IR corr. uncert. U95 (%)	N/A	N/A
Net IR corrected R <sup>2</sup>	N/A	N/A
Corr. valid inc. angle range	N/A	N/A

**3. Nine-degree Bin Responsivity:** See Note 1 on next page.

Table 2. Nine-degree responsivities

Inc. Angle	Responsivity						Net IR Corr. Responsivity					
	AM		PM		Combined		AM		PM		Combined	
	RS ( $\mu V/W/m^2$ )	U95 (%)	RS ( $\mu V/W/m^2$ )	U95 (%)	RS ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)
0-9	8.1708	*	8.1709	*	8.1709	*	N/A	N/A	N/A	N/A	N/A	N/A
9-18	8.1466	*	8.1468	*	8.1467	*	N/A	N/A	N/A	N/A	N/A	N/A
18-27	8.1339	±1.29	8.0972	±1.34	8.1156	±1.45	N/A	N/A	N/A	N/A	N/A	N/A
27-36	8.0979	±1.43	8.0555	±1.32	8.0767	±1.70	N/A	N/A	N/A	N/A	N/A	N/A
36-45	8.0030	±1.41	7.9500	±1.42	7.9765	±1.72	N/A	N/A	N/A	N/A	N/A	N/A
45-54	7.9299	±1.32	7.8592	±1.38	7.8946	±1.68	N/A	N/A	N/A	N/A	N/A	N/A
54-63	7.8066	±1.61	7.7423	±1.60	7.7745	±2.31	N/A	N/A	N/A	N/A	N/A	N/A
63-72	7.6205	±2.21	7.5929	±2.10	7.6067	±3.18	N/A	N/A	N/A	N/A	N/A	N/A
72-81	7.2065	*	7.1315	±4.21	7.1690	*	N/A	N/A	N/A	N/A	N/A	N/A
81-90	6.6125	*	6.1067	*	6.3596	*	N/A	N/A	N/A	N/A	N/A	N/A

\* The responsivity is based on extrapolated data and the corresponding uncertainty is undefined.



#### 4. The Single Responsivities: See Note 1 below.

**Table 3. Single Responsivities**

Responsivity Characterization	RS ( $\mu\text{V/W/m}^2$ )	U95 † (%)
45°	7.9216	+3.26 / -3.26
45° - 55°	7.8874	$\pm 1.55$
Composite	7.9726	+2.54 / -20.14
45° (Net IR Corr.)	N/A	N/A
45° - 55° (Net IR Corr.)	N/A	N/A
Composite (Net IR Corr.)	N/A	N/A

† Valid incident angle ranges:

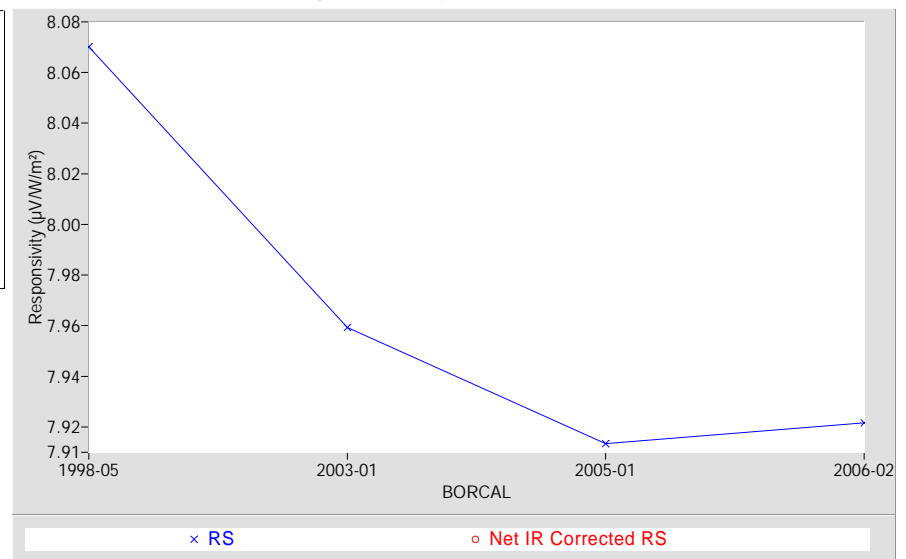
45°: 30.0° to 60.0°

45° - 55°: 45.0° to 55.0°

Composite: 16.3° to 79.1°

The instrument responsivity at  $I = 45^\circ$  may be used to monitor instrument stability. The instrument's history at  $I = 45^\circ$  is shown in Figure 2.

**Figure 2. History of instrument at  $I = 45^\circ$**



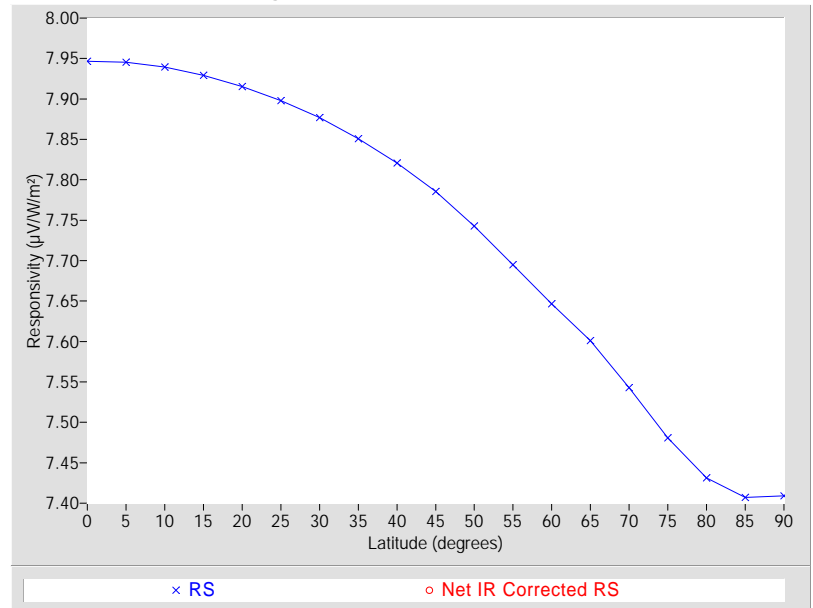
#### 5. Latitude Optimized Responsivity: See Note 1 below.

**Table 4. Latitude Optimized Responsivities**

Latitude	RS ( $\mu\text{V/W/m}^2$ )	Error estimate* (%)	RSc ( $\mu\text{V/W/m}^2$ )	Error estimate* (%)
			Net IR Corr.	Net IR Corr.
0	7.9466	+3.20 / -30.06	N/A	N/A
5	7.9453	+3.22 / -30.05	N/A	N/A
10	7.9394	+3.29 / -30.00	N/A	N/A
15	7.9291	+3.41 / -29.91	N/A	N/A
20	7.9152	+3.58 / -29.78	N/A	N/A
25	7.8979	+3.77 / -29.63	N/A	N/A
30	7.8770	+3.92 / -29.44	N/A	N/A
35	7.8509	+4.06 / -29.21	N/A	N/A
40	7.8208	+4.36 / -28.94	N/A	N/A
45	7.7857	+4.81 / -28.62	N/A	N/A
50	7.7429	+5.37 / -28.22	N/A	N/A
55	7.6950	+5.45 / -27.77	N/A	N/A
60	7.6465	+5.34 / -27.32	N/A	N/A
65	7.6012	+5.38 / -26.88	N/A	N/A
70	7.5429	+5.43 / -26.32	N/A	N/A
75	7.4806	+6.11 / -25.71	N/A	N/A
80	7.4311	+5.77 / -25.21	N/A	N/A
85	7.4073	+4.85 / -24.97	N/A	N/A
90	7.4089	+3.87 / -24.99	N/A	N/A

\* Uncertainty is undefined

**Figure 3. Latitude Optimized Responsivities**



#### Application of the responsivities and uncertainties:

The responsivities above are applied according to equation [1]:

##### Example

Instrument responsivity (RS) =  $7.34 \mu\text{V/W/m}^2 \pm 2.7\%$

Instrument output voltage (V) =  $0.00624 \text{ V}$  ( $6240 \mu\text{V}$ )

Irradiance (IRR) =  $V / RS = 6240 / 7.34 = 850.1 \text{ W/m}^2 \pm 2.7\%$

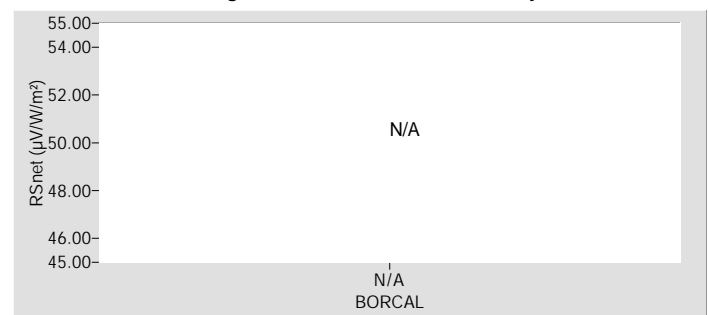
Thus, at the 95% confidence level, the irradiance lies between 827.1 and 873.1  $\text{W/m}^2$

##### Note 1:

All above methods, in conjunction with knowledge of the net infrared and sky irradiance distribution, may be used to determine the effective instrument responsivity with less uncertainties.

#### Instrument's Effective Net Infrared History (RSnet):

**Figure 4. Instrument's RSnet History**



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

#### Calibration Certificate

**Test Instrument:** Precision Spectral Pyranometer      **Manufacturer:** Eppley

**Model:** PSP      **Serial Number:** 25819F3

**Calibration Date:** 6/17/2006      **Due Date:** 6/17/2007

**Customer:** NREL-SRRL-BMS      **Calibration Site Parameters:** see Ancillary Data

**Environmental Conditions:** Outdoors, under natural sunlight (see Ancillary Data)

**Data Acquisition Dates:** 6/11-12, 6/17

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 31104	03/14/2006	03/14/2007
Diffuse Irradiance †	Eppley Black and White Pyranometer Model 8-48, S/N 32858	04/05/2006	04/05/2007
Diffuse Irradiance †	Eppley Black and White Pyranometer Model 8-48, S/N 32871	04/05/2006	04/05/2007
Data Acquisition ‡	NREL Data Proof Scanner System Model RAP-DAQ, S/N 2005-998	11/22/2005	11/22/2006
Data Acquisition ‡	NREL Data Proof Scanner System Model RAP-DAQ, S/N 2005-999	11/22/2005	11/22/2006

† Traceable to the World Radiometric Reference

‡ Traceable to the National Institute of Standards and Technology

**Number of pages of certificate:** 4

**Calibration Procedure:** [1] Myers, D., Stoffel, T., Reda, I., Wilcox, S., and Andreas, A., 2002, "Recent Progress in Reducing the Uncertainty in and Improving Pyranometer Calibrations." Journal of Solar Energy Engineering, vol. 124, pp. 44-50. The American Society of Mechanical Engineers, Transactions of the ASME.  
[2] "Improved Methods for Broadband Outdoor Radiometer Calibration (BORCAL)," Wilcox, S., Andreas, A., Reda, I., and Myers, D., Proceedings of the ARM Science Team Meeting, St. Petersburg, Florida, April 2002. Available upon request.

This calibration certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval by the calibration facility. Calibration certificates without signatures are not valid.

**Calibrated by:** Ibrahim Reda and Steve Wilcox

**Certified by:**

-----  
Afshin M. Andreas

Title: Scientist II

Date: -----

**Quality Assured by:**

-----  
Daryl R. Myers

Title: Senior Scientist II

Date: -----

# Calibration Results

## 25819F3 Eppley PSP

Figure 1. Responsivity vs Incident Angle

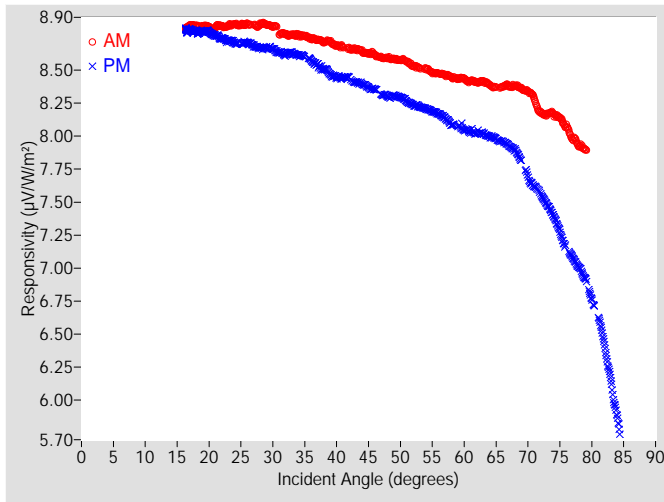


Figure 2. Responsivity vs Local Standard Time

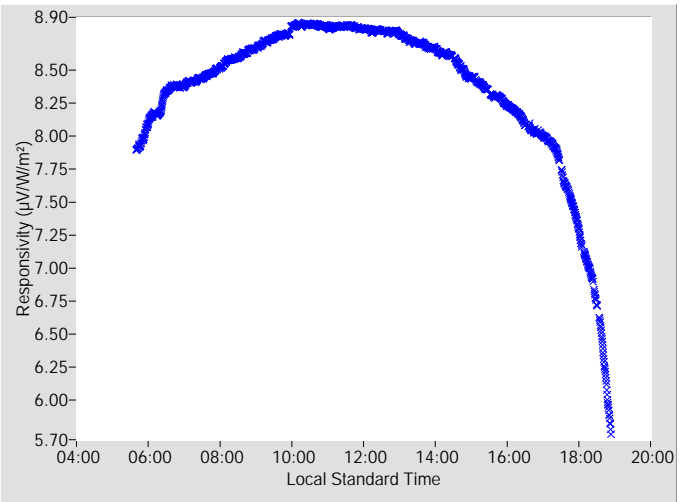


Table 2. Calibration Label Values

RS @ 45° (µV/W/m²) ‡	U95 (%) †	Tilt / Azm
8.4979	+4.51 / -5.82	0.0° / 0.0°

† Valid incident angle range: 30.0° to 60.0°

‡ Estimated thermal offset error during calibration = -20.000 W/m²

Table 3. Instrument Responsivity (RS) and Calibration Uncertainty (U95)

Inc. Angle†	AM			PM			Inc. Angle†	AM			PM		
	RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡	RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡		RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡	RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡
0	N/A	N/A	N/A	N/A	N/A	N/A	46	8.6167	0.59	95.27	8.3534	0.60	265.12
2	N/A	N/A	N/A	N/A	N/A	N/A	48	8.5936	0.56	93.45	8.3001	0.56	266.94
4	N/A	N/A	N/A	N/A	N/A	N/A	50	8.5766	0.57	91.69	8.2927	0.60	268.67
6	N/A	N/A	N/A	N/A	N/A	N/A	52	8.5305	0.64	89.99	8.2343	0.58	270.36
8	N/A	N/A	N/A	N/A	N/A	N/A	54	8.5103	0.62	88.33	8.2063	0.60	271.98
10	N/A	N/A	N/A	N/A	N/A	N/A	56	8.4748	0.62	86.75	8.1677	0.65	273.57
12	N/A	N/A	N/A	N/A	N/A	N/A	58	8.4454	0.66	85.16	8.0891	0.66	275.14
14	N/A	N/A	N/A	N/A	N/A	N/A	60	8.4364	0.69	83.64	8.0463	0.76	276.68
16	N/A	N/A	N/A	N/A	N/A	N/A	62	8.4086	0.70	82.10	8.0250	0.69	278.20
18	8.8353	0.47	152.38	8.7916	0.49	207.25	64	8.3871	0.79	80.54	7.9942	0.72	279.75
20	8.8245	0.54	142.42	8.7893	0.53	219.18	66	8.3746	0.80	79.03	7.9581	0.76	281.28
22	8.8338	0.50	134.02	8.7386	0.56	227.19	68	8.3795	0.84	77.52	7.8885	1.00	282.81
24	8.8480	0.50	127.75	8.7056	0.49	233.36	70	8.3394	1.01	75.99	7.6882	1.19	284.34
26	8.8490	0.50	122.68	8.7056	0.53	238.26	72	8.1801	1.22	74.51	7.5578	1.25	285.87
28	8.8452	0.53	118.45	8.6682	0.49	242.34	74	8.1684	1.10	72.96	7.3913	1.57	287.44
30	8.8310	0.51	114.82	8.6610	0.55	245.92	76	8.0706	1.57	71.37	7.1664	1.68	288.83
32	8.7727	0.51	111.38	8.6183	0.51	249.16	78	7.9306	1.48	69.78	7.0047	1.66	290.61
34	8.7665	0.51	108.51	8.6119	0.52	252.00	80	N/A	N/A	N/A	6.7561	2.11	292.28
36	8.7386	0.53	105.87	8.5750	0.58	254.58	82	N/A	N/A	N/A	6.4132	4.01	293.93
38	8.7119	0.52	103.45	8.5066	0.67	256.97	84	N/A	N/A	N/A	5.8660	4.19	295.69
40	8.6876	0.59	101.24	8.4461	0.53	259.21	86	N/A	N/A	N/A	N/A	N/A	N/A
42	8.6626	0.53	99.10	8.4426	0.57	261.23	88	N/A	N/A	N/A	N/A	N/A	N/A
44	8.6407	0.58	97.11	8.3937	0.56	263.29	90	N/A	N/A	N/A	N/A	N/A	N/A

† Angle of incidence (degrees)

‡ Average azimuth angle for ±0.3° of incidence angle

N/A - Not Available

# Effective Net Infrared Corrected Calibration Results

## 25819F3 Eppley PSP

Figure 3. Responsivity vs Incident Angle

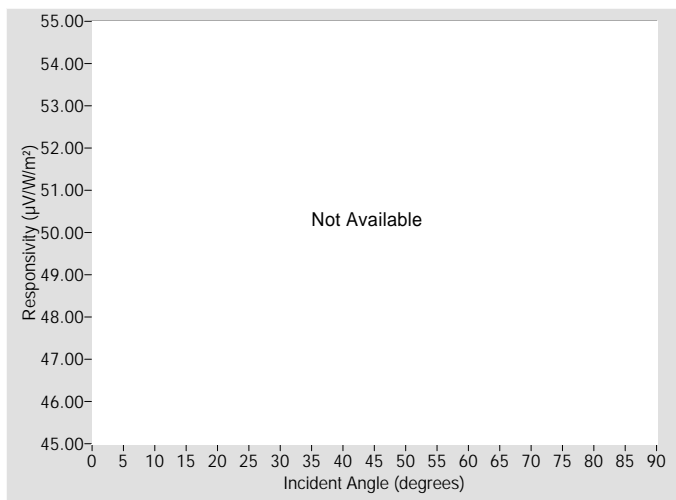


Figure 4. Responsivity vs Local Standard Time

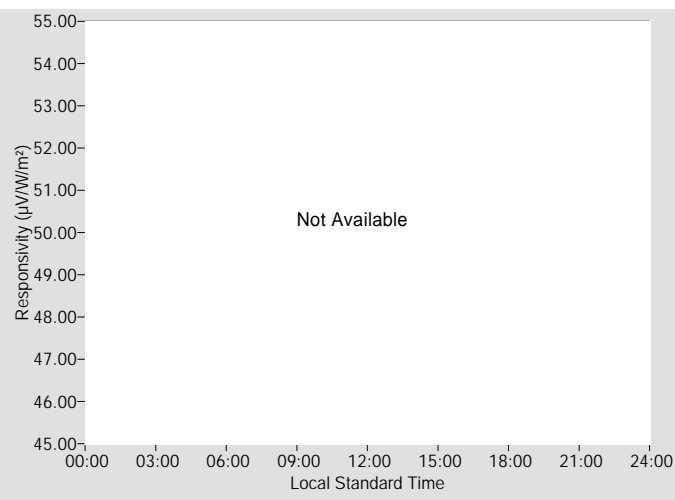


Table 4. Net IR Corrected Calibration Label Values

RSc @ 45° (μV/W/m²) ‡	U95 (%) †	Tilt / Azm
N/A	N/A	0.0° / 0.0°

† Valid incident angle range: N/A

‡ RSnet = N/A

Table 5. Net IR Corrected Instrument Responsivity (RS) and Calibration Uncertainty (U95)

Inc. Angle†	AM			PM			Inc. Angle†	AM			PM		
	RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡	RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡		RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡	RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡
0	N/A	N/A	N/A	N/A	N/A	N/A	46	N/A	N/A	N/A	N/A	N/A	N/A
2	N/A	N/A	N/A	N/A	N/A	N/A	48	N/A	N/A	N/A	N/A	N/A	N/A
4	N/A	N/A	N/A	N/A	N/A	N/A	50	N/A	N/A	N/A	N/A	N/A	N/A
6	N/A	N/A	N/A	N/A	N/A	N/A	52	N/A	N/A	N/A	N/A	N/A	N/A
8	N/A	N/A	N/A	N/A	N/A	N/A	54	N/A	N/A	N/A	N/A	N/A	N/A
10	N/A	N/A	N/A	N/A	N/A	N/A	56	N/A	N/A	N/A	N/A	N/A	N/A
12	N/A	N/A	N/A	N/A	N/A	N/A	58	N/A	N/A	N/A	N/A	N/A	N/A
14	N/A	N/A	N/A	N/A	N/A	N/A	60	N/A	N/A	N/A	N/A	N/A	N/A
16	N/A	N/A	N/A	N/A	N/A	N/A	62	N/A	N/A	N/A	N/A	N/A	N/A
18	N/A	N/A	N/A	N/A	N/A	N/A	64	N/A	N/A	N/A	N/A	N/A	N/A
20	N/A	N/A	N/A	N/A	N/A	N/A	66	N/A	N/A	N/A	N/A	N/A	N/A
22	N/A	N/A	N/A	N/A	N/A	N/A	68	N/A	N/A	N/A	N/A	N/A	N/A
24	N/A	N/A	N/A	N/A	N/A	N/A	70	N/A	N/A	N/A	N/A	N/A	N/A
26	N/A	N/A	N/A	N/A	N/A	N/A	72	N/A	N/A	N/A	N/A	N/A	N/A
28	N/A	N/A	N/A	N/A	N/A	N/A	74	N/A	N/A	N/A	N/A	N/A	N/A
30	N/A	N/A	N/A	N/A	N/A	N/A	76	N/A	N/A	N/A	N/A	N/A	N/A
32	N/A	N/A	N/A	N/A	N/A	N/A	78	N/A	N/A	N/A	N/A	N/A	N/A
34	N/A	N/A	N/A	N/A	N/A	N/A	80	N/A	N/A	N/A	N/A	N/A	N/A
36	N/A	N/A	N/A	N/A	N/A	N/A	82	N/A	N/A	N/A	N/A	N/A	N/A
38	N/A	N/A	N/A	N/A	N/A	N/A	84	N/A	N/A	N/A	N/A	N/A	N/A
40	N/A	N/A	N/A	N/A	N/A	N/A	86	N/A	N/A	N/A	N/A	N/A	N/A
42	N/A	N/A	N/A	N/A	N/A	N/A	88	N/A	N/A	N/A	N/A	N/A	N/A
44	N/A	N/A	N/A	N/A	N/A	N/A	90	N/A	N/A	N/A	N/A	N/A	N/A

† Angle of incidence (degrees)

‡ Average azimuth angle for ±0.3° of incidence angle

N/A - Not Available

## Suggested Methods of Applying Calibration Results

### 25819F3 Eppley PSP

Listed below are the results for the methods documented in "Improved Methods for Broadband Outdoor Radiometer Calibration (BORCAL)," Wilcox et al., Proceedings of the ARM Science Team Meeting, St. Petersburg, Florida, April 2002. Computing the net infrared corrected solar irradiance is documented in "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error during Outdoor Calibration using the Component Sum Method," Reda et al., Journal of Atmospheric and Oceanic Technology V. 22 (10), pp. 1531-1540, October 2005.

In all cases, the solar irradiance is calculated from the instrument responsivity using one of these equations:

$$IRR = V / RS \quad [1]$$

$$IRR (corr.) = (V - W_{net} * RS_{net}) / RS_c \quad [2]$$

where,

$IRR$  = solar irradiance (Watts per square meter),

$V$  = radiometer output voltage (microvolts),

$RS$  = responsivity of the radiometer ( $\mu V/W/m^2$ ),

$IRR (corr.)$  = effective net infrared corrected solar irradiance ( $W/m^2$ ),

$W_{net}$  = effective net infrared measured by pyrgeometer ( $W/m^2$ ),

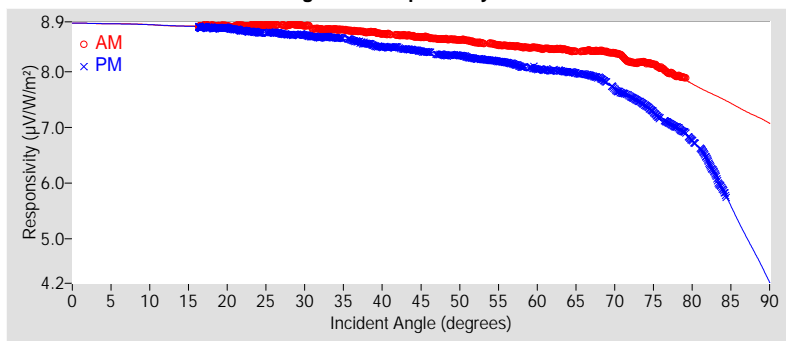
$RS_{net}$  = pyranometer net infrared response ( $\mu V/W/m^2$ ), see Table 4,

$RS_c$  = effective net infrared corrected responsivity ( $\mu V/W/m^2$ ).

**1. Two-degree Responsivities:** Responsivities are obtained from Certificate Table 3 or 5. See Note 1 on next page.

**2. AM and PM Responsivity Functions:** See Note 1 on next page.

Figure 1. Responsivity Function



$$RS (am) = \sum_{i=0}^n a_i \cdot \cos^i(I) \quad [3]$$

$$RS (pm) = \sum_{j=0}^m b_j \cdot \cos^j(I)$$

where the coefficients  $a_i$  and  $b_j$  are available upon request.

The quality of the function fit to data is shown in Figure 1 and 2.

Figure 2. Net IR Corrected Responsivity Function

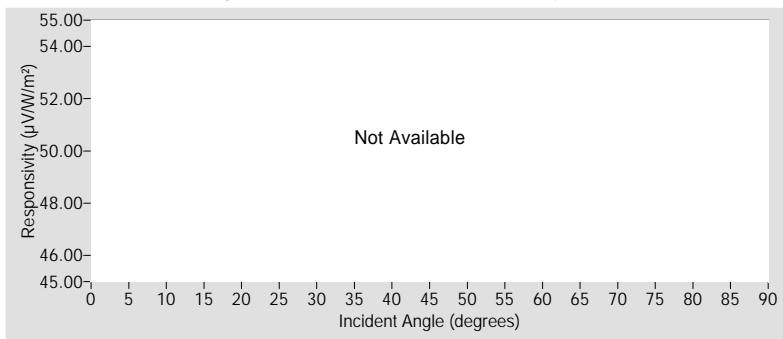


Table 1. Function Validity

	AM	PM
Uncertainty U95 (%)	±1.64	±1.64
R <sup>2</sup>	0.9999985	0.9999981
Valid incidence angle range	16.3° to 79.1°	16.3° to 84.4°
Net IR corr. uncert. U95 (%)	N/A	N/A
Net IR corrected R <sup>2</sup>	N/A	N/A
Corr. valid inc. angle range	N/A	N/A

**3. Nine-degree Bin Responsivity:** See Note 1 on next page.

Table 2. Nine-degree responsivities

Inc. Angle	Responsivity						Net IR Corr. Responsivity					
	AM		PM		Combined		AM		PM		Combined	
	RS ( $\mu V/W/m^2$ )	U95 (%)	RS ( $\mu V/W/m^2$ )	U95 (%)	RS ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)
0-9	8.8678	*	8.8676	*	8.8677	*	N/A	N/A	N/A	N/A	N/A	N/A
9-18	8.8331	*	8.8297	*	8.8314	*	N/A	N/A	N/A	N/A	N/A	N/A
18-27	8.8379	±1.65	8.7421	±1.76	8.7900	±2.13	N/A	N/A	N/A	N/A	N/A	N/A
27-36	8.7994	±1.75	8.6373	±1.75	8.7183	±2.76	N/A	N/A	N/A	N/A	N/A	N/A
36-45	8.6850	±1.74	8.4650	±1.95	8.5750	±3.31	N/A	N/A	N/A	N/A	N/A	N/A
45-54	8.5762	±1.77	8.2924	±1.89	8.4343	±3.75	N/A	N/A	N/A	N/A	N/A	N/A
54-63	8.4499	±1.75	8.0988	±2.03	8.2743	±4.43	N/A	N/A	N/A	N/A	N/A	N/A
63-72	8.3563	±1.86	7.8655	±3.13	8.1109	±7.41	N/A	N/A	N/A	N/A	N/A	N/A
72-81	8.0230	*	7.1514	±6.28	7.5872	*	N/A	N/A	N/A	N/A	N/A	N/A
81-90	7.3975	*	5.4489	*	6.4232	*	N/A	N/A	N/A	N/A	N/A	N/A

\* The responsivity is based on extrapolated data and the corresponding uncertainty is undefined.

#### 4. The Single Responsivities: See Note 1 below.

**Table 3. Single Responsivities**

Responsivity Characterization	RS ( $\mu\text{V/W/m}^2$ )	U95 † (%)
45°	8.4979	+4.51 / -5.82
45° - 55°	8.4218	$\pm 3.06$
Composite	8.5847	+3.54 / -31.52
45° (Net IR Corr.)	N/A	N/A
45° - 55° (Net IR Corr.)	N/A	N/A
Composite (Net IR Corr.)	N/A	N/A

† Valid incident angle ranges:

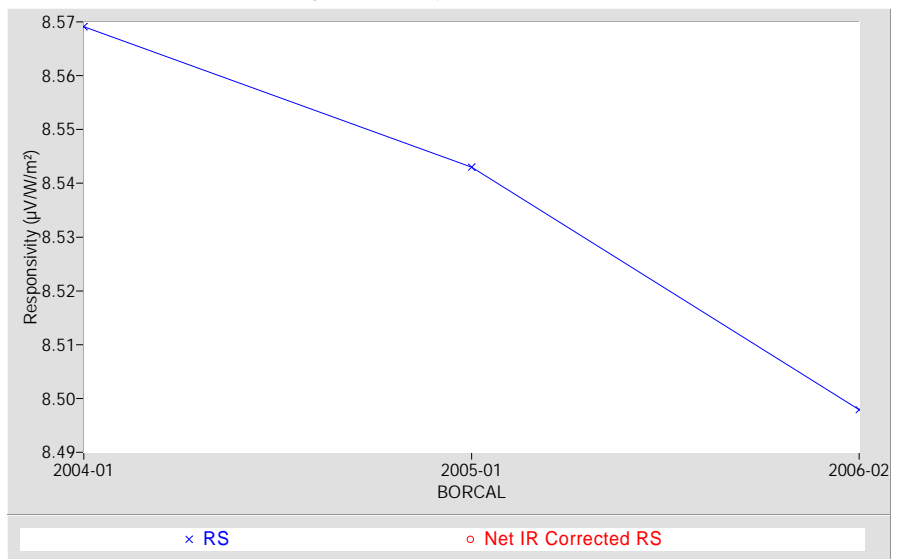
45°: 30.0° to 60.0°

45° - 55°: 45.0° to 55.0°

Composite: 16.3° to 79.1°

The instrument responsivity at  $I = 45^\circ$  may be used to monitor instrument stability. The instrument's history at  $I = 45^\circ$  is shown in Figure 2.

**Figure 2. History of instrument at  $I = 45^\circ$**



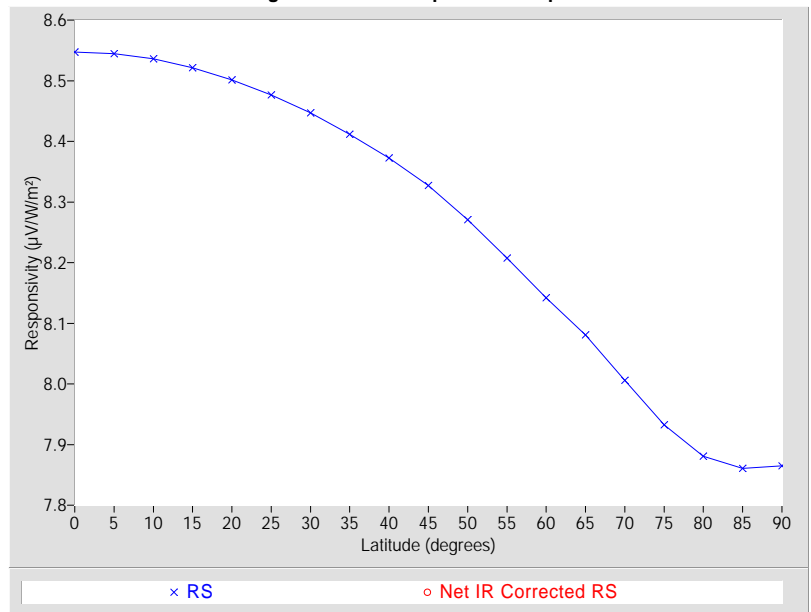
#### 5. Latitude Optimized Responsivity: See Note 1 below.

**Table 4. Latitude Optimized Responsivities**

Latitude	RS ( $\mu\text{V/W/m}^2$ )	Error estimate* (%)	RSc ( $\mu\text{V/W/m}^2$ ) Net IR Corr.	Error estimate* (%) Net IR Corr.
0	8.5471	+4.22 / -47.34	N/A	N/A
5	8.5447	+4.24 / -47.32	N/A	N/A
10	8.5360	+4.34 / -47.27	N/A	N/A
15	8.5214	+4.51 / -47.18	N/A	N/A
20	8.5014	+4.74 / -47.05	N/A	N/A
25	8.4766	+5.01 / -46.90	N/A	N/A
30	8.4468	+5.20 / -46.71	N/A	N/A
35	8.4118	+5.51 / -46.49	N/A	N/A
40	8.3728	+5.98 / -46.24	N/A	N/A
45	8.3270	+6.54 / -45.94	N/A	N/A
50	8.2706	+7.25 / -45.58	N/A	N/A
55	8.2074	+7.46 / -45.16	N/A	N/A
60	8.1419	+7.46 / -44.72	N/A	N/A
65	8.0808	+7.58 / -44.30	N/A	N/A
70	8.0057	+7.78 / -43.78	N/A	N/A
75	7.9322	+8.04 / -43.25	N/A	N/A
80	7.8808	+7.72 / -42.88	N/A	N/A
85	7.8608	+7.23 / -42.74	N/A	N/A
90	7.8652	+6.89 / -42.77	N/A	N/A

\* Uncertainty is undefined

**Figure 3. Latitude Optimized Responsivities**



#### Application of the responsivities and uncertainties:

The responsivities above are applied according to equation [1]:

##### Example

Instrument responsivity (RS) =  $7.34 \mu\text{V/W/m}^2 \pm 2.7\%$

Instrument output voltage (V) =  $0.00624 \text{ V}$  ( $6240 \mu\text{V}$ )

Irradiance (IRR) =  $V / RS = 6240 / 7.34 = 850.1 \text{ W/m}^2 \pm 2.7\%$

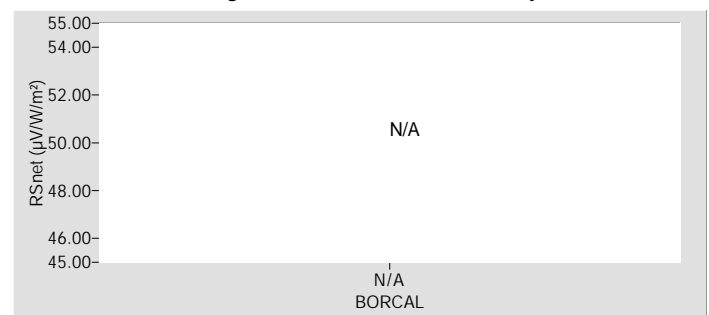
Thus, at the 95% confidence level, the irradiance lies between 827.1 and 873.1  $\text{W/m}^2$

##### Note 1:

All above methods, in conjunction with knowledge of the net infrared and sky irradiance distribution, may be used to determine the effective instrument responsivity with less uncertainties.

#### Instrument's Effective Net Infrared History (RSnet):

**Figure 4. Instrument's RSnet History**



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate

**Test Instrument:** Precision Spectral Pyranometer      **Manufacturer:** Eppley

**Model:** PSP      **Serial Number:** 30560F3

**Calibration Date:** 6/17/2006      **Due Date:** 6/17/2007

**Customer:** NREL-SRRL-BMS      **Calibration Site Parameters:** see Ancillary Data

**Environmental Conditions:** Outdoors, under natural sunlight (see Ancillary Data)

**Data Acquisition Dates:** 6/11-12, 6/17

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 31104	03/14/2006	03/14/2007
Diffuse Irradiance †	Eppley Black and White Pyranometer Model 8-48, S/N 32858	04/05/2006	04/05/2007
Diffuse Irradiance †	Eppley Black and White Pyranometer Model 8-48, S/N 32871	04/05/2006	04/05/2007
Data Acquisition ‡	NREL Data Proof Scanner System Model RAP-DAQ, S/N 2005-998	11/22/2005	11/22/2006
Data Acquisition ‡	NREL Data Proof Scanner System Model RAP-DAQ, S/N 2005-999	11/22/2005	11/22/2006

† Traceable to the World Radiometric Reference

‡ Traceable to the National Institute of Standards and Technology

**Number of pages of certificate:** 4

**Calibration Procedure:** [1] Myers, D., Stoffel, T., Reda, I., Wilcox, S., and Andreas, A., 2002, "Recent Progress in Reducing the Uncertainty in and Improving Pyranometer Calibrations." Journal of Solar Energy Engineering, vol. 124, pp. 44-50. The American Society of Mechanical Engineers, Transactions of the ASME.  
[2] "Improved Methods for Broadband Outdoor Radiometer Calibration (BORCAL)," Wilcox, S., Andreas, A., Reda, I., and Myers, D., Proceedings of the ARM Science Team Meeting, St. Petersburg, Florida, April 2002. Available upon request.

This calibration certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval by the calibration facility. Calibration certificates without signatures are not valid.

**Calibrated by:** Ibrahim Reda and Steve Wilcox

**Certified by:**

-----  
Afshin M. Andreas

Title: Scientist II

Date: -----

**Quality Assured by:**

-----  
Daryl R. Myers

Title: Senior Scientist II

Date: -----

# Calibration Results

## 30560F3 Eppley PSP

Figure 1. Responsivity vs Incident Angle

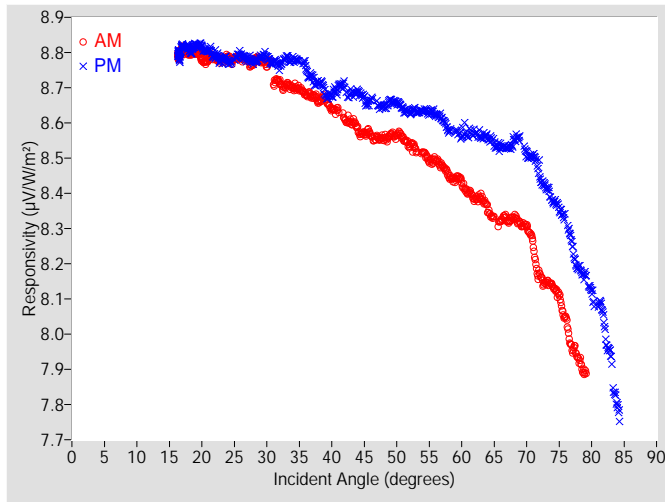


Figure 2. Responsivity vs Local Standard Time

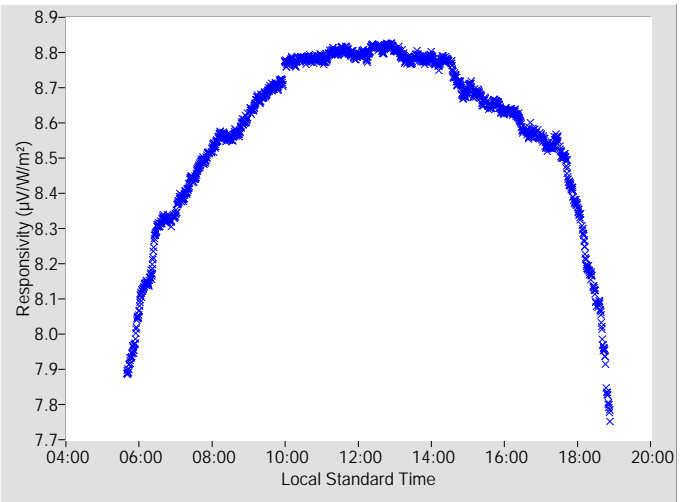


Table 2. Calibration Label Values

RS @ 45° (µV/W/m²) ‡	U95 (%) †	Tilt / Azm
8.6185	+2.53 / -2.69	0.0° / 0.0°

† Valid incident angle range: 30.0° to 60.0°

‡ Estimated thermal offset error during calibration = -20.000 W/m²

Table 3. Instrument Responsivity (RS) and Calibration Uncertainty (U95)

Inc. Angle†	AM			PM			Inc. Angle†	AM			PM		
	RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡	RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡		RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡	RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡
0	N/A	N/A	N/A	N/A	N/A	N/A	46	8.5666	0.57	95.23	8.6639	0.54	268.13
2	N/A	N/A	N/A	N/A	N/A	N/A	48	8.5580	0.56	93.45	8.6472	0.55	266.95
4	N/A	N/A	N/A	N/A	N/A	N/A	50	8.5632	0.57	91.69	8.6582	0.55	268.67
6	N/A	N/A	N/A	N/A	N/A	N/A	52	8.5363	0.62	89.99	8.6297	0.56	270.33
8	N/A	N/A	N/A	N/A	N/A	N/A	54	8.5156	0.61	88.33	8.6346	0.57	271.98
10	N/A	N/A	N/A	N/A	N/A	N/A	56	8.4957	0.63	86.76	8.6233	0.60	273.57
12	N/A	N/A	N/A	N/A	N/A	N/A	58	8.4505	0.69	85.17	8.5792	0.63	275.14
14	N/A	N/A	N/A	N/A	N/A	N/A	60	8.4314	0.72	83.61	8.5658	0.68	276.71
16	N/A	N/A	N/A	N/A	N/A	N/A	62	8.3844	0.71	82.07	8.5722	0.66	278.16
18	8.8017	0.47	152.40	8.8126	0.48	207.27	64	8.3559	0.82	80.55	8.5588	0.71	279.74
20	8.7826	0.56	142.43	8.8164	0.48	219.19	66	8.3221	0.80	79.03	8.5301	0.72	281.26
22	8.7859	0.51	134.03	8.7909	0.53	227.20	68	8.3320	0.84	77.49	8.5476	0.80	282.80
24	8.7879	0.51	127.76	8.7744	0.48	233.38	70	8.3064	0.95	75.99	8.5102	0.85	284.33
26	8.7841	0.50	122.75	8.7937	0.50	238.18	72	8.1675	1.18	74.52	8.4526	1.05	285.87
28	8.7735	0.52	118.46	8.7759	0.49	242.35	74	8.1368	1.10	72.96	8.3763	1.03	287.48
30	8.7672	0.50	114.83	8.7898	0.52	245.93	76	8.0426	1.49	71.38	8.3334	1.20	288.85
32	8.7160	0.53	111.39	8.7636	0.52	249.17	78	7.9298	1.45	69.77	8.1875	1.37	290.60
34	8.6998	0.51	108.52	8.7799	0.49	252.01	80	N/A	N/A	N/A	8.1183	1.57	292.26
36	8.6810	0.52	105.87	8.7591	0.56	254.58	82	N/A	N/A	N/A	8.0198	2.07	293.93
38	8.6612	0.52	103.46	8.7135	0.58	256.97	84	N/A	N/A	N/A	7.7919	2.69	295.70
40	8.6394	0.56	101.20	8.6809	0.53	259.22	86	N/A	N/A	N/A	N/A	N/A	N/A
42	8.6110	0.54	99.10	8.7048	0.57	261.24	88	N/A	N/A	N/A	N/A	N/A	N/A
44	8.5816	0.60	97.12	8.6871	0.53	263.30	90	N/A	N/A	N/A	N/A	N/A	N/A

† Angle of incidence (degrees)

‡ Average azimuth angle for ±0.3° of incidence angle

N/A - Not Available



# Effective Net Infrared Corrected Calibration Results

## 30560F3 Eppley PSP

Figure 3. Responsivity vs Incident Angle

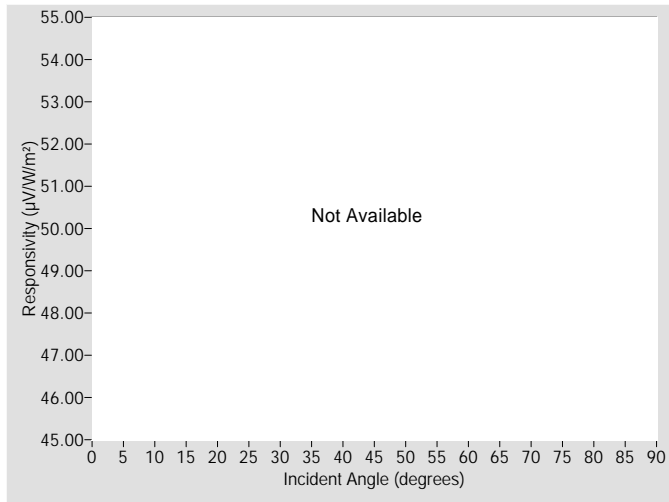


Figure 4. Responsivity vs Local Standard Time

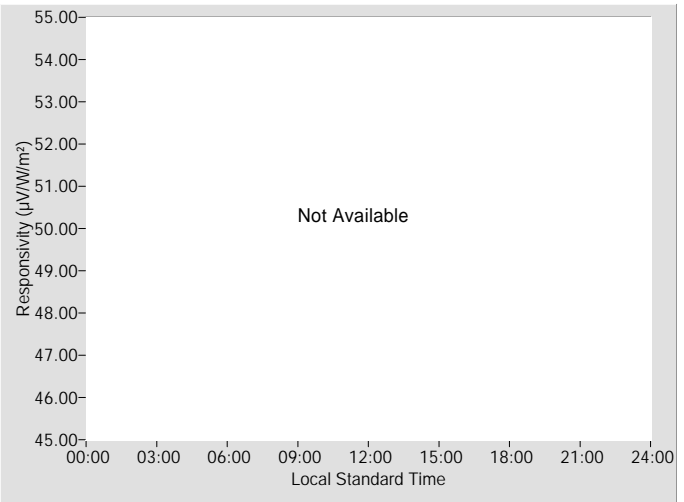


Table 4. Net IR Corrected Calibration Label Values

RSc @ 45° (µV/W/m²) ‡	U95 (%) †	Tilt / Azm
N/A	N/A	0.0° / 0.0°

† Valid incident angle range: N/A

‡ RSnet = N/A

Table 5. Net IR Corrected Instrument Responsivity (RS) and Calibration Uncertainty (U95)

Inc. Angle†	AM			PM			Inc. Angle†	AM			PM		
	RSc (µV/W/m²)	U95 ± (%)	Azm. Angle‡	RSc (µV/W/m²)	U95 ± (%)	Azm. Angle‡		RSc (µV/W/m²)	U95 ± (%)	Azm. Angle‡	RSc (µV/W/m²)	U95 ± (%)	Azm. Angle‡
0	N/A	N/A	N/A	N/A	N/A	N/A	46	N/A	N/A	N/A	N/A	N/A	N/A
2	N/A	N/A	N/A	N/A	N/A	N/A	48	N/A	N/A	N/A	N/A	N/A	N/A
4	N/A	N/A	N/A	N/A	N/A	N/A	50	N/A	N/A	N/A	N/A	N/A	N/A
6	N/A	N/A	N/A	N/A	N/A	N/A	52	N/A	N/A	N/A	N/A	N/A	N/A
8	N/A	N/A	N/A	N/A	N/A	N/A	54	N/A	N/A	N/A	N/A	N/A	N/A
10	N/A	N/A	N/A	N/A	N/A	N/A	56	N/A	N/A	N/A	N/A	N/A	N/A
12	N/A	N/A	N/A	N/A	N/A	N/A	58	N/A	N/A	N/A	N/A	N/A	N/A
14	N/A	N/A	N/A	N/A	N/A	N/A	60	N/A	N/A	N/A	N/A	N/A	N/A
16	N/A	N/A	N/A	N/A	N/A	N/A	62	N/A	N/A	N/A	N/A	N/A	N/A
18	N/A	N/A	N/A	N/A	N/A	N/A	64	N/A	N/A	N/A	N/A	N/A	N/A
20	N/A	N/A	N/A	N/A	N/A	N/A	66	N/A	N/A	N/A	N/A	N/A	N/A
22	N/A	N/A	N/A	N/A	N/A	N/A	68	N/A	N/A	N/A	N/A	N/A	N/A
24	N/A	N/A	N/A	N/A	N/A	N/A	70	N/A	N/A	N/A	N/A	N/A	N/A
26	N/A	N/A	N/A	N/A	N/A	N/A	72	N/A	N/A	N/A	N/A	N/A	N/A
28	N/A	N/A	N/A	N/A	N/A	N/A	74	N/A	N/A	N/A	N/A	N/A	N/A
30	N/A	N/A	N/A	N/A	N/A	N/A	76	N/A	N/A	N/A	N/A	N/A	N/A
32	N/A	N/A	N/A	N/A	N/A	N/A	78	N/A	N/A	N/A	N/A	N/A	N/A
34	N/A	N/A	N/A	N/A	N/A	N/A	80	N/A	N/A	N/A	N/A	N/A	N/A
36	N/A	N/A	N/A	N/A	N/A	N/A	82	N/A	N/A	N/A	N/A	N/A	N/A
38	N/A	N/A	N/A	N/A	N/A	N/A	84	N/A	N/A	N/A	N/A	N/A	N/A
40	N/A	N/A	N/A	N/A	N/A	N/A	86	N/A	N/A	N/A	N/A	N/A	N/A
42	N/A	N/A	N/A	N/A	N/A	N/A	88	N/A	N/A	N/A	N/A	N/A	N/A
44	N/A	N/A	N/A	N/A	N/A	N/A	90	N/A	N/A	N/A	N/A	N/A	N/A

† Angle of incidence (degrees)

‡ Average azimuth angle for ±0.3° of incidence angle

N/A - Not Available

## Suggested Methods of Applying Calibration Results

### 30560F3 Eppley PSP

Listed below are the results for the methods documented in "Improved Methods for Broadband Outdoor Radiometer Calibration (BORCAL)," Wilcox et al., Proceedings of the ARM Science Team Meeting, St. Petersburg, Florida, April 2002. Computing the net infrared corrected solar irradiance is documented in "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error during Outdoor Calibration using the Component Sum Method," Reda et al., Journal of Atmospheric and Oceanic Technology V. 22 (10), pp. 1531-1540, October 2005.

In all cases, the solar irradiance is calculated from the instrument responsivity using one of these equations:

$$IRR = V / RS \quad [1]$$

$$IRR (corr.) = (V - W_{net} * RS_{net}) / RS_{sc} \quad [2]$$

where,

$IRR$  = solar irradiance (Watts per square meter),

$V$  = radiometer output voltage (microvolts),

$RS$  = responsivity of the radiometer ( $\mu V/W/m^2$ ),

$IRR (corr.)$  = effective net infrared corrected solar irradiance ( $W/m^2$ ),

$W_{net}$  = effective net infrared measured by pyrgeometer ( $W/m^2$ ),

$RS_{net}$  = pyranometer net infrared response ( $\mu V/W/m^2$ ), see Table 4,

$RS_{sc}$  = effective net infrared corrected responsivity ( $\mu V/W/m^2$ ).

**1. Two-degree Responsivities:** Responsivities are obtained from Certificate Table 3 or 5. See Note 1 on next page.

**2. AM and PM Responsivity Functions:** See Note 1 on next page.

Figure 1. Responsivity Function

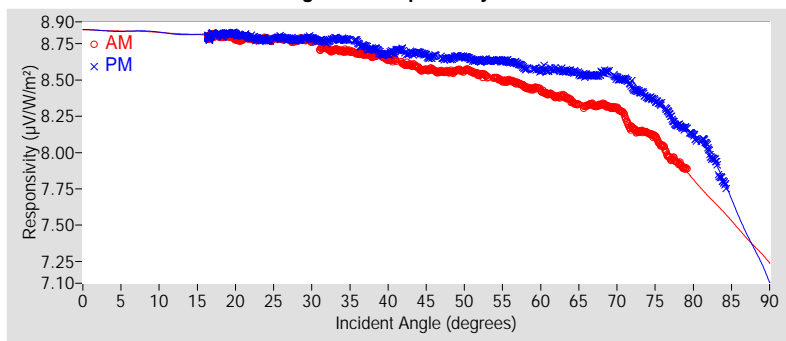


Figure 2. Net IR Corrected Responsivity Function



$$RS (am) = \sum_{i=0}^n a_i \cdot \cos^i(I) \quad [3]$$

$$RS (pm) = \sum_{j=0}^m b_j \cdot \cos^j(I)$$

where the coefficients  $a_i$  and  $b_j$  are available upon request.

The quality of the function fit to data is shown in Figure 1 and 2.

Table 1. Function Validity

	AM	PM
Uncertainty U95 (%)	±1.12	±1.12
R <sup>2</sup>	0.9999990	0.9999985
Valid incidence angle range	16.3° to 79.1°	16.3° to 84.3°
Net IR corr. uncert. U95 (%)	N/A	N/A
Net IR corrected R <sup>2</sup>	N/A	N/A
Corr. valid inc. angle range	N/A	N/A

**3. Nine-degree Bin Responsivity:** See Note 1 on next page.

Table 2. Nine-degree responsivities

Inc. Angle	Responsivity						Net IR Corr. Responsivity					
	AM		PM		Combined		AM		PM		Combined	
	RS ( $\mu V/W/m^2$ )	U95 (%)	RS ( $\mu V/W/m^2$ )	U95 (%)	RS ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)
0-9	8.8388	*	8.8389	*	8.8389	*	N/A	N/A	N/A	N/A	N/A	N/A
9-18	8.8170	*	8.8185	*	8.8177	*	N/A	N/A	N/A	N/A	N/A	N/A
18-27	8.7874	±1.12	8.7952	±1.14	8.7913	±1.16	N/A	N/A	N/A	N/A	N/A	N/A
27-36	8.7359	±1.26	8.7768	±1.13	8.7564	±1.44	N/A	N/A	N/A	N/A	N/A	N/A
36-45	8.6322	±1.27	8.7040	±1.18	8.6681	±1.82	N/A	N/A	N/A	N/A	N/A	N/A
45-54	8.5540	±1.16	8.6515	±1.15	8.6028	±1.73	N/A	N/A	N/A	N/A	N/A	N/A
54-63	8.4514	±1.40	8.5905	±1.20	8.5210	±2.48	N/A	N/A	N/A	N/A	N/A	N/A
63-72	8.3172	±1.40	8.5314	±1.23	8.4243	±3.08	N/A	N/A	N/A	N/A	N/A	N/A
72-81	8.0126	*	8.2870	±2.46	8.1498	*	N/A	N/A	N/A	N/A	N/A	N/A
81-90	7.4997	*	7.6166	*	7.5582	*	N/A	N/A	N/A	N/A	N/A	N/A

\* The responsivity is based on extrapolated data and the corresponding uncertainty is undefined.

#### 4. The Single Responsivities: See Note 1 below.

**Table 3. Single Responsivities**

Responsivity Characterization	RS ( $\mu\text{V/W/m}^2$ )	U95 † (%)
45°	8.6185	+2.53 / -2.69
45° - 55°	8.5977	$\pm 1.53$
Composite	8.6833	+1.91 / -12.65
45° (Net IR Corr.)	N/A	N/A
45° - 55° (Net IR Corr.)	N/A	N/A
Composite (Net IR Corr.)	N/A	N/A

† Valid incident angle ranges:

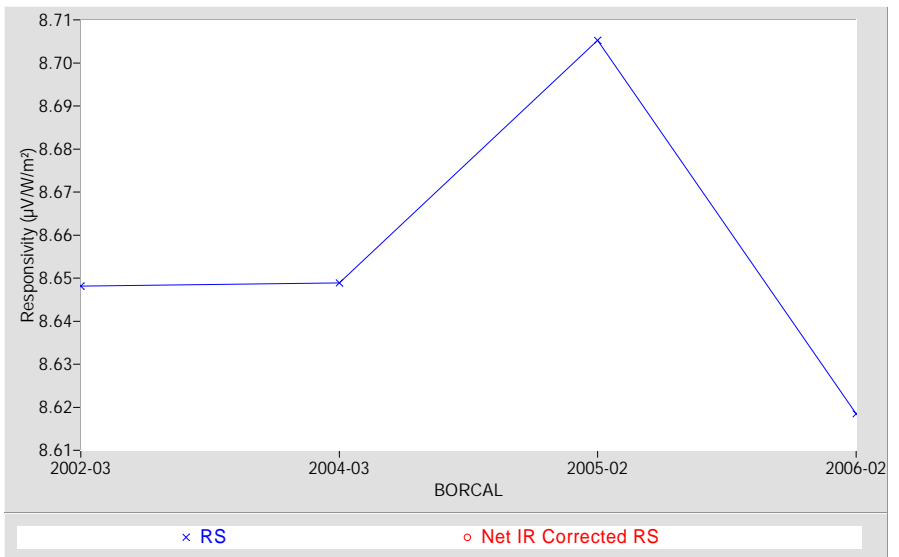
45°: 30.0° to 60.0°

45° - 55°: 45.0° to 55.0°

Composite: 16.3° to 79.1°

The instrument responsivity at  $I = 45^\circ$  may be used to monitor instrument stability. The instrument's history at  $I = 45^\circ$  is shown in Figure 2.

**Figure 2. History of instrument at  $I = 45^\circ$**



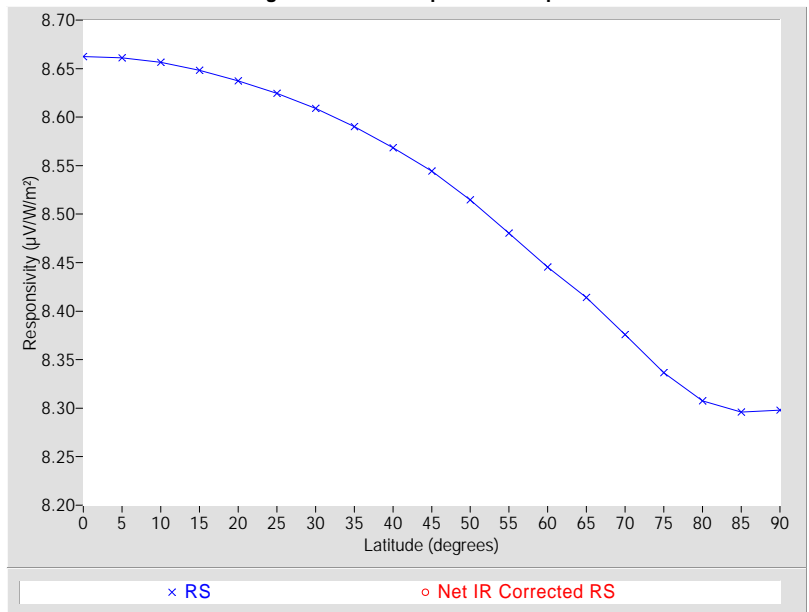
#### 5. Latitude Optimized Responsivity: See Note 1 below.

**Table 4. Latitude Optimized Responsivities**

Latitude	RS ( $\mu\text{V/W/m}^2$ )	Error estimate* (%)	RSc ( $\mu\text{V/W/m}^2$ )	Error estimate* (%)
			Net IR Corr.	Net IR Corr.
0	8.6622	+2.41 / -16.55	N/A	N/A
5	8.6612	+2.42 / -16.54	N/A	N/A
10	8.6565	+2.47 / -16.50	N/A	N/A
15	8.6483	+2.56 / -16.42	N/A	N/A
20	8.6375	+2.67 / -16.31	N/A	N/A
25	8.6244	+2.80 / -16.19	N/A	N/A
30	8.6090	+2.88 / -16.04	N/A	N/A
35	8.5900	+2.94 / -15.85	N/A	N/A
40	8.5684	+3.11 / -15.64	N/A	N/A
45	8.5442	+3.17 / -15.40	N/A	N/A
50	8.5148	+3.39 / -15.11	N/A	N/A
55	8.4804	+3.73 / -14.77	N/A	N/A
60	8.4455	+3.76 / -14.42	N/A	N/A
65	8.4140	+3.49 / -14.10	N/A	N/A
70	8.3759	+3.69 / -13.71	N/A	N/A
75	8.3367	+3.84 / -13.30	N/A	N/A
80	8.3074	+3.85 / -13.00	N/A	N/A
85	8.2961	+3.42 / -12.88	N/A	N/A
90	8.2980	+3.23 / -12.90	N/A	N/A

\* Uncertainty is undefined

**Figure 3. Latitude Optimized Responsivities**



#### Application of the responsivities and uncertainties:

The responsivities above are applied according to equation [1]:

##### Example

Instrument responsivity (RS) =  $7.34 \mu\text{V/W/m}^2 \pm 2.7\%$

Instrument output voltage (V) =  $0.00624 \text{ V}$  ( $6240 \mu\text{V}$ )

Irradiance (IRR) =  $V / RS = 6240 / 7.34 = 850.1 \text{ W/m}^2 \pm 2.7\%$

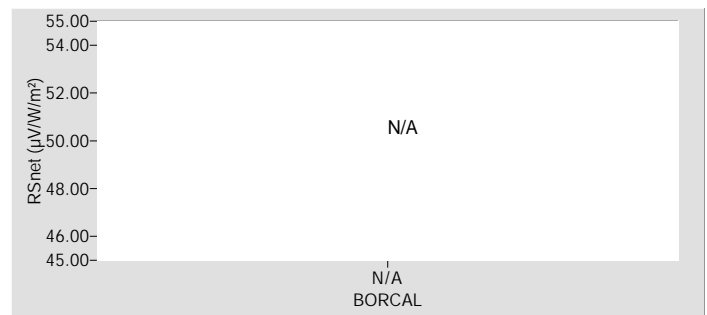
Thus, at the 95% confidence level, the irradiance lies between 827.1 and 873.1  $\text{W/m}^2$

##### Note 1:

All above methods, in conjunction with knowledge of the net infrared and sky irradiance distribution, may be used to determine the effective instrument responsivity with less uncertainties.

#### Instrument's Effective Net Infrared History (RSnet):

**Figure 4. Instrument's RSnet History**



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate

**Test Instrument:** Normal Incidence Pyrheliometer **Manufacturer:** Eppley  
**Model:** NIP **Serial Number:** 31355E6  
**Calibration Date:** 6/17/2006 **Due Date:** 6/17/2007  
**Customer:** NREL-SRRL-BMS **Calibration Site Parameters:** see Ancillary Data  
**Environmental Conditions:** Outdoors, under natural sunlight (see Ancillary Data)  
**Data Acquisition Dates:** 6/11-12, 6/17

Table 1. Traceability

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 31104	03/14/2006	03/14/2007
Diffuse Irradiance †	Eppley Black and White Pyranometer Model 8-48, S/N 32858	04/05/2006	04/05/2007
Diffuse Irradiance †	Eppley Black and White Pyranometer Model 8-48, S/N 32871	04/05/2006	04/05/2007
Data Acquisition ‡	NREL Data Proof Scanner System Model RAP-DAQ, S/N 2005-998	11/22/2005	11/22/2006
Data Acquisition ‡	NREL Data Proof Scanner System Model RAP-DAQ, S/N 2005-999	11/22/2005	11/22/2006

† Traceable to the World Radiometric Reference

‡ Traceable to the National Institute of Standards and Technology

**Number of pages of certificate:** 3

**Calibration Procedure:** [1] Myers, D., Stoffel, T., Reda, I., Wilcox, S., and Andreas, A., 2002, "Recent Progress in Reducing the Uncertainty in and Improving Pyranometer Calibrations." Journal of Solar Energy Engineering, vol. 124, pp. 44-50. The American Society of Mechanical Engineers, Transactions of the ASME.  
[2] "Improved Methods for Broadband Outdoor Radiometer Calibration (BORCAL)," Wilcox, S., Andreas, A., Reda, I., and Myers, D., Proceedings of the ARM Science Team Meeting, St. Petersburg, Florida, April 2002. Available upon request.

This calibration certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval by the calibration facility. Calibration certificates without signatures are not valid.

**Calibrated by:** Ibrahim Reda and Steve Wilcox

**Certified by:**

-----  
Afshin M. Andreas

Title: Scientist II

Date: -----

**Quality Assured by:**

-----  
Daryl R. Myers

Title: Senior Scientist II

Date: -----

# Calibration Results

## 31355E6 Eppley NIP

Figure 1. Responsivity vs Zenith Angle

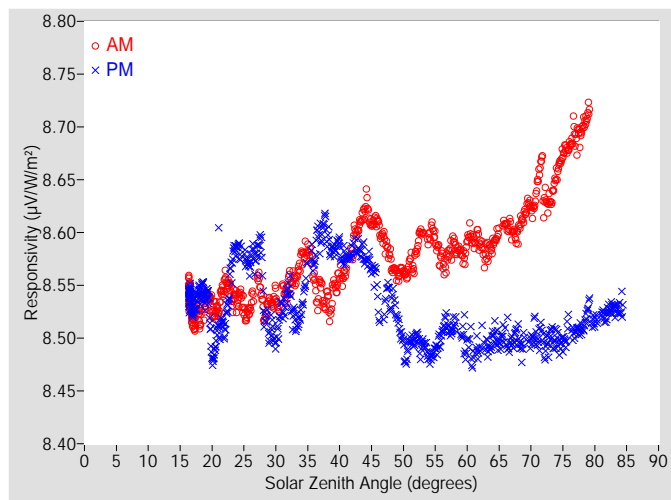


Figure 2. Responsivity vs Local Standard Time

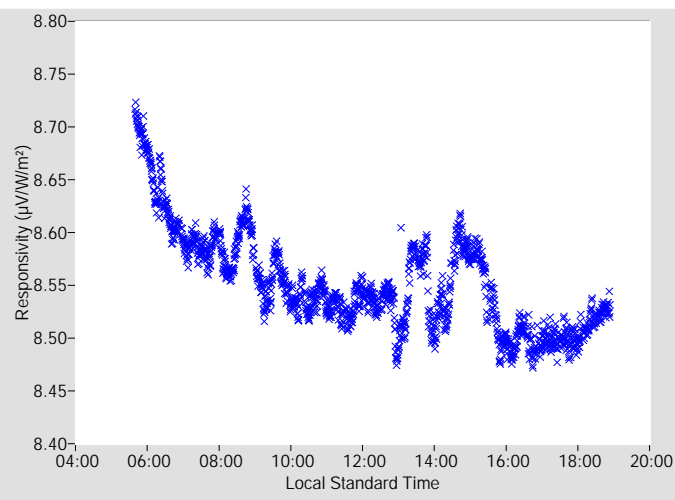


Table 2. Calibration Label Values

RS @ 45° (μV/W/m²) ‡	U95 (%) †	Tilt / Azm
8.5877	+0.95 / -1.64	N/A

† Valid zenith angle range: 30.0° to 60.0°

‡ Estimated thermal offset error during calibration is unspecified.

Table 3. Instrument Responsivity (RS) and Calibration Uncertainty (U95)

Zen. Angle†	AM			PM			Zen. Angle†	AM			PM		
	RS (μV/W/m²)	U95 ± (%)	Azm. Angle‡	RS (μV/W/m²)	U95 ± (%)	Azm. Angle‡		RS (μV/W/m²)	U95 ± (%)	Azm. Angle‡	RS (μV/W/m²)	U95 ± (%)	Azm. Angle‡
0	N/A	N/A	N/A	N/A	N/A	N/A	46	8.6098	0.36	95.26	8.5354	0.46	265.12
2	N/A	N/A	N/A	N/A	N/A	N/A	48	8.5745	0.40	93.44	8.5347	0.39	266.94
4	N/A	N/A	N/A	N/A	N/A	N/A	50	8.5630	0.35	91.68	8.4913	0.43	268.66
6	N/A	N/A	N/A	N/A	N/A	N/A	52	8.5825	0.41	89.98	8.5009	0.36	270.36
8	N/A	N/A	N/A	N/A	N/A	N/A	54	8.5949	0.35	88.33	8.4815	0.36	271.98
10	N/A	N/A	N/A	N/A	N/A	N/A	56	8.5745	0.37	86.75	8.5018	0.41	273.57
12	N/A	N/A	N/A	N/A	N/A	N/A	58	8.5902	0.36	85.20	8.5141	0.35	275.10
14	N/A	N/A	N/A	N/A	N/A	N/A	60	8.5906	0.40	83.64	8.4907	0.44	276.68
16	N/A	N/A	N/A	N/A	N/A	N/A	62	8.5899	0.39	82.10	8.4886	0.38	278.15
18	8.5207	0.38	152.36	8.5426	0.37	207.23	64	8.5878	0.38	80.54	8.5003	0.39	279.75
20	8.5308	0.36	142.40	8.4873	0.54	219.17	66	8.6077	0.35	79.03	8.5023	0.38	281.32
22	8.5508	0.41	134.00	8.5116	0.70	227.18	68	8.5997	0.38	77.52	8.4997	0.39	282.79
24	8.5351	0.36	127.73	8.5849	0.40	233.36	70	8.6231	0.39	75.99	8.4978	0.38	284.33
26	8.5292	0.37	122.67	8.5711	0.38	238.19	72	8.6418	0.48	74.51	8.4934	0.39	285.86
28	8.5279	0.43	118.44	8.5469	0.69	242.33	74	8.6543	0.45	72.96	8.5004	0.37	287.43
30	8.5399	0.36	114.82	8.4989	0.42	245.96	76	8.6814	0.40	71.37	8.5156	0.39	288.83
32	8.5500	0.38	111.38	8.5451	0.45	249.16	78	8.6986	0.44	69.78	8.5082	0.36	290.60
34	8.5753	0.40	108.51	8.5261	0.51	252.00	80	N/A	N/A	N/A	8.5174	0.37	292.28
36	8.5577	0.49	105.86	8.5744	0.42	254.63	82	N/A	N/A	N/A	8.5238	0.35	293.92
38	8.5385	0.40	103.45	8.6024	0.41	256.96	84	N/A	N/A	N/A	8.5299	0.36	295.69
40	8.5602	0.36	101.24	8.5856	0.36	259.21	86	N/A	N/A	N/A	N/A	N/A	N/A
42	8.5833	0.41	99.14	8.5834	0.35	261.22	88	N/A	N/A	N/A	N/A	N/A	N/A
44	8.6238	0.39	97.16	8.5764	0.37	263.29	90	N/A	N/A	N/A	N/A	N/A	N/A

† Solar zenith angle (degrees)

‡ Average azimuth angle for ±0.3° of zenith angle

N/A - Not Available

# Suggested Methods of Applying Calibration Results

## 31355E6 Eppley NIP

Listed below are the results for the methods documented in "Improved Methods for Broadband Outdoor Radiometer Calibration (BORCAL)," Wilcox, S., Andreas, A., Reda, I., and Myers, D., Proceedings of the ARM Science Team Meeting, St. Petersburg, Florida, April 2002. Available upon request.

In all cases, the solar irradiance is calculated from the instrument responsivity using the equation:

$$IRR = V / RS \quad [1]$$

where,

$IRR$  = solar irradiance (Watts per square meter)  
 $V$  = radiometer output voltage (microvolts)  
 $RS$  = responsivity of the radiometer ( $\mu V/W/m^2$ )

### 1. The Single Responsivities:

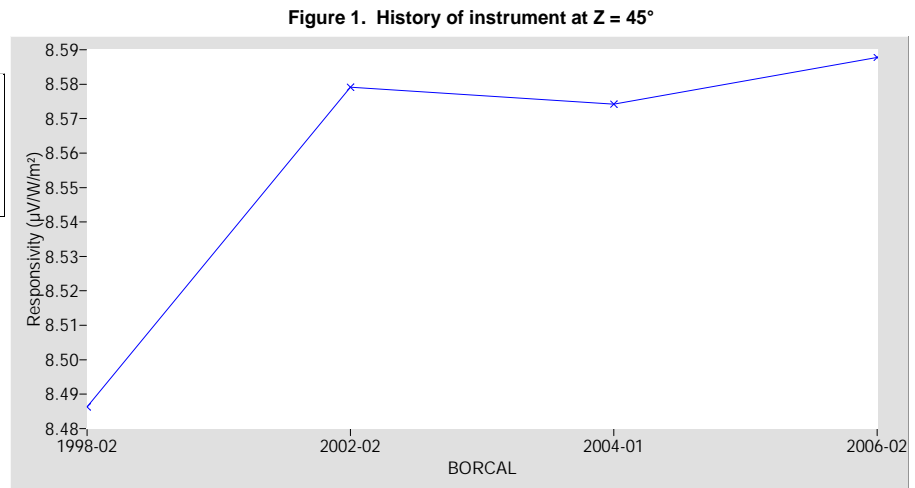
**Table 1. Single Responsivities**

Responsivity Characterization	RS ( $\mu V/W/m^2$ )	U95 (%)
45°	8.5877	+0.95 / -1.64 †
Average	8.5545	+2.13 / -1.32 ‡

† Valid zenith angle range: 30.0° to 60.0°

‡ Valid zenith angle range: 16.3° to 79.1°

The instrument responsivity at  $Z = 45^\circ$  may be used to monitor instrument stability. The instrument's history at  $Z = 45^\circ$  is shown in Figure 1.



### Application of the responsivities and uncertainties:

The responsivities above are applied according to equation [1]:

*Example*

Instrument responsivity ( $RS$ ) =  $7.34 \mu V/W/m^2 \pm 2.7\%$   
Instrument output voltage ( $V$ ) =  $0.00624 V$  ( $6240 \mu V$ )  
Irradiance ( $IRR$ ) =  $V / RS = 6240 / 7.34 = 850.1 W/m^2 \pm 2.7\%$

Thus, at the 95% confidence level, the irradiance lies between 827.1 and 873.1  $W/m^2$

# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

#### Calibration Certificate

**Test Instrument:** Silicon Pyranometer **Manufacturer:** Licor  
**Model:** LI200 **Serial Number:** PY1726  
**Calibration Date:** 6/17/2006 **Due Date:** 6/17/2007  
**Customer:** NREL-SRRL-BMS **Calibration Site Parameters:** see Ancillary Data  
**Environmental Conditions:** Outdoors, under natural sunlight (see Ancillary Data)  
**Data Acquisition Dates:** 6/11-12, 6/17

Table 1. Traceability

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppeley Absolute Cavity Radiometer Model HF, S/N 31104	03/14/2006	03/14/2007
Diffuse Irradiance †	Eppeley Black and White Pyranometer Model 8-48, S/N 32858	04/05/2006	04/05/2007
Diffuse Irradiance †	Eppeley Black and White Pyranometer Model 8-48, S/N 32871	04/05/2006	04/05/2007
Data Acquisition ‡	NREL Data Proof Scanner System Model RAP-DAQ, S/N 2005-998	11/22/2005	11/22/2006
Data Acquisition ‡	NREL Data Proof Scanner System Model RAP-DAQ, S/N 2005-999	11/22/2005	11/22/2006

† Traceable to the World Radiometric Reference

‡ Traceable to the National Institute of Standards and Technology

**Number of pages of certificate:** 4

**Calibration Procedure:** [1] Myers, D., Stoffel, T., Reda, I., Wilcox, S., and Andreas, A., 2002, "Recent Progress in Reducing the Uncertainty in and Improving Pyranometer Calibrations." Journal of Solar Energy Engineering, vol. 124, pp. 44-50. The American Society of Mechanical Engineers, Transactions of the ASME.  
[2] "Improved Methods for Broadband Outdoor Radiometer Calibration (BORCAL)," Wilcox, S., Andreas, A., Reda, I., and Myers, D., Proceedings of the ARM Science Team Meeting, St. Petersburg, Florida, April 2002. Available upon request.

This calibration certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval by the calibration facility. Calibration certificates without signatures are not valid.

**Calibrated by:** Ibrahim Reda and Steve Wilcox

**Certified by:**

-----  
Afshin M. Andreas

Title: Scientist II

Date: -----

**Quality Assured by:**

-----  
Daryl R. Myers

Title: Senior Scientist II

Date: -----

# Calibration Results

## PY1726 Licor LI200

Figure 1. Responsivity vs Incident Angle

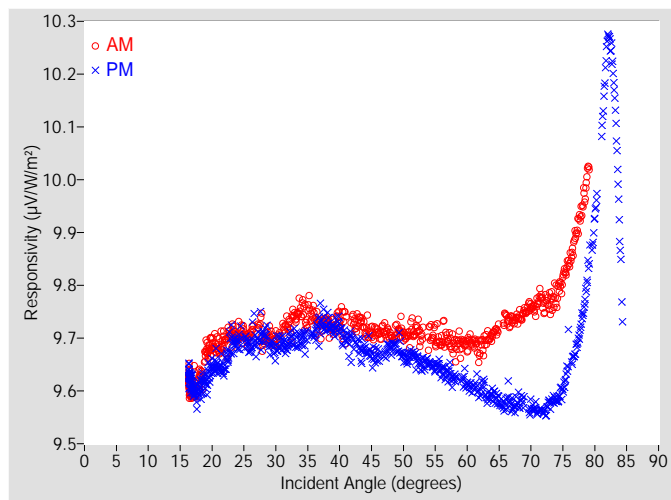


Figure 2. Responsivity vs Local Standard Time

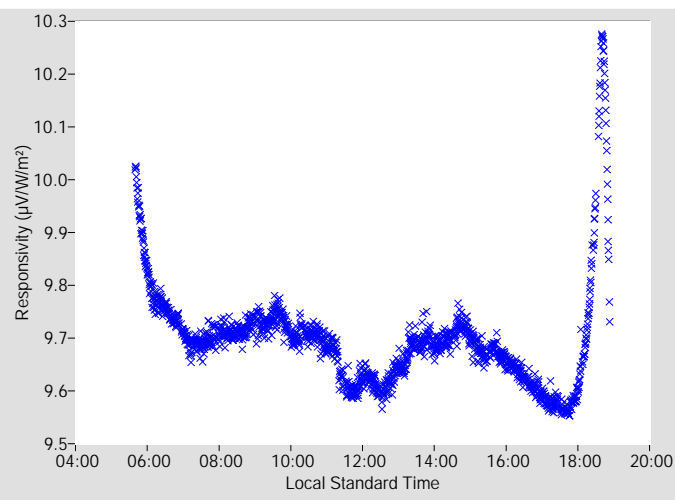


Table 2. Calibration Label Values

RS @ 45° (µV/W/m²) ‡	U95 (%) †	Tilt / Azm
9.6898	+1.46 / -1.39	0.0° / 0.0°

† Valid incident angle range: 30.0° to 60.0°

‡ Estimated thermal offset error during calibration is unspecified.

Table 3. Instrument Responsivity (RS) and Calibration Uncertainty (U95)

Inc. Angle†	AM			PM			Inc. Angle†	AM			PM		
	RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡	RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡		RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡	RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡
0	N/A	N/A	N/A	N/A	N/A	N/A	46	9.7116	0.58	95.26	9.6663	0.56	265.16
2	N/A	N/A	N/A	N/A	N/A	N/A	48	9.7036	0.57	93.44	9.6823	0.55	266.89
4	N/A	N/A	N/A	N/A	N/A	N/A	50	9.7059	0.64	91.68	9.6663	0.61	268.66
6	N/A	N/A	N/A	N/A	N/A	N/A	52	9.7148	0.64	90.02	9.6605	0.58	270.36
8	N/A	N/A	N/A	N/A	N/A	N/A	54	9.7036	0.64	88.32	9.6530	0.58	271.97
10	N/A	N/A	N/A	N/A	N/A	N/A	56	9.6983	0.66	86.74	9.6365	0.61	273.56
12	N/A	N/A	N/A	N/A	N/A	N/A	58	9.6820	0.69	85.16	9.6247	0.64	275.17
14	N/A	N/A	N/A	N/A	N/A	N/A	60	9.6894	0.67	83.64	9.6096	0.67	276.73
16	N/A	N/A	N/A	N/A	N/A	N/A	62	9.6810	0.74	82.10	9.5992	0.68	278.24
18	9.6248	0.63	152.33	9.6045	0.57	207.38	64	9.7065	0.76	80.57	9.5933	0.69	279.74
20	9.6878	0.56	142.39	9.6425	0.64	219.28	66	9.7385	0.79	79.02	9.5754	0.77	281.29
22	9.6948	0.58	134.11	9.6500	0.62	227.28	68	9.7404	0.84	77.52	9.5771	0.78	282.79
24	9.7076	0.55	127.83	9.6910	0.54	233.24	70	9.7598	0.92	75.98	9.5665	0.84	284.32
26	9.7093	0.53	122.65	9.6797	0.63	238.24	72	9.7628	0.99	74.51	9.5613	0.89	285.86
28	9.6990	0.61	118.35	9.7040	0.58	242.40	74	9.7825	1.12	72.99	9.5825	0.99	287.46
30	9.6960	0.51	114.73	9.6793	0.53	245.97	76	9.8451	1.27	71.40	9.6810	1.23	288.86
32	9.7262	0.59	111.44	9.6918	0.53	249.15	78	9.9495	1.50	69.77	9.7402	1.50	290.64
34	9.7550	0.58	108.50	9.6977	0.53	251.99	80	N/A	N/A	N/A	9.9267	1.63	292.25
36	9.7405	0.63	105.91	9.7060	0.64	254.62	82	N/A	N/A	N/A	10.261	2.05	293.96
38	9.7339	0.54	103.44	9.7268	0.53	257.01	84	N/A	N/A	N/A	9.8757	3.26	295.66
40	9.7376	0.62	101.23	9.7235	0.57	259.20	86	N/A	N/A	N/A	N/A	N/A	N/A
42	9.7305	0.55	99.09	9.6898	0.58	261.22	88	N/A	N/A	N/A	N/A	N/A	N/A
44	9.7152	0.57	97.11	9.6784	0.58	263.23	90	N/A	N/A	N/A	N/A	N/A	N/A

† Angle of incidence (degrees)

‡ Average azimuth angle for ±0.3° of incidence angle

N/A - Not Available



# Effective Net Infrared Corrected Calibration Results

## PY1726 Licor LI200

Figure 3. Responsivity vs Incident Angle

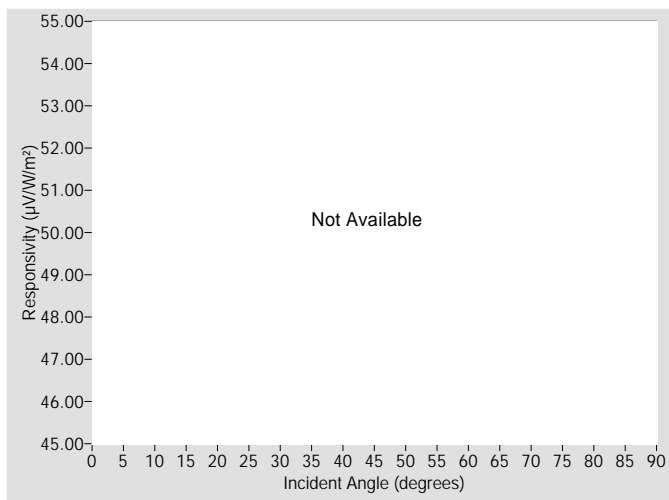


Figure 4. Responsivity vs Local Standard Time

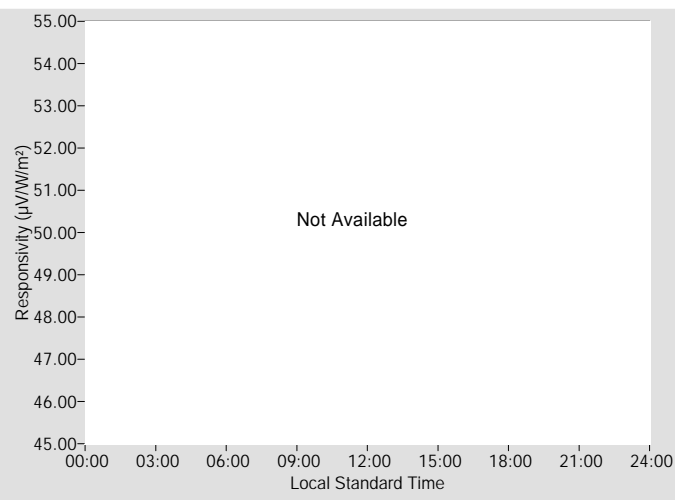


Table 4. Net IR Corrected Calibration Label Values

RSc @ 45° (μV/W/m²) ‡	U95 (%) †	Tilt / Azm
N/A	N/A	0.0° / 0.0°

† Valid incident angle range: N/A

‡ RSnet = N/A

Table 5. Net IR Corrected Instrument Responsivity (RS) and Calibration Uncertainty (U95)

Inc. Angle†	AM			PM			Inc. Angle†	AM			PM		
	RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡	RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡		RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡	RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡
0	N/A	N/A	N/A	N/A	N/A	N/A	46	N/A	N/A	N/A	N/A	N/A	N/A
2	N/A	N/A	N/A	N/A	N/A	N/A	48	N/A	N/A	N/A	N/A	N/A	N/A
4	N/A	N/A	N/A	N/A	N/A	N/A	50	N/A	N/A	N/A	N/A	N/A	N/A
6	N/A	N/A	N/A	N/A	N/A	N/A	52	N/A	N/A	N/A	N/A	N/A	N/A
8	N/A	N/A	N/A	N/A	N/A	N/A	54	N/A	N/A	N/A	N/A	N/A	N/A
10	N/A	N/A	N/A	N/A	N/A	N/A	56	N/A	N/A	N/A	N/A	N/A	N/A
12	N/A	N/A	N/A	N/A	N/A	N/A	58	N/A	N/A	N/A	N/A	N/A	N/A
14	N/A	N/A	N/A	N/A	N/A	N/A	60	N/A	N/A	N/A	N/A	N/A	N/A
16	N/A	N/A	N/A	N/A	N/A	N/A	62	N/A	N/A	N/A	N/A	N/A	N/A
18	N/A	N/A	N/A	N/A	N/A	N/A	64	N/A	N/A	N/A	N/A	N/A	N/A
20	N/A	N/A	N/A	N/A	N/A	N/A	66	N/A	N/A	N/A	N/A	N/A	N/A
22	N/A	N/A	N/A	N/A	N/A	N/A	68	N/A	N/A	N/A	N/A	N/A	N/A
24	N/A	N/A	N/A	N/A	N/A	N/A	70	N/A	N/A	N/A	N/A	N/A	N/A
26	N/A	N/A	N/A	N/A	N/A	N/A	72	N/A	N/A	N/A	N/A	N/A	N/A
28	N/A	N/A	N/A	N/A	N/A	N/A	74	N/A	N/A	N/A	N/A	N/A	N/A
30	N/A	N/A	N/A	N/A	N/A	N/A	76	N/A	N/A	N/A	N/A	N/A	N/A
32	N/A	N/A	N/A	N/A	N/A	N/A	78	N/A	N/A	N/A	N/A	N/A	N/A
34	N/A	N/A	N/A	N/A	N/A	N/A	80	N/A	N/A	N/A	N/A	N/A	N/A
36	N/A	N/A	N/A	N/A	N/A	N/A	82	N/A	N/A	N/A	N/A	N/A	N/A
38	N/A	N/A	N/A	N/A	N/A	N/A	84	N/A	N/A	N/A	N/A	N/A	N/A
40	N/A	N/A	N/A	N/A	N/A	N/A	86	N/A	N/A	N/A	N/A	N/A	N/A
42	N/A	N/A	N/A	N/A	N/A	N/A	88	N/A	N/A	N/A	N/A	N/A	N/A
44	N/A	N/A	N/A	N/A	N/A	N/A	90	N/A	N/A	N/A	N/A	N/A	N/A

† Angle of incidence (degrees)

‡ Average azimuth angle for ±0.3° of incidence angle

N/A - Not Available

# Suggested Methods of Applying Calibration Results

## PY1726 Licor LI200

Listed below are the results for the methods documented in "Improved Methods for Broadband Outdoor Radiometer Calibration (BORCAL)," Wilcox et al., Proceedings of the ARM Science Team Meeting, St. Petersburg, Florida, April 2002. Computing the net infrared corrected solar irradiance is documented in "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error during Outdoor Calibration using the Component Sum Method," Reda et al., Journal of Atmospheric and Oceanic Technology V. 22 (10), pp. 1531-1540, October 2005.

In all cases, the solar irradiance is calculated from the instrument responsivity using one of these equations:

$$\begin{aligned} IRR &= V / RS \\ IRR (corr.) &= (V - W_{net} * RS_{net}) / RS_c \end{aligned} \quad \begin{matrix} [1] \\ [2] \end{matrix}$$

where,

$$\begin{aligned} IRR &= \text{solar irradiance (Watts per square meter),} \\ V &= \text{radiometer output voltage (microvolts),} \\ RS &= \text{responsivity of the radiometer } (\mu V/W/m^2), \\ IRR (corr.) &= \text{effective net infrared corrected solar irradiance (W/m}^2\text{),} \\ W_{net} &= \text{effective net infrared measured by pyrgeometer (W/m}^2\text{),} \\ RS_{net} &= \text{pyranometer net infrared response } (\mu V/W/m^2\text{), see Table 4,} \\ RS_c &= \text{effective net infrared corrected responsivity } (\mu V/W/m^2). \end{aligned}$$

**1. Two-degree Responsivities:** Responsivities are obtained from Certificate Table 3 or 5. See Note 1 on next page.

**2. AM and PM Responsivity Functions:** See Note 1 on next page.

Figure 1. Responsivity Function

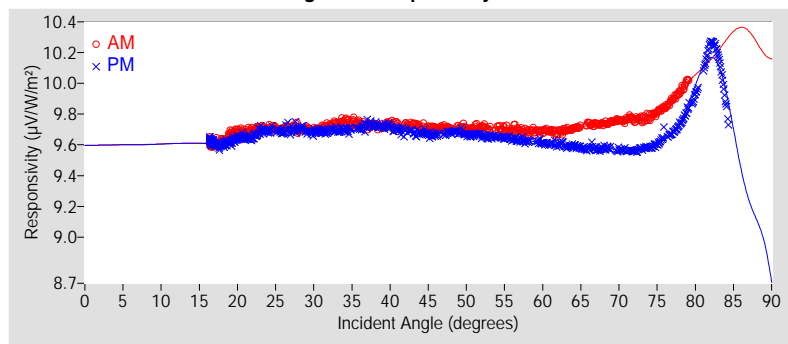
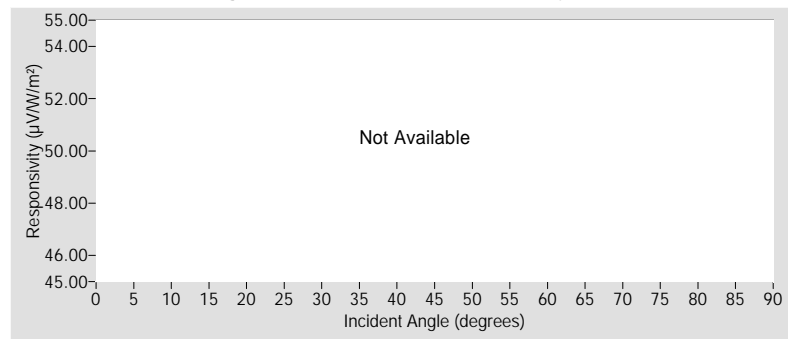


Figure 2. Net IR Corrected Responsivity Function



$$\begin{aligned} RS (am) &= \sum_{i=0}^n a_i \cdot \cos^i(I) \\ RS (pm) &= \sum_{j=0}^m b_j \cdot \cos^j(I) \end{aligned} \quad [3]$$

where the coefficients  $a_i$  and  $b_j$  are available upon request.

The quality of the function fit to data is shown in Figure 1 and 2.

Table 1. Function Validity

	AM	PM
Uncertainty U95 (%)	±1.27	±1.27
R <sup>2</sup>	0.9999996	0.9999945
Valid incidence angle range	16.3° to 79.0°	16.3° to 84.3°
Net IR corr. uncert. U95 (%)	N/A	N/A
Net IR corrected R <sup>2</sup>	N/A	N/A
Corr. valid inc. angle range	N/A	N/A

**3. Nine-degree Bin Responsivity:** See Note 1 on next page.

Table 2. Nine-degree responsivities

Inc. Angle	Responsivity						Net IR Corr. Responsivity					
	AM		PM		Combined		AM		PM		Combined	
	RS (μV/W/m²)	U95 (%)	RS (μV/W/m²)	U95 (%)	RS (μV/W/m²)	U95 (%)	RSc (μV/W/m²)	U95 (%)	RSc (μV/W/m²)	U95 (%)	RSc (μV/W/m²)	U95 (%)
0-9	9.5995	*	9.5997	*	9.5996	*	N/A	N/A	N/A	N/A	N/A	N/A
9-18	9.6106	*	9.6089	*	9.6098	*	N/A	N/A	N/A	N/A	N/A	N/A
18-27	9.6893	±1.33	9.6583	±1.33	9.6738	±1.47	N/A	N/A	N/A	N/A	N/A	N/A
27-36	9.7198	±1.30	9.6924	±1.27	9.7061	±1.35	N/A	N/A	N/A	N/A	N/A	N/A
36-45	9.7324	±1.28	9.7059	±1.30	9.7191	±1.40	N/A	N/A	N/A	N/A	N/A	N/A
45-54	9.7084	±1.27	9.6679	±1.28	9.6882	±1.37	N/A	N/A	N/A	N/A	N/A	N/A
54-63	9.6907	±1.28	9.6221	±1.30	9.6564	±1.54	N/A	N/A	N/A	N/A	N/A	N/A
63-72	9.7367	±1.31	9.5757	±1.29	9.6562	±1.99	N/A	N/A	N/A	N/A	N/A	N/A
72-81	9.8836	*	9.7129	±2.77	9.7983	*	N/A	N/A	N/A	N/A	N/A	N/A
81-90	10.247	*	9.5654	*	9.9063	*	N/A	N/A	N/A	N/A	N/A	N/A

\* The responsivity is based on extrapolated data and the corresponding uncertainty is undefined.

#### 4. The Single Responsivities: See Note 1 below.

**Table 3. Single Responsivities**

Responsivity Characterization	RS ( $\mu\text{V/W/m}^2$ )	U95 † (%)
45°	9.6898	+1.46 / -1.39
45° - 55°	9.6864	$\pm 1.32$
Composite	9.6698	+6.42 / -1.75
45° (Net IR Corr.)	N/A	N/A
45° - 55° (Net IR Corr.)	N/A	N/A
Composite (Net IR Corr.)	N/A	N/A

† Valid incident angle ranges:

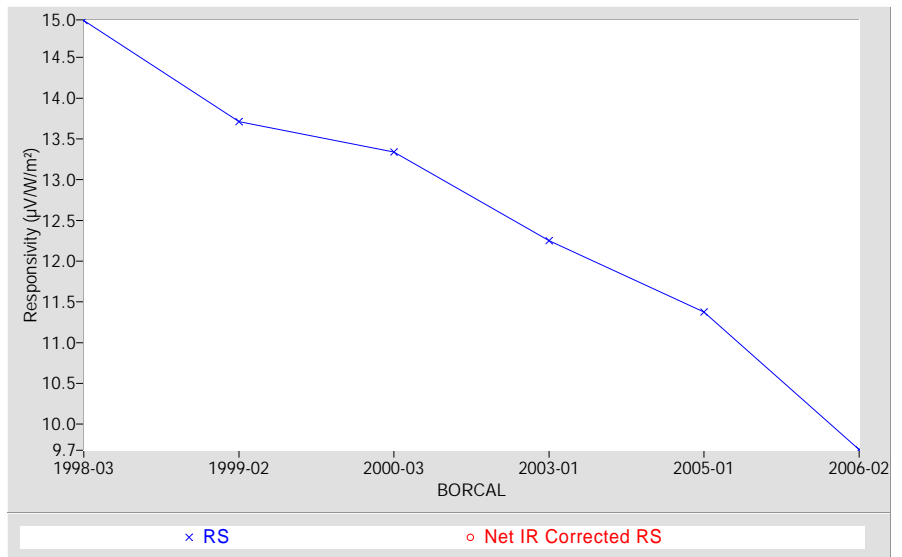
45°: 30.0° to 60.0°

45° - 55°: 45.0° to 55.0°

Composite: 16.3° to 79.0°

The instrument responsivity at  $I = 45^\circ$  may be used to monitor instrument stability. The instrument's history at  $I = 45^\circ$  is shown in Figure 2.

**Figure 2. History of instrument at  $I = 45^\circ$**



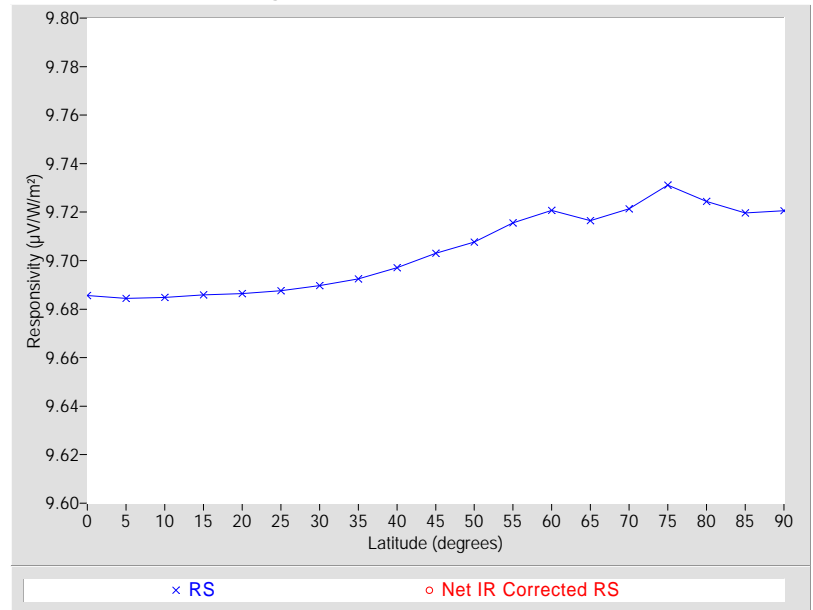
#### 5. Latitude Optimized Responsivity: See Note 1 below.

**Table 4. Latitude Optimized Responsivities**

Latitude	RS ( $\mu\text{V/W/m}^2$ )	Error estimate* (%)	RSc ( $\mu\text{V/W/m}^2$ ) Net IR Corr.	Error estimate* (%) Net IR Corr.
0	9.6856	+7.12 / -7.44	N/A	N/A
5	9.6845	+7.14 / -7.43	N/A	N/A
10	9.6848	+7.13 / -7.43	N/A	N/A
15	9.6859	+7.12 / -7.44	N/A	N/A
20	9.6864	+7.12 / -7.44	N/A	N/A
25	9.6876	+7.10 / -7.46	N/A	N/A
30	9.6897	+7.08 / -7.48	N/A	N/A
35	9.6925	+7.05 / -7.50	N/A	N/A
40	9.6971	+7.00 / -7.55	N/A	N/A
45	9.7030	+6.94 / -7.60	N/A	N/A
50	9.7076	+6.89 / -7.64	N/A	N/A
55	9.7156	+6.80 / -7.72	N/A	N/A
60	9.7208	+6.74 / -7.77	N/A	N/A
65	9.7164	+6.79 / -7.73	N/A	N/A
70	9.7214	+6.74 / -7.77	N/A	N/A
75	9.7312	+6.63 / -7.86	N/A	N/A
80	9.7244	+6.70 / -7.80	N/A	N/A
85	9.7196	+6.76 / -7.76	N/A	N/A
90	9.7205	+6.75 / -7.77	N/A	N/A

\* Uncertainty is undefined

**Figure 3. Latitude Optimized Responsivities**



#### Application of the responsivities and uncertainties:

The responsivities above are applied according to equation [1]:

##### Example

Instrument responsivity (RS) =  $7.34 \mu\text{V/W/m}^2 \pm 2.7\%$

Instrument output voltage (V) =  $0.00624 \text{ V}$  ( $6240 \mu\text{V}$ )

Irradiance (IRR) =  $V / RS = 6240 / 7.34 = 850.1 \text{ W/m}^2 \pm 2.7\%$

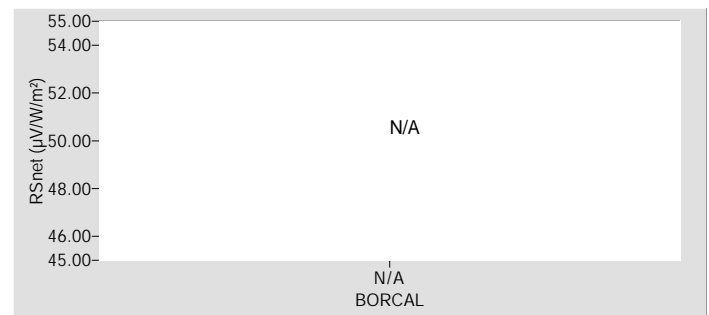
Thus, at the 95% confidence level, the irradiance lies between 827.1 and 873.1  $\text{W/m}^2$

##### Note 1:

All above methods, in conjunction with knowledge of the net infrared and sky irradiance distribution, may be used to determine the effective instrument responsivity with less uncertainties.

#### Instrument's Effective Net Infrared History (RSnet):

**Figure 4. Instrument's RSnet History**



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate

**Test Instrument:** Silicon Pyranometer **Manufacturer:** Licor

**Model:** LI200 **Serial Number:** PY1744

**Calibration Date:** 6/17/2006 **Due Date:** 6/17/2007

**Customer:** NREL-SRRL-BMS **Calibration Site Parameters:** see Ancillary Data

**Environmental Conditions:** Outdoors, under natural sunlight (see Ancillary Data)

**Data Acquisition Dates:** 6/11-12, 6/17

Table 1. Traceability

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppeley Absolute Cavity Radiometer Model HF, S/N 31104	03/14/2006	03/14/2007
Diffuse Irradiance †	Eppeley Black and White Pyranometer Model 8-48, S/N 32858	04/05/2006	04/05/2007
Diffuse Irradiance †	Eppeley Black and White Pyranometer Model 8-48, S/N 32871	04/05/2006	04/05/2007
Data Acquisition ‡	NREL Data Proof Scanner System Model RAP-DAQ, S/N 2005-998	11/22/2005	11/22/2006
Data Acquisition ‡	NREL Data Proof Scanner System Model RAP-DAQ, S/N 2005-999	11/22/2005	11/22/2006

† Traceable to the World Radiometric Reference

‡ Traceable to the National Institute of Standards and Technology

**Number of pages of certificate:** 4

**Calibration Procedure:** [1] Myers, D., Stoffel, T., Reda, I., Wilcox, S., and Andreas, A., 2002, "Recent Progress in Reducing the Uncertainty in and Improving Pyranometer Calibrations." Journal of Solar Energy Engineering, vol. 124, pp. 44-50. The American Society of Mechanical Engineers, Transactions of the ASME.  
[2] "Improved Methods for Broadband Outdoor Radiometer Calibration (BORCAL)," Wilcox, S., Andreas, A., Reda, I., and Myers, D., Proceedings of the ARM Science Team Meeting, St. Petersburg, Florida, April 2002. Available upon request.

This calibration certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval by the calibration facility. Calibration certificates without signatures are not valid.

**Calibrated by:** Ibrahim Reda and Steve Wilcox

**Certified by:**

-----  
Afshin M. Andreas

Title: Scientist II

Date: -----

**Quality Assured by:**

-----  
Daryl R. Myers

Title: Senior Scientist II

Date: -----

# Calibration Results

## PY1744 Licor LI200

Figure 1. Responsivity vs Incident Angle

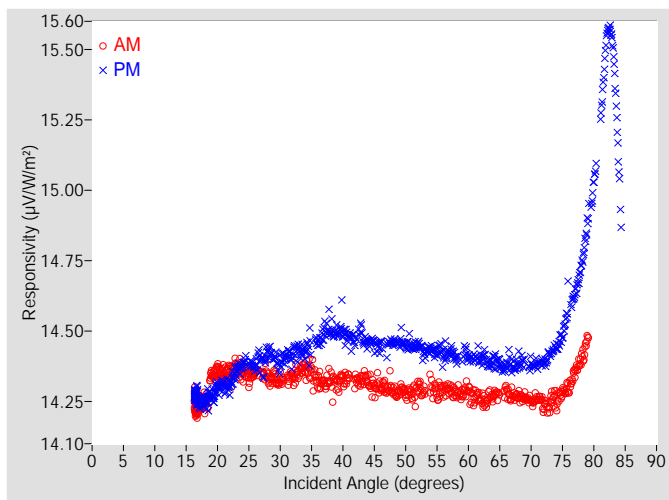


Figure 2. Responsivity vs Local Standard Time

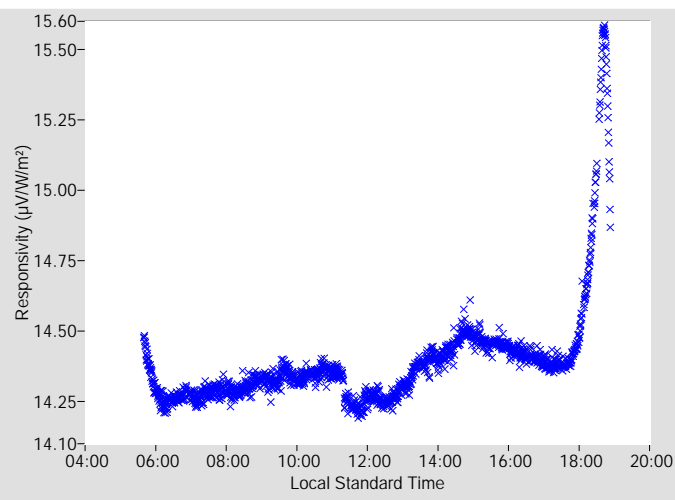


Table 2. Calibration Label Values

RS @ 45° (µV/W/m²) ‡	U95 (%) †	Tilt / Azm
14.379	+2.13 / -1.54	0.0° / 0.0°

† Valid incident angle range: 30.0° to 60.0°

‡ Estimated thermal offset error during calibration is unspecified.

Table 3. Instrument Responsivity (RS) and Calibration Uncertainty (U95)

Inc. Angle†	AM			PM			Inc. Angle†	AM			PM		
	RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡	RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡		RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡	RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡
0	N/A	N/A	N/A	N/A	N/A	N/A	46	14.298	0.61	95.26	14.447	0.56	265.16
2	N/A	N/A	N/A	N/A	N/A	N/A	48	14.290	0.64	93.44	14.460	0.53	266.89
4	N/A	N/A	N/A	N/A	N/A	N/A	50	14.280	0.59	91.68	14.450	0.60	268.66
6	N/A	N/A	N/A	N/A	N/A	N/A	52	14.303	0.65	90.02	14.452	0.59	270.36
8	N/A	N/A	N/A	N/A	N/A	N/A	54	14.311	0.66	88.32	14.434	0.58	271.97
10	N/A	N/A	N/A	N/A	N/A	N/A	56	14.291	0.65	86.74	14.410	0.66	273.56
12	N/A	N/A	N/A	N/A	N/A	N/A	58	14.278	0.65	85.16	14.405	0.63	275.17
14	N/A	N/A	N/A	N/A	N/A	N/A	60	14.290	0.72	83.64	14.406	0.65	276.69
16	N/A	N/A	N/A	N/A	N/A	N/A	62	14.261	0.72	82.10	14.400	0.68	278.24
18	14.258	0.67	152.33	14.251	0.53	207.38	64	14.270	0.75	80.57	14.397	0.70	279.74
20	14.359	0.54	142.39	14.300	0.53	219.28	66	14.285	0.80	79.02	14.376	0.76	281.29
22	14.351	0.61	134.11	14.310	0.57	227.28	68	14.267	0.84	77.52	14.385	0.79	282.79
24	14.353	0.57	127.83	14.379	0.51	233.24	70	14.252	0.92	75.98	14.380	0.84	284.32
26	14.351	0.54	122.65	14.376	0.55	238.24	72	14.234	0.99	74.51	14.389	0.90	285.86
28	14.337	0.56	118.43	14.425	0.61	242.40	74	14.256	1.09	72.99	14.441	1.00	287.46
30	14.323	0.52	114.73	14.384	0.54	245.97	76	14.300	1.23	71.40	14.620	1.27	288.86
32	14.335	0.56	111.44	14.413	0.56	249.15	78	14.405	1.42	69.77	14.736	1.54	290.64
34	14.363	0.56	108.50	14.431	0.67	251.99	80	N/A	N/A	N/A	15.028	1.63	292.25
36	14.325	0.63	105.91	14.459	0.53	254.62	82	N/A	N/A	N/A	15.533	2.11	293.96
38	14.330	0.65	103.49	14.516	0.60	257.04	84	N/A	N/A	N/A	15.085	3.18	295.66
40	14.328	0.56	101.23	14.515	0.74	259.22	86	N/A	N/A	N/A	N/A	N/A	N/A
42	14.326	0.54	99.09	14.469	0.61	261.22	88	N/A	N/A	N/A	N/A	N/A	N/A
44	14.317	0.61	97.11	14.458	0.55	263.23	90	N/A	N/A	N/A	N/A	N/A	N/A

† Angle of incidence (degrees)

‡ Average azimuth angle for ±0.3° of incidence angle

N/A - Not Available

# Effective Net Infrared Corrected Calibration Results

## PY1744 Licor LI200

Figure 3. Responsivity vs Incident Angle

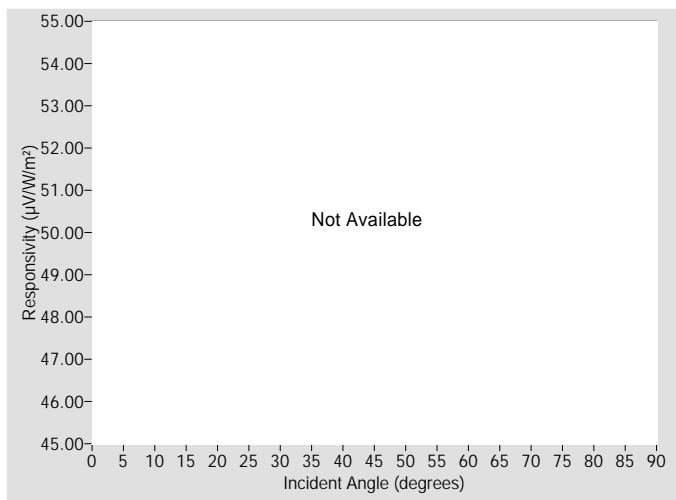


Figure 4. Responsivity vs Local Standard Time

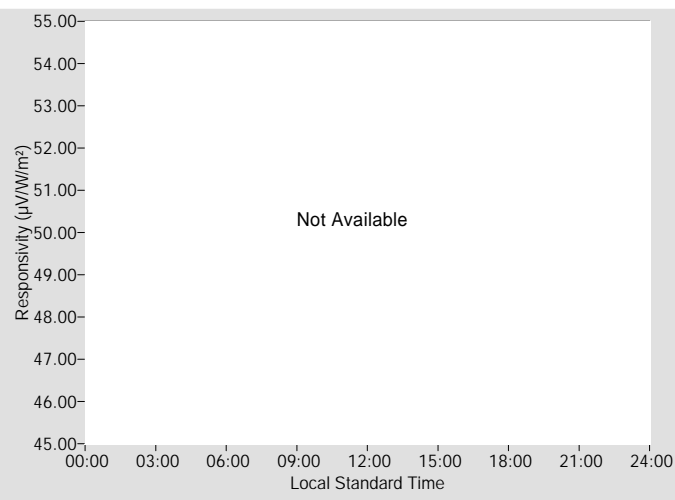


Table 4. Net IR Corrected Calibration Label Values

RSc @ 45° (µV/W/m²) ‡	U95 (%) †	Tilt / Azm
N/A	N/A	0.0° / 0.0°

† Valid incident angle range: N/A

‡ RSnet = N/A

Table 5. Net IR Corrected Instrument Responsivity (RS) and Calibration Uncertainty (U95)

Inc. Angle†	AM			PM			Inc. Angle†	AM			PM		
	RSc (µV/W/m²)	U95 ± (%)	Azm. Angle‡	RSc (µV/W/m²)	U95 ± (%)	Azm. Angle‡		RSc (µV/W/m²)	U95 ± (%)	Azm. Angle‡	RSc (µV/W/m²)	U95 ± (%)	Azm. Angle‡
0	N/A	N/A	N/A	N/A	N/A	N/A	46	N/A	N/A	N/A	N/A	N/A	N/A
2	N/A	N/A	N/A	N/A	N/A	N/A	48	N/A	N/A	N/A	N/A	N/A	N/A
4	N/A	N/A	N/A	N/A	N/A	N/A	50	N/A	N/A	N/A	N/A	N/A	N/A
6	N/A	N/A	N/A	N/A	N/A	N/A	52	N/A	N/A	N/A	N/A	N/A	N/A
8	N/A	N/A	N/A	N/A	N/A	N/A	54	N/A	N/A	N/A	N/A	N/A	N/A
10	N/A	N/A	N/A	N/A	N/A	N/A	56	N/A	N/A	N/A	N/A	N/A	N/A
12	N/A	N/A	N/A	N/A	N/A	N/A	58	N/A	N/A	N/A	N/A	N/A	N/A
14	N/A	N/A	N/A	N/A	N/A	N/A	60	N/A	N/A	N/A	N/A	N/A	N/A
16	N/A	N/A	N/A	N/A	N/A	N/A	62	N/A	N/A	N/A	N/A	N/A	N/A
18	N/A	N/A	N/A	N/A	N/A	N/A	64	N/A	N/A	N/A	N/A	N/A	N/A
20	N/A	N/A	N/A	N/A	N/A	N/A	66	N/A	N/A	N/A	N/A	N/A	N/A
22	N/A	N/A	N/A	N/A	N/A	N/A	68	N/A	N/A	N/A	N/A	N/A	N/A
24	N/A	N/A	N/A	N/A	N/A	N/A	70	N/A	N/A	N/A	N/A	N/A	N/A
26	N/A	N/A	N/A	N/A	N/A	N/A	72	N/A	N/A	N/A	N/A	N/A	N/A
28	N/A	N/A	N/A	N/A	N/A	N/A	74	N/A	N/A	N/A	N/A	N/A	N/A
30	N/A	N/A	N/A	N/A	N/A	N/A	76	N/A	N/A	N/A	N/A	N/A	N/A
32	N/A	N/A	N/A	N/A	N/A	N/A	78	N/A	N/A	N/A	N/A	N/A	N/A
34	N/A	N/A	N/A	N/A	N/A	N/A	80	N/A	N/A	N/A	N/A	N/A	N/A
36	N/A	N/A	N/A	N/A	N/A	N/A	82	N/A	N/A	N/A	N/A	N/A	N/A
38	N/A	N/A	N/A	N/A	N/A	N/A	84	N/A	N/A	N/A	N/A	N/A	N/A
40	N/A	N/A	N/A	N/A	N/A	N/A	86	N/A	N/A	N/A	N/A	N/A	N/A
42	N/A	N/A	N/A	N/A	N/A	N/A	88	N/A	N/A	N/A	N/A	N/A	N/A
44	N/A	N/A	N/A	N/A	N/A	N/A	90	N/A	N/A	N/A	N/A	N/A	N/A

† Angle of incidence (degrees)

‡ Average azimuth angle for ±0.3° of incidence angle

N/A - Not Available

# Suggested Methods of Applying Calibration Results

## PY1744 Licor LI200

Listed below are the results for the methods documented in "Improved Methods for Broadband Outdoor Radiometer Calibration (BORCAL)," Wilcox et al., Proceedings of the ARM Science Team Meeting, St. Petersburg, Florida, April 2002. Computing the net infrared corrected solar irradiance is documented in "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error during Outdoor Calibration using the Component Sum Method," Reda et al., Journal of Atmospheric and Oceanic Technology V. 22 (10), pp. 1531-1540, October 2005.

In all cases, the solar irradiance is calculated from the instrument responsivity using one of these equations:

$$IRR = V / RS \quad [1]$$

$$IRR (corr.) = (V - W_{net} * RS_{net}) / RS_c \quad [2]$$

where,

$IRR$  = solar irradiance (Watts per square meter),

$V$  = radiometer output voltage (microvolts),

$RS$  = responsivity of the radiometer ( $\mu V/W/m^2$ ),

$IRR (corr.)$  = effective net infrared corrected solar irradiance ( $W/m^2$ ),

$W_{net}$  = effective net infrared measured by pyrgeometer ( $W/m^2$ ),

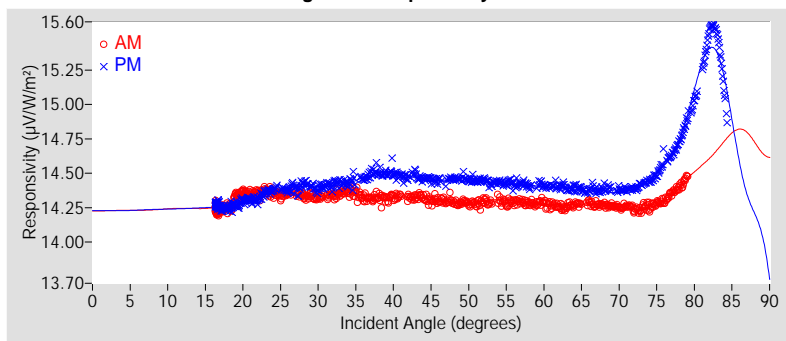
$RS_{net}$  = pyranometer net infrared response ( $\mu V/W/m^2$ ), see Table 4,

$RS_c$  = effective net infrared corrected responsivity ( $\mu V/W/m^2$ ).

**1. Two-degree Responsivities:** Responsivities are obtained from Certificate Table 3 or 5. See Note 1 on next page.

**2. AM and PM Responsivity Functions:** See Note 1 on next page.

Figure 1. Responsivity Function



$$RS (am) = \sum_{i=0}^n a_i \cdot \cos^i(I) \quad [3]$$

$$RS (pm) = \sum_{j=0}^m b_j \cdot \cos^j(I)$$

where the coefficients  $a_i$  and  $b_j$  are available upon request.

The quality of the function fit to data is shown in Figure 1 and 2.

Figure 2. Net IR Corrected Responsivity Function

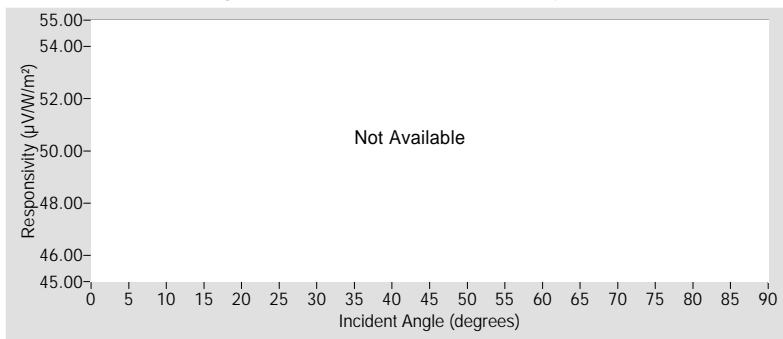


Table 1. Function Validity

	AM	PM
Uncertainty U95 (%)	±1.24	±1.24
R <sup>2</sup>	0.9999996	0.9999954
Valid incidence angle range	16.3° to 79.0°	16.3° to 84.3°
Net IR corr. uncert. U95 (%)	N/A	N/A
Net IR corrected R <sup>2</sup>	N/A	N/A
Corr. valid inc. angle range	N/A	N/A

**3. Nine-degree Bin Responsivity:** See Note 1 on next page.

Table 2. Nine-degree responsivities

Inc. Angle	Responsivity						Net IR Corr. Responsivity					
	AM		PM		Combined		AM		PM		Combined	
	RS ( $\mu V/W/m^2$ )	U95 (%)	RS ( $\mu V/W/m^2$ )	U95 (%)	RS ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)
0-9	14.230	*	14.230	*	14.230	*	N/A	N/A	N/A	N/A	N/A	N/A
9-18	14.247	*	14.246	*	14.246	*	N/A	N/A	N/A	N/A	N/A	N/A
18-27	14.341	±1.27	14.330	±1.33	14.335	±1.41	N/A	N/A	N/A	N/A	N/A	N/A
27-36	14.337	±1.24	14.413	±1.25	14.375	±1.40	N/A	N/A	N/A	N/A	N/A	N/A
36-45	14.326	±1.24	14.487	±1.26	14.407	±1.59	N/A	N/A	N/A	N/A	N/A	N/A
45-54	14.294	±1.24	14.450	±1.25	14.372	±1.53	N/A	N/A	N/A	N/A	N/A	N/A
54-63	14.285	±1.24	14.408	±1.24	14.347	±1.45	N/A	N/A	N/A	N/A	N/A	N/A
63-72	14.266	±1.24	14.383	±1.25	14.324	±1.46	N/A	N/A	N/A	N/A	N/A	N/A
72-81	14.345	*	14.667	±3.01	14.506	*	N/A	N/A	N/A	N/A	N/A	N/A
81-90	14.703	*	14.722	*	14.713	*	N/A	N/A	N/A	N/A	N/A	N/A

\* The responsivity is based on extrapolated data and the corresponding uncertainty is undefined.

#### 4. The Single Responsivities: See Note 1 below.

**Table 3. Single Responsivities**

Responsivity Characterization	RS ( $\mu\text{V/W/m}^2$ )	U95 † (%)
45°	14.379	+2.13 / -1.54
45° - 55°	14.371	±1.39
Composite	14.335	+7.62 / -1.42
45° (Net IR Corr.)	N/A	N/A
45° - 55° (Net IR Corr.)	N/A	N/A
Composite (Net IR Corr.)	N/A	N/A

† Valid incident angle ranges:

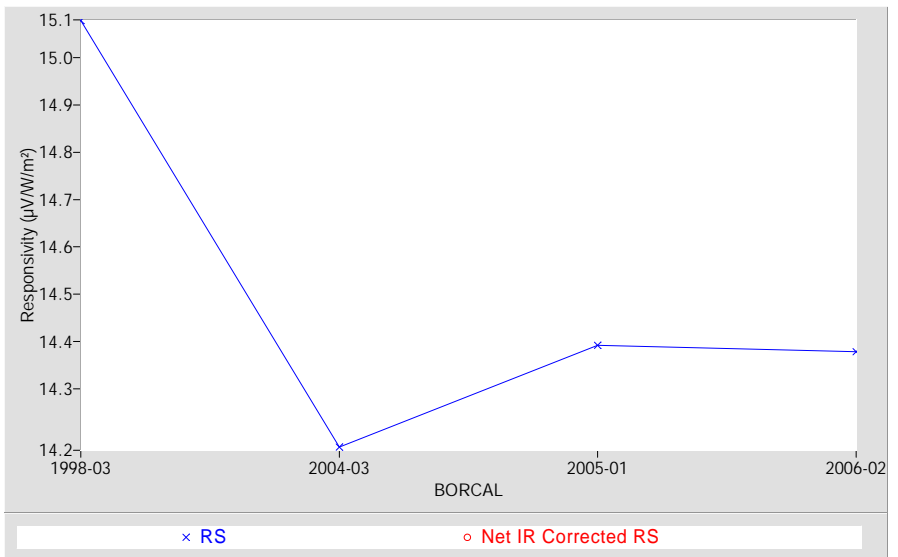
45°: 30.0° to 60.0°

45° - 55°: 45.0° to 55.0°

Composite: 16.3° to 79.0°

The instrument responsivity at  $I = 45^\circ$  may be used to monitor instrument stability. The instrument's history at  $I = 45^\circ$  is shown in Figure 2.

**Figure 2. History of instrument at  $I = 45^\circ$**



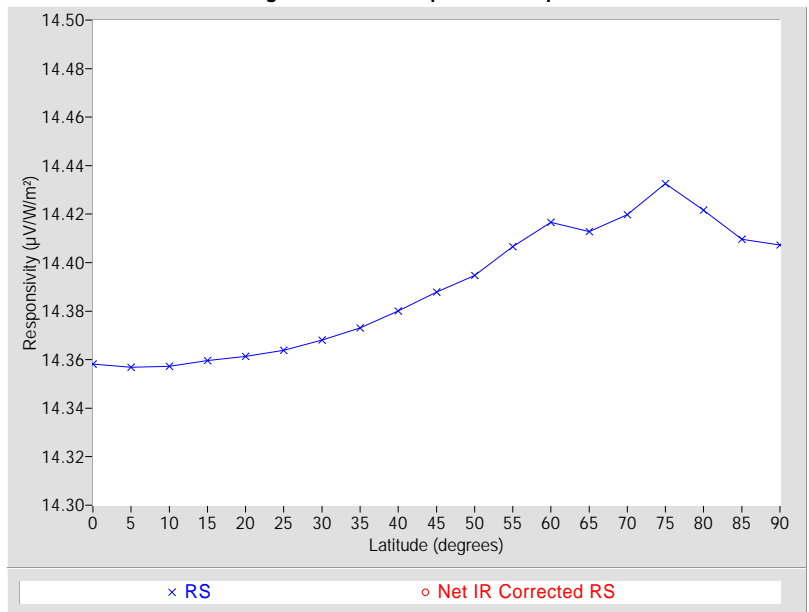
#### 5. Latitude Optimized Responsivity: See Note 1 below.

**Table 4. Latitude Optimized Responsivities**

Latitude	RS ( $\mu\text{V/W/m}^2$ )	Error estimate* (%)	RSc ( $\mu\text{V/W/m}^2$ )		Error estimate* (%)	
			Net IR Corr.	Net IR Corr.	Net IR Corr.	Net IR Corr.
0	14.358	+7.41 / -2.46	N/A	N/A	N/A	N/A
5	14.357	+7.42 / -2.45	N/A	N/A	N/A	N/A
10	14.357	+7.42 / -2.45	N/A	N/A	N/A	N/A
15	14.360	+7.40 / -2.47	N/A	N/A	N/A	N/A
20	14.361	+7.39 / -2.48	N/A	N/A	N/A	N/A
25	14.364	+7.37 / -2.49	N/A	N/A	N/A	N/A
30	14.368	+7.34 / -2.52	N/A	N/A	N/A	N/A
35	14.373	+7.30 / -2.55	N/A	N/A	N/A	N/A
40	14.380	+7.25 / -2.59	N/A	N/A	N/A	N/A
45	14.388	+7.20 / -2.63	N/A	N/A	N/A	N/A
50	14.395	+7.15 / -2.67	N/A	N/A	N/A	N/A
55	14.407	+7.06 / -2.75	N/A	N/A	N/A	N/A
60	14.417	+6.99 / -2.81	N/A	N/A	N/A	N/A
65	14.413	+7.01 / -2.78	N/A	N/A	N/A	N/A
70	14.420	+6.96 / -2.83	N/A	N/A	N/A	N/A
75	14.433	+6.87 / -2.90	N/A	N/A	N/A	N/A
80	14.422	+6.95 / -2.84	N/A	N/A	N/A	N/A
85	14.410	+7.04 / -2.77	N/A	N/A	N/A	N/A
90	14.407	+7.05 / -2.75	N/A	N/A	N/A	N/A

\* Uncertainty is undefined

**Figure 3. Latitude Optimized Responsivities**



#### Application of the responsivities and uncertainties:

The responsivities above are applied according to equation [1]:

##### Example

Instrument responsivity (RS) =  $7.34 \mu\text{V/W/m}^2 \pm 2.7\%$

Instrument output voltage (V) =  $0.00624 \text{ V}$  ( $6240 \mu\text{V}$ )

Irradiance (IRR) =  $V / RS = 6240 / 7.34 = 850.1 \text{ W/m}^2 \pm 2.7\%$

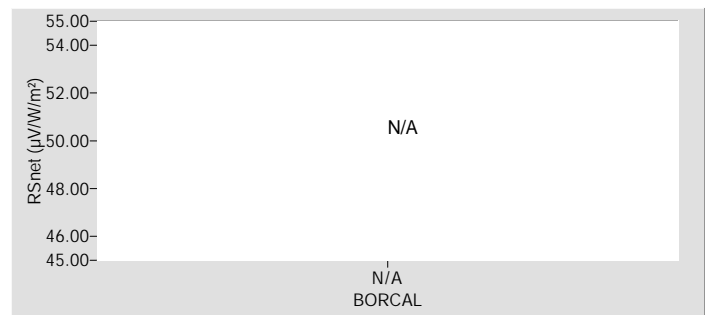
Thus, at the 95% confidence level, the irradiance lies between 827.1 and 873.1  $\text{W/m}^2$

##### Note 1:

All above methods, in conjunction with knowledge of the net infrared and sky irradiance distribution, may be used to determine the effective instrument responsivity with less uncertainties.

#### Instrument's Effective Net Infrared History (RSnet):

**Figure 4. Instrument's RSnet History**





# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate

**Test Instrument:** Silicon Pyranometer **Manufacturer:** Licor

**Model:** LI200 **Serial Number:** PY28244

**Calibration Date:** 6/17/2006 **Due Date:** 6/17/2007

**Customer:** NREL-SRRL-BMS **Calibration Site Parameters:** see Ancillary Data

**Environmental Conditions:** Outdoors, under natural sunlight (see Ancillary Data)

**Data Acquisition Dates:** 6/11-12, 6/17

Table 1. Traceability

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppeley Absolute Cavity Radiometer Model HF, S/N 31104	03/14/2006	03/14/2007
Diffuse Irradiance †	Eppeley Black and White Pyranometer Model 8-48, S/N 32858	04/05/2006	04/05/2007
Diffuse Irradiance †	Eppeley Black and White Pyranometer Model 8-48, S/N 32871	04/05/2006	04/05/2007
Data Acquisition ‡	NREL Data Proof Scanner System Model RAP-DAQ, S/N 2005-998	11/22/2005	11/22/2006
Data Acquisition ‡	NREL Data Proof Scanner System Model RAP-DAQ, S/N 2005-999	11/22/2005	11/22/2006

† Traceable to the World Radiometric Reference

‡ Traceable to the National Institute of Standards and Technology

**Number of pages of certificate:** 4

**Calibration Procedure:** [1] Myers, D., Stoffel, T., Reda, I., Wilcox, S., and Andreas, A., 2002, "Recent Progress in Reducing the Uncertainty in and Improving Pyranometer Calibrations." Journal of Solar Energy Engineering, vol. 124, pp. 44-50. The American Society of Mechanical Engineers, Transactions of the ASME. [2] "Improved Methods for Broadband Outdoor Radiometer Calibration (BORCAL)," Wilcox, S., Andreas, A., Reda, I., and Myers, D., Proceedings of the ARM Science Team Meeting, St. Petersburg, Florida, April 2002. Available upon request.

This calibration certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval by the calibration facility. Calibration certificates without signatures are not valid.

**Calibrated by:** Ibrahim Reda and Steve Wilcox

**Certified by:**

-----  
Afshin M. Andreas

Title: Scientist II

Date: -----

**Quality Assured by:**

-----  
Daryl R. Myers

Title: Senior Scientist II

Date: -----

# Calibration Results

PY28244 Licor LI200

Figure 1. Responsivity vs Incident Angle

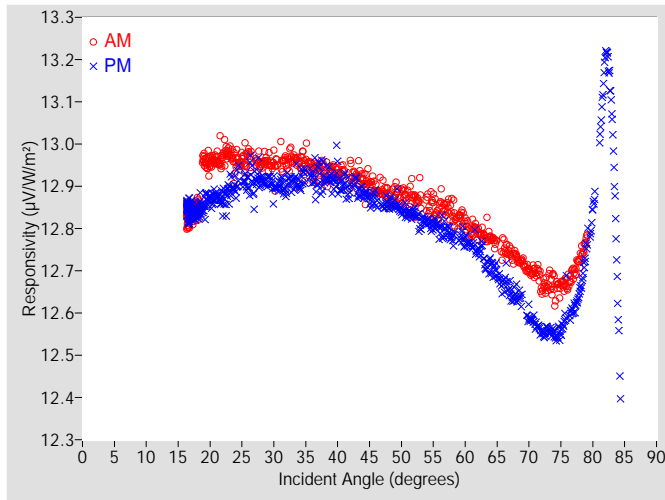


Figure 2. Responsivity vs Local Standard Time

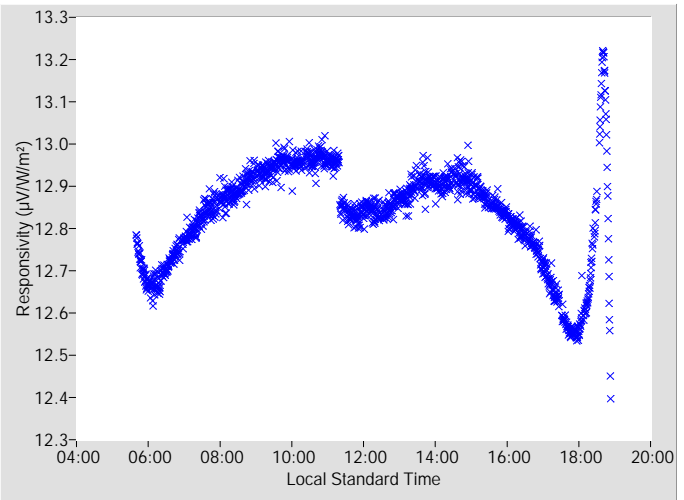


Table 2. Calibration Label Values

RS @ 45° (µV/W/m²) ‡	U95 (%) †	Tilt / Azm
12.889	+1.43 / -1.55	0.0° / 0.0°

† Valid incident angle range: 30.0° to 60.0°

‡ Estimated thermal offset error during calibration is unspecified.

Table 3. Instrument Responsivity (RS) and Calibration Uncertainty (U95)

Inc. Angle†	AM			PM			Inc. Angle†	AM			PM		
	RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡	RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡		RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡	RS (µV/W/m²)	U95 ± (%)	Azm. Angle‡
0	N/A	N/A	N/A	N/A	N/A	N/A	46	12.893	0.56	95.26	12.866	0.54	268.16
2	N/A	N/A	N/A	N/A	N/A	N/A	48	12.883	0.59	93.44	12.856	0.54	266.89
4	N/A	N/A	N/A	N/A	N/A	N/A	50	12.876	0.62	91.68	12.843	0.59	268.66
6	N/A	N/A	N/A	N/A	N/A	N/A	52	12.868	0.68	90.02	12.837	0.59	270.36
8	N/A	N/A	N/A	N/A	N/A	N/A	54	12.860	0.63	88.32	12.815	0.57	271.97
10	N/A	N/A	N/A	N/A	N/A	N/A	56	12.853	0.67	86.74	12.799	0.62	273.56
12	N/A	N/A	N/A	N/A	N/A	N/A	58	12.843	0.69	85.16	12.780	0.62	275.17
14	N/A	N/A	N/A	N/A	N/A	N/A	60	12.814	0.70	83.64	12.768	0.65	276.69
16	N/A	N/A	N/A	N/A	N/A	N/A	62	12.791	0.71	82.10	12.745	0.69	278.24
18	12.854	0.75	152.33	12.840	0.52	207.38	64	12.780	0.78	80.57	12.711	0.69	279.74
20	12.957	0.56	142.27	12.871	0.53	219.28	66	12.753	0.80	79.02	12.667	0.77	281.29
22	12.971	0.57	134.11	12.871	0.54	227.28	68	12.736	0.84	77.52	12.640	0.79	282.79
24	12.954	0.59	127.83	12.901	0.55	233.24	70	12.701	0.92	75.98	12.592	0.85	284.32
26	12.973	0.56	122.65	12.909	0.68	238.24	72	12.665	1.00	74.51	12.554	0.89	285.86
28	12.952	0.52	118.43	12.916	0.54	242.40	74	12.663	1.11	72.99	12.546	0.97	287.46
30	12.946	0.62	114.76	12.896	0.54	245.97	76	12.671	1.21	71.40	12.638	1.20	288.86
32	12.961	0.56	111.44	12.901	0.52	249.15	78	12.731	1.40	69.77	12.656	1.40	290.64
34	12.959	0.59	108.50	12.901	0.54	251.99	80	N/A	N/A	N/A	12.841	1.56	292.25
36	12.939	0.61	105.91	12.920	0.62	254.62	82	N/A	N/A	N/A	13.206	2.00	293.96
38	12.935	0.55	103.44	12.928	0.58	257.01	84	N/A	N/A	N/A	12.605	3.54	295.66
40	12.930	0.54	101.23	12.927	0.66	259.22	86	N/A	N/A	N/A	N/A	N/A	N/A
42	12.930	0.57	99.09	12.896	0.56	261.22	88	N/A	N/A	N/A	N/A	N/A	N/A
44	12.920	0.66	97.15	12.887	0.52	263.23	90	N/A	N/A	N/A	N/A	N/A	N/A

† Angle of incidence (degrees)

‡ Average azimuth angle for ±0.3° of incidence angle

N/A - Not Available

# Effective Net Infrared Corrected Calibration Results

## PY28244 Licor LI200

Figure 3. Responsivity vs Incident Angle

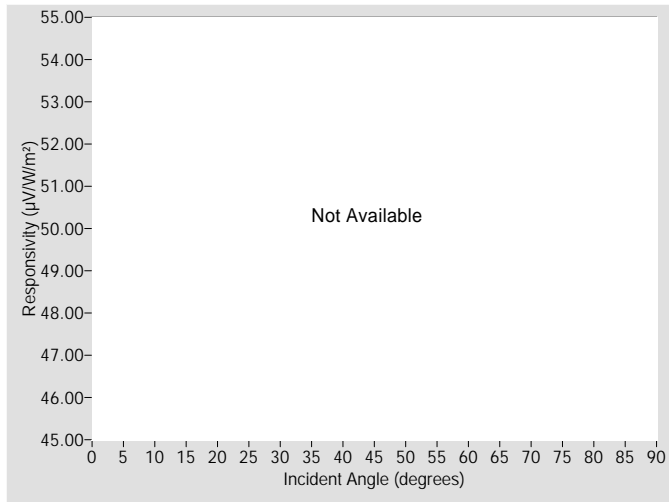


Figure 4. Responsivity vs Local Standard Time

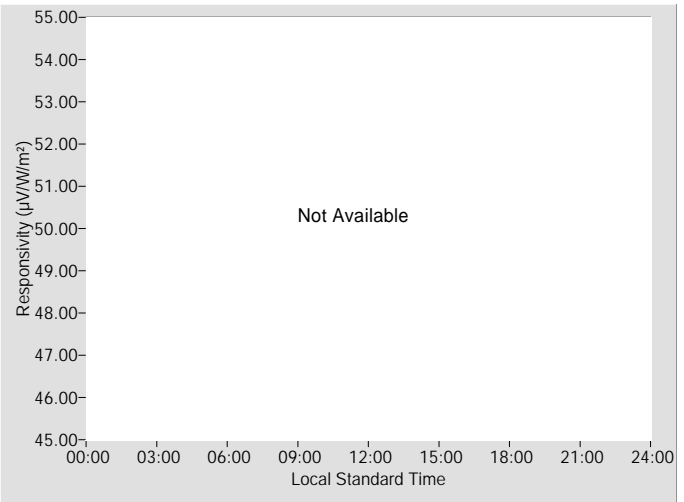


Table 4. Net IR Corrected Calibration Label Values

RSc @ 45° (μV/W/m²) ‡	U95 (%) †	Tilt / Azm
N/A	N/A	0.0° / 0.0°

† Valid incident angle range: N/A

‡ RSnet = N/A

Table 5. Net IR Corrected Instrument Responsivity (RS) and Calibration Uncertainty (U95)

Inc. Angle†	AM			PM			Inc. Angle†	AM			PM		
	RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡	RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡		RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡	RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡
0	N/A	N/A	N/A	N/A	N/A	N/A	46	N/A	N/A	N/A	N/A	N/A	N/A
2	N/A	N/A	N/A	N/A	N/A	N/A	48	N/A	N/A	N/A	N/A	N/A	N/A
4	N/A	N/A	N/A	N/A	N/A	N/A	50	N/A	N/A	N/A	N/A	N/A	N/A
6	N/A	N/A	N/A	N/A	N/A	N/A	52	N/A	N/A	N/A	N/A	N/A	N/A
8	N/A	N/A	N/A	N/A	N/A	N/A	54	N/A	N/A	N/A	N/A	N/A	N/A
10	N/A	N/A	N/A	N/A	N/A	N/A	56	N/A	N/A	N/A	N/A	N/A	N/A
12	N/A	N/A	N/A	N/A	N/A	N/A	58	N/A	N/A	N/A	N/A	N/A	N/A
14	N/A	N/A	N/A	N/A	N/A	N/A	60	N/A	N/A	N/A	N/A	N/A	N/A
16	N/A	N/A	N/A	N/A	N/A	N/A	62	N/A	N/A	N/A	N/A	N/A	N/A
18	N/A	N/A	N/A	N/A	N/A	N/A	64	N/A	N/A	N/A	N/A	N/A	N/A
20	N/A	N/A	N/A	N/A	N/A	N/A	66	N/A	N/A	N/A	N/A	N/A	N/A
22	N/A	N/A	N/A	N/A	N/A	N/A	68	N/A	N/A	N/A	N/A	N/A	N/A
24	N/A	N/A	N/A	N/A	N/A	N/A	70	N/A	N/A	N/A	N/A	N/A	N/A
26	N/A	N/A	N/A	N/A	N/A	N/A	72	N/A	N/A	N/A	N/A	N/A	N/A
28	N/A	N/A	N/A	N/A	N/A	N/A	74	N/A	N/A	N/A	N/A	N/A	N/A
30	N/A	N/A	N/A	N/A	N/A	N/A	76	N/A	N/A	N/A	N/A	N/A	N/A
32	N/A	N/A	N/A	N/A	N/A	N/A	78	N/A	N/A	N/A	N/A	N/A	N/A
34	N/A	N/A	N/A	N/A	N/A	N/A	80	N/A	N/A	N/A	N/A	N/A	N/A
36	N/A	N/A	N/A	N/A	N/A	N/A	82	N/A	N/A	N/A	N/A	N/A	N/A
38	N/A	N/A	N/A	N/A	N/A	N/A	84	N/A	N/A	N/A	N/A	N/A	N/A
40	N/A	N/A	N/A	N/A	N/A	N/A	86	N/A	N/A	N/A	N/A	N/A	N/A
42	N/A	N/A	N/A	N/A	N/A	N/A	88	N/A	N/A	N/A	N/A	N/A	N/A
44	N/A	N/A	N/A	N/A	N/A	N/A	90	N/A	N/A	N/A	N/A	N/A	N/A

† Angle of incidence (degrees)

‡ Average azimuth angle for ±0.3° of incidence angle

N/A - Not Available

## Suggested Methods of Applying Calibration Results

### PY28244 Licor LI200

Listed below are the results for the methods documented in "Improved Methods for Broadband Outdoor Radiometer Calibration (BORCAL)," Wilcox et al., Proceedings of the ARM Science Team Meeting, St. Petersburg, Florida, April 2002. Computing the net infrared corrected solar irradiance is documented in "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error during Outdoor Calibration using the Component Sum Method," Reda et al., Journal of Atmospheric and Oceanic Technology V. 22 (10), pp. 1531-1540, October 2005.

In all cases, the solar irradiance is calculated from the instrument responsivity using one of these equations:

$$IRR = V / RS \quad [1]$$

$$IRR (corr.) = (V - W_{net} * RS_{net}) / RS_{c} \quad [2]$$

where,

$IRR$  = solar irradiance (Watts per square meter),

$V$  = radiometer output voltage (microvolts),

$RS$  = responsivity of the radiometer ( $\mu V/W/m^2$ ),

$IRR (corr.)$  = effective net infrared corrected solar irradiance ( $W/m^2$ ),

$W_{net}$  = effective net infrared measured by pyrgeometer ( $W/m^2$ ),

$RS_{net}$  = pyranometer net infrared response ( $\mu V/W/m^2$ ), see Table 4,

$RS_{c}$  = effective net infrared corrected responsivity ( $\mu V/W/m^2$ ).

**1. Two-degree Responsivities:** Responsivities are obtained from Certificate Table 3 or 5. See Note 1 on next page.

**2. AM and PM Responsivity Functions:** See Note 1 on next page.

Figure 1. Responsivity Function

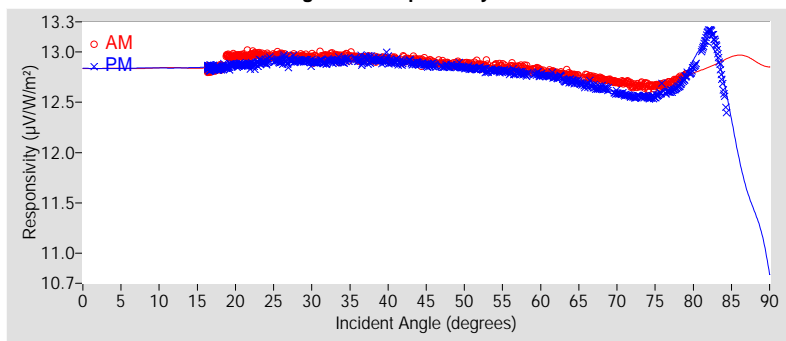
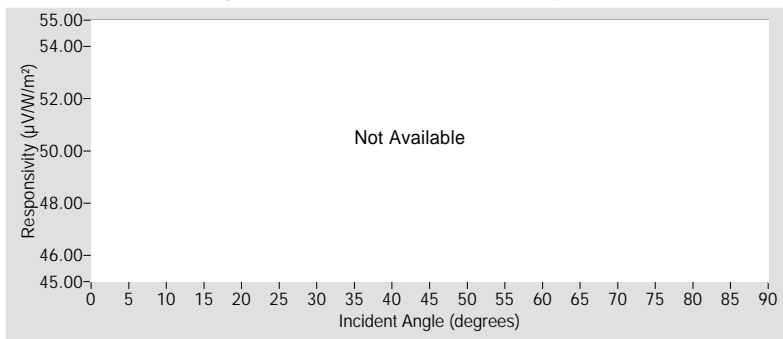


Figure 2. Net IR Corrected Responsivity Function



$$RS (am) = \sum_{i=0}^n a_i \cdot \cos^i(I) \quad [3]$$

$$RS (pm) = \sum_{j=0}^m b_j \cdot \cos^j(I)$$

where the coefficients  $a_i$  and  $b_j$  are available upon request.

The quality of the function fit to data is shown in Figure 1 and 2.

Table 1. Function Validity

	AM	PM
Uncertainty U95 (%)	±1.30	±1.30
R <sup>2</sup>	0.9999997	0.9999944
Valid incidence angle range	16.3° to 79.0°	16.3° to 84.3°
Net IR corr. uncert. U95 (%)	N/A	N/A
Net IR corrected R <sup>2</sup>	N/A	N/A
Corr. valid inc. angle range	N/A	N/A

**3. Nine-degree Bin Responsivity:** See Note 1 on next page.

Table 2. Nine-degree responsivities

Inc. Angle	Responsivity						Net IR Corr. Responsivity					
	AM		PM		Combined		AM		PM		Combined	
	RS ( $\mu V/W/m^2$ )	U95 (%)	RS ( $\mu V/W/m^2$ )	U95 (%)	RS ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)
0-9	12.836	*	12.837	*	12.837	*	N/A	N/A	N/A	N/A	N/A	N/A
9-18	12.844	*	12.843	*	12.844	*	N/A	N/A	N/A	N/A	N/A	N/A
18-27	12.949	±1.36	12.881	±1.32	12.915	±1.48	N/A	N/A	N/A	N/A	N/A	N/A
27-36	12.954	±1.30	12.904	±1.30	12.929	±1.34	N/A	N/A	N/A	N/A	N/A	N/A
36-45	12.930	±1.30	12.911	±1.32	12.921	±1.36	N/A	N/A	N/A	N/A	N/A	N/A
45-54	12.880	±1.31	12.848	±1.32	12.864	±1.40	N/A	N/A	N/A	N/A	N/A	N/A
54-63	12.832	±1.33	12.778	±1.34	12.805	±1.50	N/A	N/A	N/A	N/A	N/A	N/A
63-72	12.738	±1.37	12.646	±1.44	12.692	±1.79	N/A	N/A	N/A	N/A	N/A	N/A
72-81	12.704	*	12.662	±2.10	12.683	*	N/A	N/A	N/A	N/A	N/A	N/A
81-90	12.901	*	12.125	*	12.513	*	N/A	N/A	N/A	N/A	N/A	N/A

\* The responsivity is based on extrapolated data and the corresponding uncertainty is undefined.

#### 4. The Single Responsivities: See Note 1 below.

**Table 3. Single Responsivities**

Responsivity Characterization	RS ( $\mu\text{V/W/m}^2$ )	U95 † (%)
45°	12.889	+1.43 / -1.55
45° - 55°	12.860	±1.36
Composite	12.856	+2.19 / -2.60
45° (Net IR Corr.)	N/A	N/A
45° - 55° (Net IR Corr.)	N/A	N/A
Composite (Net IR Corr.)	N/A	N/A

† Valid incident angle ranges:

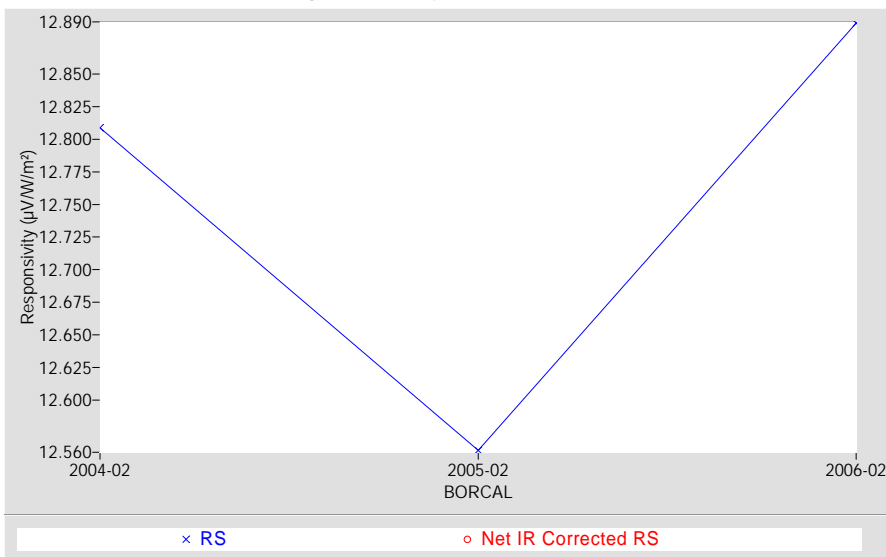
45°: 30.0° to 60.0°

45° - 55°: 45.0° to 55.0°

Composite: 16.3° to 79.0°

The instrument responsivity at  $I = 45^\circ$  may be used to monitor instrument stability. The instrument's history at  $I = 45^\circ$  is shown in Figure 2.

**Figure 2. History of instrument at  $I = 45^\circ$**



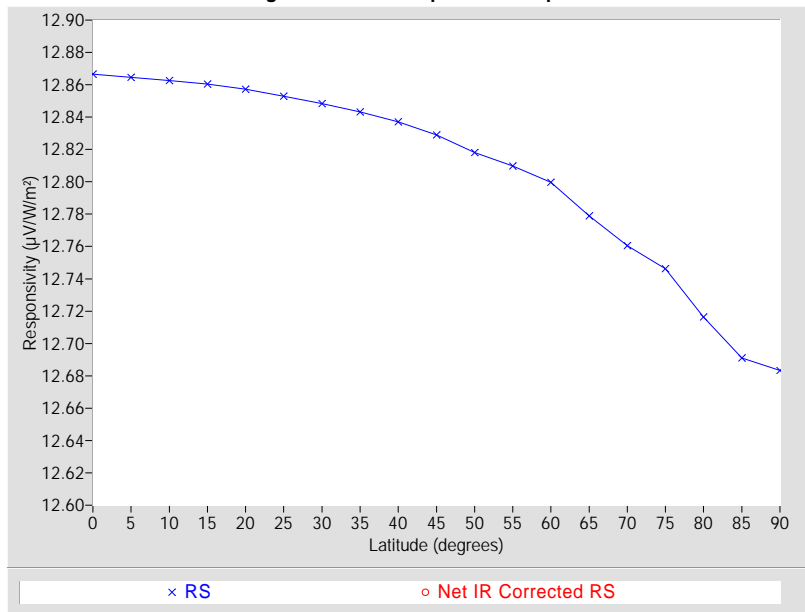
#### 5. Latitude Optimized Responsivity: See Note 1 below.

**Table 4. Latitude Optimized Responsivities**

Latitude	RS ( $\mu\text{V/W/m}^2$ )	Error estimate* (%)	RSc ( $\mu\text{V/W/m}^2$ )	Error estimate* (%)
			Net IR Corr.	Net IR Corr.
0	12.867	+2.12 / -13.12	N/A	N/A
5	12.865	+2.13 / -13.10	N/A	N/A
10	12.863	+2.14 / -13.09	N/A	N/A
15	12.861	+2.16 / -13.08	N/A	N/A
20	12.857	+2.18 / -13.05	N/A	N/A
25	12.853	+2.20 / -13.03	N/A	N/A
30	12.848	+2.23 / -12.99	N/A	N/A
35	12.843	+2.27 / -12.96	N/A	N/A
40	12.837	+2.31 / -12.92	N/A	N/A
45	12.829	+2.36 / -12.86	N/A	N/A
50	12.818	+2.43 / -12.79	N/A	N/A
55	12.810	+2.49 / -12.73	N/A	N/A
60	12.800	+2.56 / -12.66	N/A	N/A
65	12.779	+2.70 / -12.52	N/A	N/A
70	12.760	+2.83 / -12.40	N/A	N/A
75	12.746	+2.93 / -12.30	N/A	N/A
80	12.716	+3.15 / -12.10	N/A	N/A
85	12.691	+3.34 / -11.92	N/A	N/A
90	12.683	+3.40 / -11.87	N/A	N/A

\* Uncertainty is undefined

**Figure 3. Latitude Optimized Responsivities**



#### Application of the responsivities and uncertainties:

The responsivities above are applied according to equation [1]:

##### Example

Instrument responsivity (RS) =  $7.34 \mu\text{V/W/m}^2 \pm 2.7\%$

Instrument output voltage (V) =  $0.00624 \text{ V}$  ( $6240 \mu\text{V}$ )

Irradiance (IRR) =  $V / RS = 6240 / 7.34 = 850.1 \text{ W/m}^2 \pm 2.7\%$

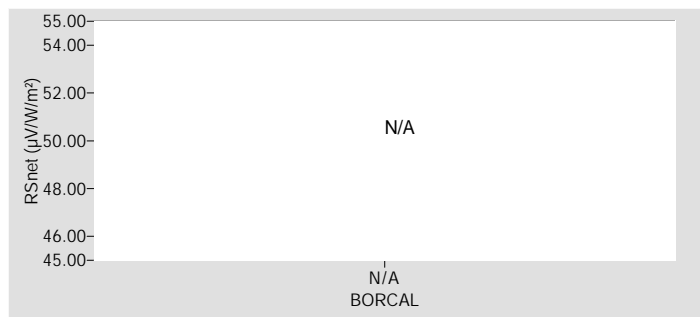
Thus, at the 95% confidence level, the irradiance lies between 827.1 and 873.1  $\text{W/m}^2$

##### Note 1:

All above methods, in conjunction with knowledge of the net infrared and sky irradiance distribution, may be used to determine the effective instrument responsivity with less uncertainties.

#### Instrument's Effective Net Infrared History (RSnet):

**Figure 4. Instrument's RSnet History**



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate

**Test Instrument:** Silicon Pyranometer      **Manufacturer:** Licor

**Model:** LI200      **Serial Number:** PY28257

**Calibration Date:** 6/17/2006      **Due Date:** 6/17/2007

**Customer:** NREL-SRRL-BMS      **Calibration Site Parameters:** see Ancillary Data

**Environmental Conditions:** Outdoors, under natural sunlight (see Ancillary Data)

**Data Acquisition Dates:** 6/11-12, 6/17

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppeley Absolute Cavity Radiometer Model HF, S/N 31104	03/14/2006	03/14/2007
Diffuse Irradiance †	Eppeley Black and White Pyranometer Model 8-48, S/N 32858	04/05/2006	04/05/2007
Diffuse Irradiance †	Eppeley Black and White Pyranometer Model 8-48, S/N 32871	04/05/2006	04/05/2007
Data Acquisition ‡	NREL Data Proof Scanner System Model RAP-DAQ, S/N 2005-998	11/22/2005	11/22/2006
Data Acquisition ‡	NREL Data Proof Scanner System Model RAP-DAQ, S/N 2005-999	11/22/2005	11/22/2006

† Traceable to the World Radiometric Reference

‡ Traceable to the National Institute of Standards and Technology

**Number of pages of certificate:** 4

**Calibration Procedure:** [1] Myers, D., Stoffel, T., Reda, I., Wilcox, S., and Andreas, A., 2002, "Recent Progress in Reducing the Uncertainty in and Improving Pyranometer Calibrations." Journal of Solar Energy Engineering, vol. 124, pp. 44-50. The American Society of Mechanical Engineers, Transactions of the ASME.  
[2] "Improved Methods for Broadband Outdoor Radiometer Calibration (BORCAL)," Wilcox, S., Andreas, A., Reda, I., and Myers, D., Proceedings of the ARM Science Team Meeting, St. Petersburg, Florida, April 2002. Available upon request.

This calibration certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval by the calibration facility. Calibration certificates without signatures are not valid.

**Calibrated by:** Ibrahim Reda and Steve Wilcox

**Certified by:**

-----  
Afshin M. Andreas

Title: Scientist II

Date: -----

**Quality Assured by:**

-----  
Daryl R. Myers

Title: Senior Scientist II

Date: -----

# Calibration Results

PY28257 Licor LI200

Figure 1. Responsivity vs Incident Angle

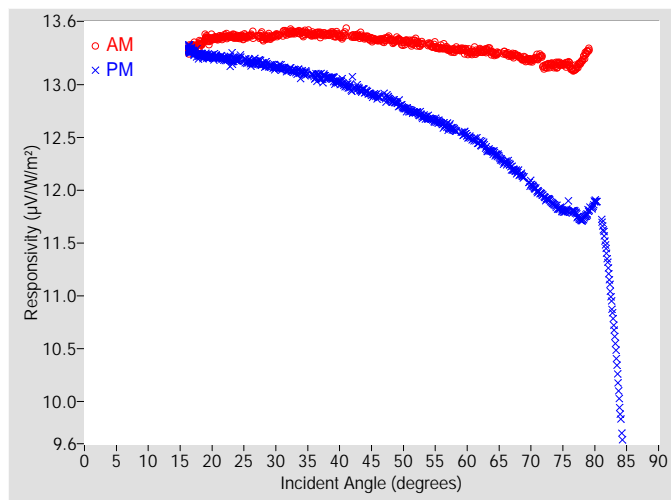


Figure 2. Responsivity vs Local Standard Time

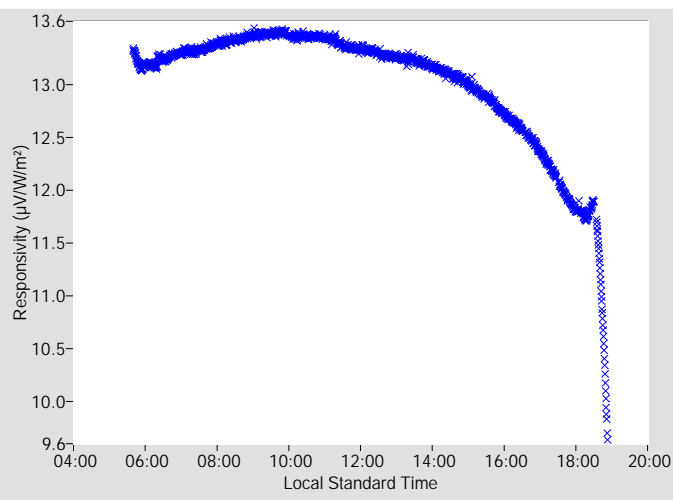


Table 2. Calibration Label Values

RS @ 45° (μV/W/m²) ‡	U95 (%) †	Tilt / Azm
13.167	+3.32 / -5.49	0.0° / 0.0°

† Valid incident angle range: 30.0° to 60.0°

‡ Estimated thermal offset error during calibration is unspecified.

Table 3. Instrument Responsivity (RS) and Calibration Uncertainty (U95)

Inc. Angle†	AM			PM			Inc. Angle†	AM			PM		
	RS (μV/W/m²)	U95 ± (%)	Azm. Angle‡	RS (μV/W/m²)	U95 ± (%)	Azm. Angle‡		RS (μV/W/m²)	U95 ± (%)	Azm. Angle‡	RS (μV/W/m²)	U95 ± (%)	Azm. Angle‡
0	N/A	N/A	N/A	N/A	N/A	N/A	46	13.423	0.55	95.26	12.885	0.56	265.16
2	N/A	N/A	N/A	N/A	N/A	N/A	48	13.429	0.60	93.44	12.856	0.61	266.89
4	N/A	N/A	N/A	N/A	N/A	N/A	50	13.394	0.60	91.68	12.784	0.69	268.66
6	N/A	N/A	N/A	N/A	N/A	N/A	52	13.409	0.63	90.02	12.737	0.63	270.36
8	N/A	N/A	N/A	N/A	N/A	N/A	54	13.384	0.62	88.32	12.682	0.62	271.97
10	N/A	N/A	N/A	N/A	N/A	N/A	56	13.352	0.64	86.78	12.627	0.69	273.56
12	N/A	N/A	N/A	N/A	N/A	N/A	58	13.328	0.65	85.16	12.571	0.65	275.17
14	N/A	N/A	N/A	N/A	N/A	N/A	60	13.322	0.69	83.64	12.513	0.70	276.69
16	N/A	N/A	N/A	N/A	N/A	N/A	62	13.320	0.74	82.10	12.445	0.75	278.24
18	13.383	0.71	152.33	13.281	0.57	207.38	64	13.299	0.78	80.57	12.362	0.73	279.74
20	13.439	0.63	142.39	13.264	0.52	219.28	66	13.298	0.79	79.02	12.260	0.87	281.29
22	13.460	0.54	134.11	13.244	0.60	227.28	68	13.270	0.86	77.52	12.163	0.89	282.79
24	13.452	0.52	127.83	13.236	0.56	233.24	70	13.231	0.94	75.98	12.056	0.93	284.32
26	13.466	0.55	122.75	13.216	0.54	238.24	72	13.187	1.10	74.51	11.942	0.96	285.86
28	13.449	0.58	118.35	13.190	0.54	242.40	74	13.187	1.08	72.99	11.837	1.04	287.46
30	13.469	0.52	114.73	13.164	0.52	245.97	76	13.190	1.24	71.40	11.849	1.17	288.86
32	13.488	0.55	111.44	13.139	0.51	249.15	78	13.232	1.51	69.77	11.721	1.33	290.64
34	13.494	0.54	108.56	13.110	0.59	251.99	80	N/A	N/A	N/A	11.885	1.52	292.25
36	13.476	0.56	105.91	13.082	0.57	254.62	82	N/A	N/A	N/A	11.307	4.80	293.96
38	13.476	0.52	103.44	13.067	0.60	257.01	84	N/A	N/A	N/A	9.9136	5.76	295.66
40	13.464	0.57	101.23	13.027	0.60	259.20	86	N/A	N/A	N/A	N/A	N/A	N/A
42	13.459	0.60	99.09	12.991	0.73	261.13	88	N/A	N/A	N/A	N/A	N/A	N/A
44	13.448	0.59	97.11	12.940	0.58	263.23	90	N/A	N/A	N/A	N/A	N/A	N/A

† Angle of incidence (degrees)

‡ Average azimuth angle for ±0.3° of incidence angle

N/A - Not Available

# Effective Net Infrared Corrected Calibration Results

## PY28257 Licor LI200

Figure 3. Responsivity vs Incident Angle

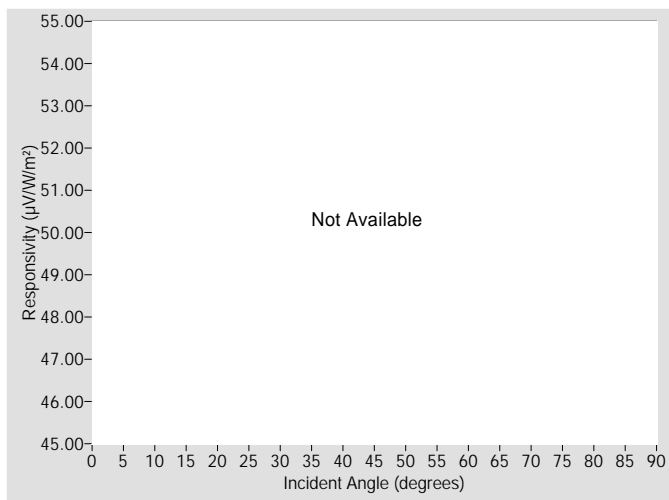


Figure 4. Responsivity vs Local Standard Time

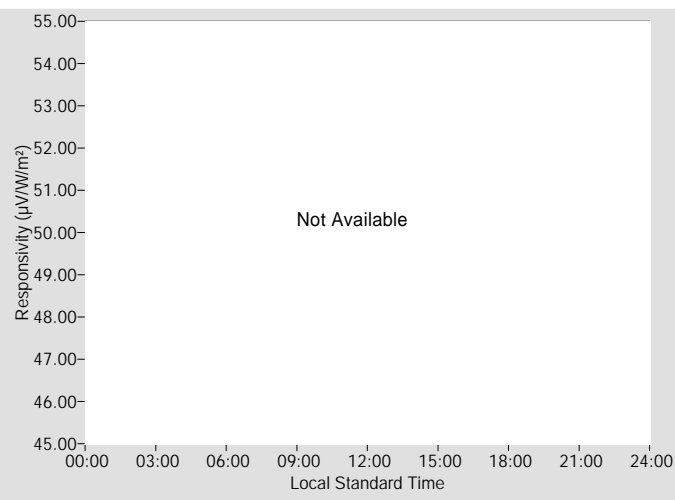


Table 4. Net IR Corrected Calibration Label Values

RSc @ 45° (μV/W/m²) ‡	U95 (%) †	Tilt / Azm
N/A	N/A	0.0° / 0.0°

† Valid incident angle range: N/A

‡ RSnet = N/A

Table 5. Net IR Corrected Instrument Responsivity (RS) and Calibration Uncertainty (U95)

Inc. Angle†	AM			PM			Inc. Angle†	AM			PM		
	RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡	RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡		RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡	RSc (μV/W/m²)	U95 ± (%)	Azm. Angle‡
0	N/A	N/A	N/A	N/A	N/A	N/A	46	N/A	N/A	N/A	N/A	N/A	N/A
2	N/A	N/A	N/A	N/A	N/A	N/A	48	N/A	N/A	N/A	N/A	N/A	N/A
4	N/A	N/A	N/A	N/A	N/A	N/A	50	N/A	N/A	N/A	N/A	N/A	N/A
6	N/A	N/A	N/A	N/A	N/A	N/A	52	N/A	N/A	N/A	N/A	N/A	N/A
8	N/A	N/A	N/A	N/A	N/A	N/A	54	N/A	N/A	N/A	N/A	N/A	N/A
10	N/A	N/A	N/A	N/A	N/A	N/A	56	N/A	N/A	N/A	N/A	N/A	N/A
12	N/A	N/A	N/A	N/A	N/A	N/A	58	N/A	N/A	N/A	N/A	N/A	N/A
14	N/A	N/A	N/A	N/A	N/A	N/A	60	N/A	N/A	N/A	N/A	N/A	N/A
16	N/A	N/A	N/A	N/A	N/A	N/A	62	N/A	N/A	N/A	N/A	N/A	N/A
18	N/A	N/A	N/A	N/A	N/A	N/A	64	N/A	N/A	N/A	N/A	N/A	N/A
20	N/A	N/A	N/A	N/A	N/A	N/A	66	N/A	N/A	N/A	N/A	N/A	N/A
22	N/A	N/A	N/A	N/A	N/A	N/A	68	N/A	N/A	N/A	N/A	N/A	N/A
24	N/A	N/A	N/A	N/A	N/A	N/A	70	N/A	N/A	N/A	N/A	N/A	N/A
26	N/A	N/A	N/A	N/A	N/A	N/A	72	N/A	N/A	N/A	N/A	N/A	N/A
28	N/A	N/A	N/A	N/A	N/A	N/A	74	N/A	N/A	N/A	N/A	N/A	N/A
30	N/A	N/A	N/A	N/A	N/A	N/A	76	N/A	N/A	N/A	N/A	N/A	N/A
32	N/A	N/A	N/A	N/A	N/A	N/A	78	N/A	N/A	N/A	N/A	N/A	N/A
34	N/A	N/A	N/A	N/A	N/A	N/A	80	N/A	N/A	N/A	N/A	N/A	N/A
36	N/A	N/A	N/A	N/A	N/A	N/A	82	N/A	N/A	N/A	N/A	N/A	N/A
38	N/A	N/A	N/A	N/A	N/A	N/A	84	N/A	N/A	N/A	N/A	N/A	N/A
40	N/A	N/A	N/A	N/A	N/A	N/A	86	N/A	N/A	N/A	N/A	N/A	N/A
42	N/A	N/A	N/A	N/A	N/A	N/A	88	N/A	N/A	N/A	N/A	N/A	N/A
44	N/A	N/A	N/A	N/A	N/A	N/A	90	N/A	N/A	N/A	N/A	N/A	N/A

† Angle of incidence (degrees)

‡ Average azimuth angle for ±0.3° of incidence angle

N/A - Not Available



## Suggested Methods of Applying Calibration Results

### PY28257 Licor LI200

Listed below are the results for the methods documented in "Improved Methods for Broadband Outdoor Radiometer Calibration (BORCAL)," Wilcox et al., Proceedings of the ARM Science Team Meeting, St. Petersburg, Florida, April 2002. Computing the net infrared corrected solar irradiance is documented in "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error during Outdoor Calibration using the Component Sum Method," Reda et al., Journal of Atmospheric and Oceanic Technology V. 22 (10), pp. 1531-1540, October 2005.

In all cases, the solar irradiance is calculated from the instrument responsivity using one of these equations:

$$IRR = V / RS \quad [1]$$

$$IRR (corr.) = (V - W_{net} * RS_{net}) / RS_{c} \quad [2]$$

where,

$IRR$  = solar irradiance (Watts per square meter),

$V$  = radiometer output voltage (microvolts),

$RS$  = responsivity of the radiometer ( $\mu V/W/m^2$ ),

$IRR (corr.)$  = effective net infrared corrected solar irradiance ( $W/m^2$ ),

$W_{net}$  = effective net infrared measured by pyrgeometer ( $W/m^2$ ),

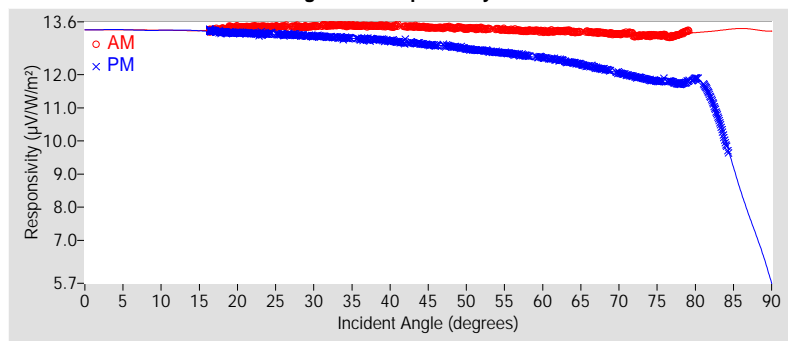
$RS_{net}$  = pyranometer net infrared response ( $\mu V/W/m^2$ ), see Table 4,

$RS_{c}$  = effective net infrared corrected responsivity ( $\mu V/W/m^2$ ).

**1. Two-degree Responsivities:** Responsivities are obtained from Certificate Table 3 or 5. See Note 1 on next page.

**2. AM and PM Responsivity Functions:** See Note 1 on next page.

Figure 1. Responsivity Function



$$RS (am) = \sum_{i=0}^n a_i \cdot \cos^i(I) \quad [3]$$

$$RS (pm) = \sum_{j=0}^m b_j \cdot \cos^j(I)$$

where the coefficients  $a_i$  and  $b_j$  are available upon request.

The quality of the function fit to data is shown in Figure 1 and 2.

Figure 2. Net IR Corrected Responsivity Function

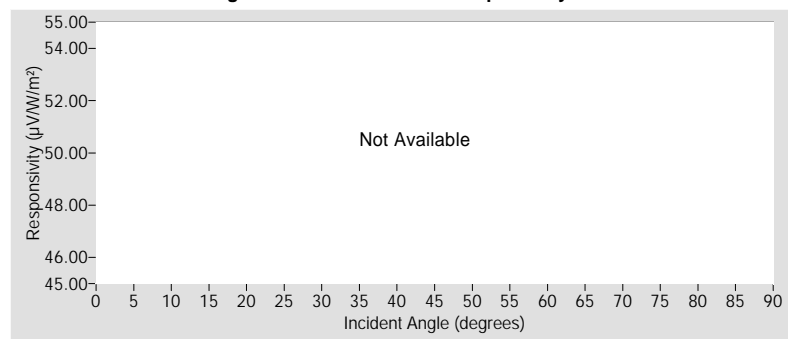


Table 1. Function Validity

	AM	PM
Uncertainty U95 (%)	±1.95	±1.95
R <sup>2</sup>	0.9999998	0.9999949
Valid incidence angle range	16.3° to 79.0°	16.3° to 84.3°
Net IR corr. uncert. U95 (%)	N/A	N/A
Net IR corrected R <sup>2</sup>	N/A	N/A
Corr. valid inc. angle range	N/A	N/A

**3. Nine-degree Bin Responsivity:** See Note 1 on next page.

Table 2. Nine-degree responsivities

Inc. Angle	Responsivity						Net IR Corr. Responsivity					
	AM		PM		Combined		AM		PM		Combined	
	RS ( $\mu V/W/m^2$ )	U95 (%)	RS ( $\mu V/W/m^2$ )	U95 (%)	RS ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)	RSc ( $\mu V/W/m^2$ )	U95 (%)
0-9	13.357	*	13.357	*	13.357	*	N/A	N/A	N/A	N/A	N/A	N/A
9-18	13.344	*	13.335	*	13.340	*	N/A	N/A	N/A	N/A	N/A	N/A
18-27	13.443	±1.98	13.246	±1.97	13.345	±2.38	N/A	N/A	N/A	N/A	N/A	N/A
27-36	13.476	±1.96	13.148	±2.00	13.312	±2.88	N/A	N/A	N/A	N/A	N/A	N/A
36-45	13.464	±1.96	13.018	±2.04	13.241	±3.54	N/A	N/A	N/A	N/A	N/A	N/A
45-54	13.413	±1.96	12.809	±2.13	13.111	±4.44	N/A	N/A	N/A	N/A	N/A	N/A
54-63	13.337	±1.97	12.561	±2.20	12.949	±5.54	N/A	N/A	N/A	N/A	N/A	N/A
63-72	13.270	±2.00	12.197	±2.61	12.734	±7.63	N/A	N/A	N/A	N/A	N/A	N/A
72-81	13.214	*	11.836	±2.14	12.525	*	N/A	N/A	N/A	N/A	N/A	N/A
81-90	13.351	*	8.8486	*	11.100	*	N/A	N/A	N/A	N/A	N/A	N/A

\* The responsivity is based on extrapolated data and the corresponding uncertainty is undefined.

#### 4. The Single Responsivities: See Note 1 below.

**Table 3. Single Responsivities**

Responsivity Characterization	RS ( $\mu\text{V/W/m}^2$ )	U95 † (%)
45°	13.167	+3.32 / -5.49
45° - 55°	13.099	$\pm 3.54$
Composite	13.185	+3.03 / -24.32
45° (Net IR Corr.)	N/A	N/A
45° - 55° (Net IR Corr.)	N/A	N/A
Composite (Net IR Corr.)	N/A	N/A

† Valid incident angle ranges:

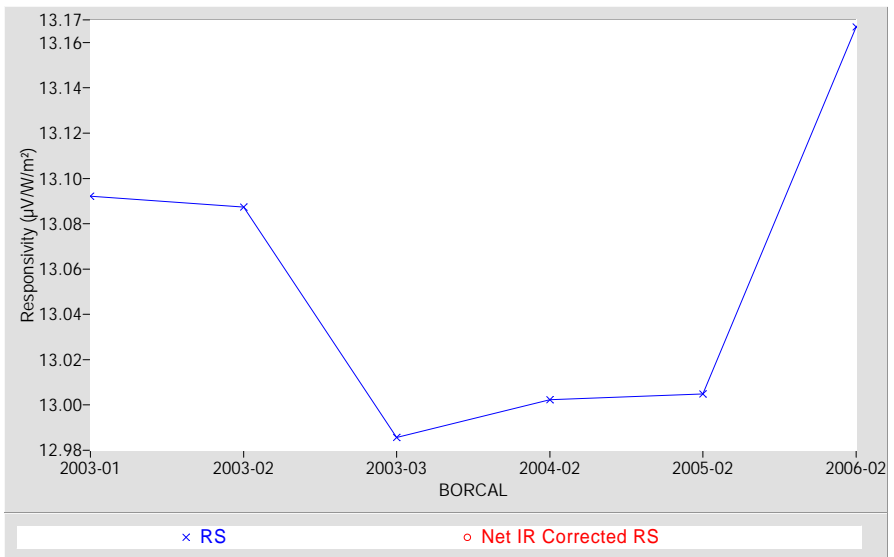
45°: 30.0° to 60.0°

45° - 55°: 45.0° to 55.0°

Composite: 16.3° to 79.0°

The instrument responsivity at  $I = 45^\circ$  may be used to monitor instrument stability. The instrument's history at  $I = 45^\circ$  is shown in Figure 2.

**Figure 2. History of instrument at  $I = 45^\circ$**



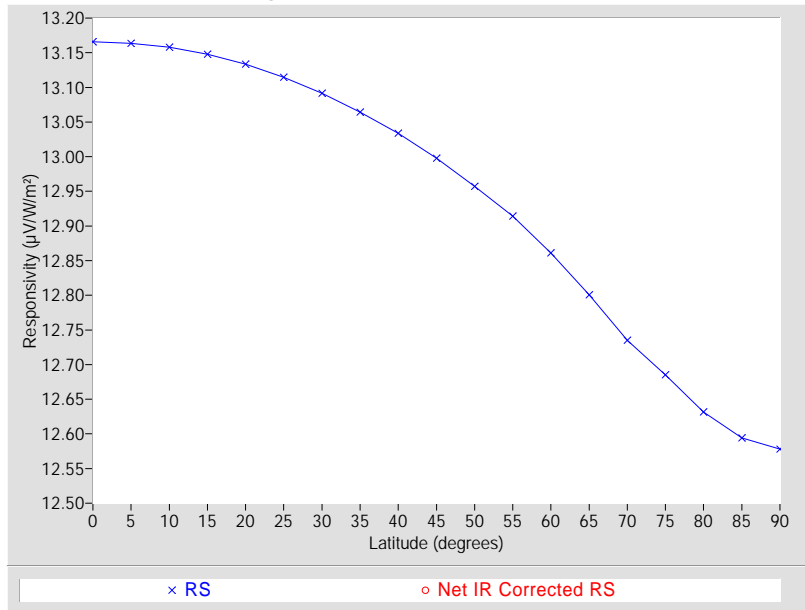
#### 5. Latitude Optimized Responsivity: See Note 1 below.

**Table 4. Latitude Optimized Responsivities**

Latitude	RS ( $\mu\text{V/W/m}^2$ )	Error estimate* (%)	RSc ( $\mu\text{V/W/m}^2$ )		Error estimate* (%)	
			Net IR Corr.	Net IR Corr.	Net IR Corr.	Net IR Corr.
0	13.166	+3.14 / -50.89	N/A	N/A	N/A	N/A
5	13.164	+3.16 / -50.88	N/A	N/A	N/A	N/A
10	13.158	+3.19 / -50.86	N/A	N/A	N/A	N/A
15	13.148	+3.26 / -50.82	N/A	N/A	N/A	N/A
20	13.133	+3.35 / -50.77	N/A	N/A	N/A	N/A
25	13.114	+3.47 / -50.69	N/A	N/A	N/A	N/A
30	13.091	+3.62 / -50.61	N/A	N/A	N/A	N/A
35	13.064	+3.80 / -50.50	N/A	N/A	N/A	N/A
40	13.034	+4.01 / -50.39	N/A	N/A	N/A	N/A
45	12.998	+4.26 / -50.25	N/A	N/A	N/A	N/A
50	12.957	+4.56 / -50.09	N/A	N/A	N/A	N/A
55	12.914	+4.87 / -49.93	N/A	N/A	N/A	N/A
60	12.861	+5.20 / -49.72	N/A	N/A	N/A	N/A
65	12.800	+5.53 / -49.48	N/A	N/A	N/A	N/A
70	12.735	+5.79 / -49.22	N/A	N/A	N/A	N/A
75	12.685	+6.01 / -49.02	N/A	N/A	N/A	N/A
80	12.632	+6.38 / -48.81	N/A	N/A	N/A	N/A
85	12.594	+6.68 / -48.66	N/A	N/A	N/A	N/A
90	12.578	+6.81 / -48.59	N/A	N/A	N/A	N/A

\* Uncertainty is undefined

**Figure 3. Latitude Optimized Responsivities**



#### Application of the responsivities and uncertainties:

The responsivities above are applied according to equation [1]:

##### Example

Instrument responsivity (RS) =  $7.34 \mu\text{V/W/m}^2 \pm 2.7\%$

Instrument output voltage (V) =  $0.00624 \text{ V}$  ( $6240 \mu\text{V}$ )

Irradiance (IRR) =  $V / RS = 6240 / 7.34 = 850.1 \text{ W/m}^2 \pm 2.7\%$

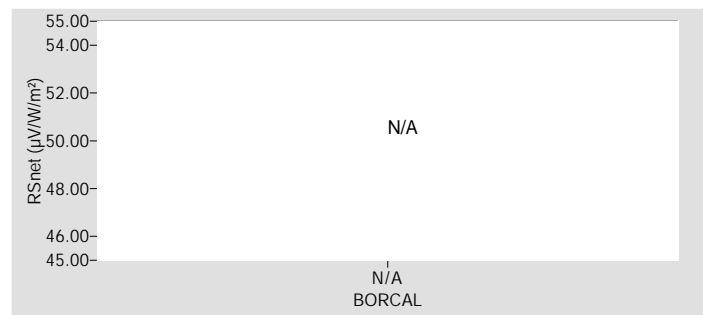
Thus, at the 95% confidence level, the irradiance lies between 827.1 and 873.1  $\text{W/m}^2$

##### Note 1:

All above methods, in conjunction with knowledge of the net infrared and sky irradiance distribution, may be used to determine the effective instrument responsivity with less uncertainties.

#### Instrument's Effective Net Infrared History (RSnet):

**Figure 4. Instrument's RSnet History**



# Ancillary Data for BORCAL 2006-02

Calibration Facility: Solar Radiation Research Laboratory

Latitude: 39.740°N

Longitude: 105.180°W

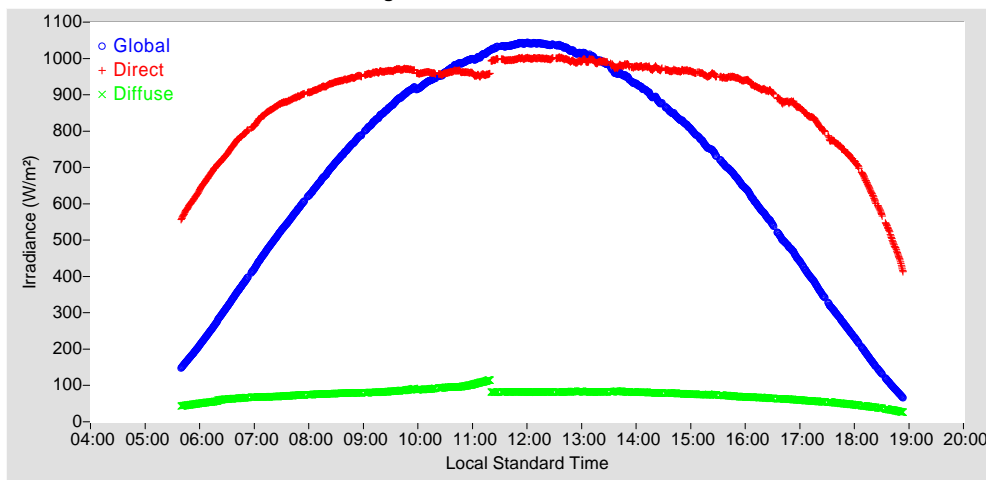
Elevation: 1829.0 meters AMSL

Avg. Station Pressure: 835.0 mBar

Time Zone: -7.0

Reference Irradiance: 0.0° / 0.0° Tilt / Azm

Figure 1. Reference Irradiance



The reference global irradiance (G) is calculated using:  $G = B * \cos(I) + D$ , where I is the refraction-corrected solar incidence angle.

## Meteorological Observations:

Figure 2. Temperature

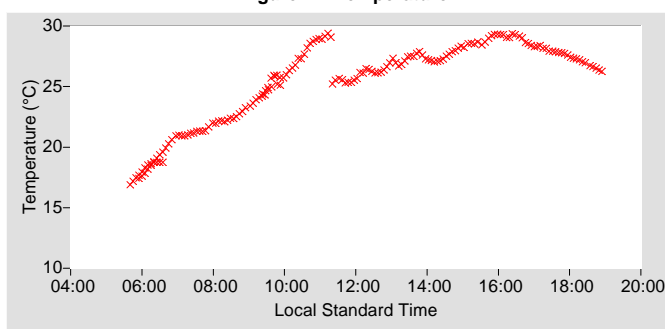


Figure 3. Humidity

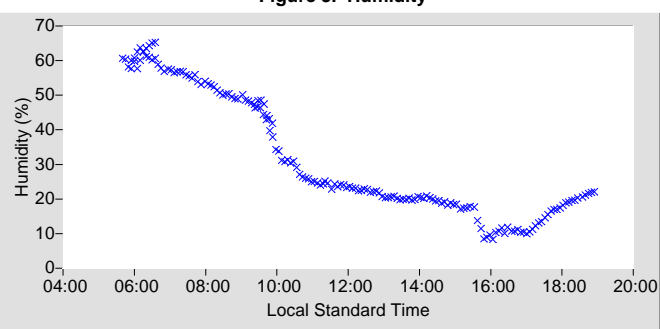


Figure 4. Pressure

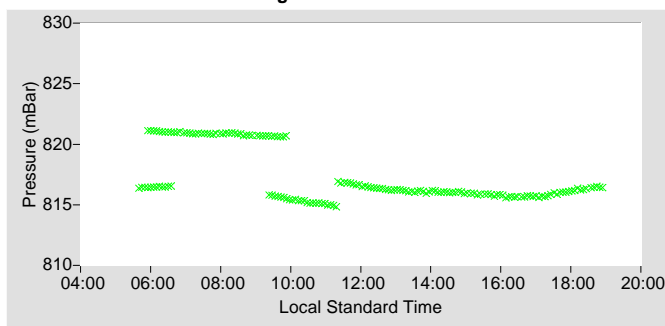


Figure 5. Effective Net Infrared

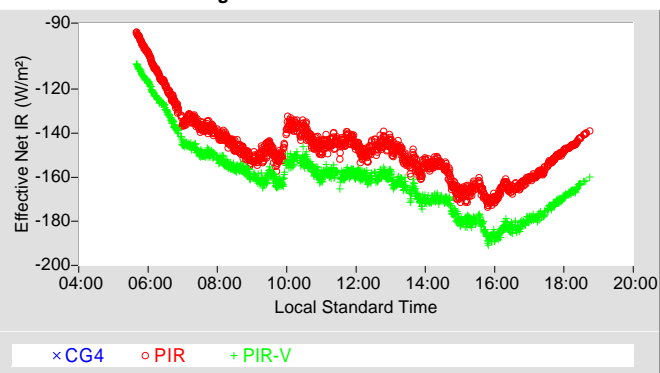


Figure 6. Estimated Broadband Aerosol Optical Depth

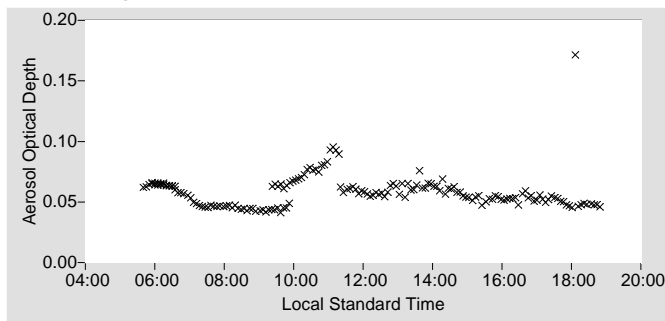


Table 1. Meteorological Observations

Observations	Mean
Temperature (°C)	25.19
Humidity (%)	32.85
Pressure (mBar)	817.3
Est. Aerosol Optical Depth (BB)	0.0582

For other information about the calibration facility visit: <http://www.nrel.gov/srri>

## **Appendix 2**

# **BORCAL Notes**

Instrument, Configuration, and Session Notes for the BORCAL

# BORCAL Notes

---

Facility: Solar Radiation Research Laboratory

Comments:

Avg. Station Pressure & Temperature is for Denver, CO, which is used for the Solar Position Algorithm (SPA).